### Antineutrino Data: Reactor Operational Data Uncertainties

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## Reactor Evaluation Through Inspection of Near-field Antineutrinos (RETINA)



## Translating neutron-based fission into detector event rates $n_b(t) = \frac{N_d}{4\pi I^2} \sigma_b^{IBD} \epsilon_b S_b(t) + B_b$

- $S_b(t)$  = antineutrinos generated for given burnup and • Uncertainties:  $\frac{dN(E,t)}{dEdt} = \frac{P_{th}(t)}{\overline{E_f}(t)} \sum_{i=1}^{4} \frac{f_i(t)s_i(E)c_i^{ne}(E)}{\overline{E_f}(t)}$
- - Thermal power + energy release per fission
  - Relative fission rate for each isotope
  - Fission product distribution
  - Neutron spectrum

## **Operational Uncertainties**

- Initial reactor fuel loading: mass and enrichment
- Reactor geometry
- Total thermal power
- Effect of temperature and other operational parameters on XS and neutron flux
- Propagation of fuel burnup

Antineutrino analysis for continuous monitoring of nuclear reactors: Sensitivity study

Journal of Applied Physics 118, 164902 (2015); https://doi.org/10.1063/1.4934638

#### Comparison of reactor antineutrino sources





#### Low-power core: AFR-100

Parameter	Value (293 K)
Power (MW <sub>t</sub> /MW <sub>e</sub> )	250/100
Cycle length	30 EFPY
Capacity factor	90%
Active core height	110 cm
No. fuel assemblies	150
Initial HM inventory	24.64 t
Fuel form	U-10Zr
Core average enrichment	13.47%
Volumetric power density	58.2 kW/L



C. Grandy. "An Overview of U.S. SFR Design Concepts", GIF/INPRO Workshop on SFR Safety, December, 2011.





### The RETINA detector suite is based on currentgeneration antineutrino detectors

Parameter	PROSPECT AD-I	PROSPECT AD-II (est.)	RETINA (each)	
Scintillator	EJ-309	EJ-309	EJ-309	
Proton density	$5.5 \times 10^{28} / m^3$	N/A	$5.5 \times 10^{28} / m^3$	
Neutron capture dopant	<sup>6</sup> Li	<sup>6</sup> Li	<sup>6</sup> Li	
Target mass (total)	2940 kg	10 t	< 10 t	
Target mass (fiducial)	1480 kg	~ 7 t	5 t	
Efficiency in fiducial vol.	42%	N/A	42%	
Reactor source power	85 MW	85 MW	2600 MW / 250 MW	
Core-detector standoff	6.9 m / 9.4 m	15 m	25 m / 17 m	
S:B ratio	3.1 / 1.8	3.0	~ 8.0 / 1.5	



#### Detector suite configuration



## The UCFR yields multiple SQ of plutonium per assembly, but its purity is compromised

- The UCFR breeds plutonium above the burn zone, depletes it as the burn zone moves upward, and leaves relatively unusable plutonium behind.
- Once steady-state burn zone propagation begins, the amount of weapons-grade plutonium remains relatively constant
- Depleted plutonium below the burn zone is contaminated with both <sup>240</sup>Pu and many fission products.



## The UCFR-1000 antineutrino signal evolves quickly, then enters a steady state



### The AFR-100 yields little plutonium per assembly

- The AFR's low power density (~20% of traditional SFR designs) keeps the average plutonium content per assembly below 8 kg for nearly the entire cycle.
- Plutonium breeding is concentrated in the inner assemblies near the core midplane as part of the effort to offset increased neutron absorption in the late cycle.



 Core-edge plutonium is ultra-pure due to cross section dominance by uranium isotopes (~15% <sup>235</sup>U enrichment), but one SQ cannot be obtained from fewer than two (late-cycle) or three (mid-cycle) assemblies.

# The AFR-100 antineutrino signal evolves gradually over the entire burnup cycle



### Fuel Cross Section Update Scheme



### Effects of XS updates





## Summary

- The uncertainty on the reactor antineutrino source arising from the model of the reactor and its burnup cycle is propagated through the calculated isotopic fission rates, determined by:
  - the initial-state reactor compositions,
  - the microscopic cross sections for each interaction, and
  - the operating history of the reactor.
- The approach to propagating uncertainty on each of these becomes complex due to the significant correlation and anti-correlation introduced through the imposition of a total thermal power output for the reactor.
- Question: what effect covariances will have on uncertainty quantification of antineutrino rate and spectrum?

	0 EFPY	<sup>235</sup> U	<sup>238</sup> U	<sup>239</sup> Pu	<sup>240</sup> Pu	<sup>241</sup> Pu	15 EFPY	<sup>235</sup> U	<sup>238</sup> U	<sup>239</sup> Pu	<sup>240</sup> Pu	<sup>241</sup> Pu
	<sup>235</sup> U	2.95×10 <sup>−6</sup>	-1.20×10 <sup>-5</sup>	<b>−7.23</b> ×10 <sup>−7</sup>	1.13×10 <sup>−7</sup>	−2.87×10 <sup>-7</sup>	<sup>235</sup> U	1.15×10 <sup>−5</sup>	−8.11×10 <sup>-6</sup>	-1.56×10 <sup>-5</sup>	−1.80×10 <sup>-5</sup>	−2.45×10 <sup>-5</sup>
	<sup>238</sup> U	-1.20×10 <sup>-5</sup>	6.49×10 <sup>−5</sup>	9.95×10 <sup>-7</sup>	−2.86×10 <sup>-6</sup>	−2.06×10 <sup>-6</sup>	<sup>238</sup> U	-8.11×10 <sup>-6</sup>	5.75×10 <sup>-5</sup>	-1.39×10 <sup>-5</sup>	-1.80×10 <sup>-5</sup>	-2.47×10 <sup>-5</sup>
	<sup>239</sup> Pu	<b>-7.23</b> ×10 <sup>-7</sup>	9.95×10 <sup>-7</sup>	4.33×10 <sup>-5</sup>	1.23×10 <sup>-5</sup>	1.83×10 <sup>-5</sup>	<sup>239</sup> Pu	-1.56×10 <sup>-5</sup>	-1.39×10 <sup>-5</sup>	3.87×10 <sup>-5</sup>	3.91×10 <sup>-5</sup>	5.21×10 <sup>-5</sup>
	<sup>240</sup> Pu	1.13×10 <sup>−7</sup>	−2.86×10 <sup>-6</sup>	1.23×10 <sup>-5</sup>	5.09×10 <sup>-5</sup>	1.14×10 <sup>−5</sup>	<sup>240</sup> Pu	-1.80×10 <sup>-5</sup>	-1.80×10 <sup>-5</sup>	3.91×10 <sup>−5</sup>	2.55×10 <sup>-4</sup>	2.41×10 <sup>−4</sup>
	<sup>241</sup> Pu	-2.87×10 <sup>-7</sup>	-2.06×10 <sup>-6</sup>	1.83×10 <sup>-5</sup>	1.14×10 <sup>-5</sup>	1.16×10 <sup>-4</sup>	<sup>241</sup> Pu	−2.45×10 <sup>-5</sup>	-2.47×10 <sup>-5</sup>	5.21×10 <sup>-5</sup>	2.41×10 <sup>-4</sup>	7.18×10 <sup>−4</sup>
	1 EFPY	<sup>235</sup> U	<sup>238</sup> U	<sup>239</sup> Pu	<sup>240</sup> Pu	<sup>241</sup> Pu	30 EFPY	<sup>235</sup> U	<sup>238</sup> U	<sup>239</sup> Pu	<sup>240</sup> Pu	<sup>241</sup> Pu
	1 Е <b>FPY</b> <sup>235</sup> U	<sup>235</sup> U 3.23×10 <sup>−6</sup>	<sup>238</sup> U −1.22×10 <sup>-5</sup>	<sup>239</sup> Pu -4.91×10 <sup>-6</sup>	<sup>240</sup> Pu −5.07×10 <sup>-6</sup>	<sup>241</sup> Pu −5.97×10 <sup>-6</sup>	30 Е <b>ГРҮ</b> <sup>235</sup> U	<sup>235</sup> ∪ 1.37×10 <sup>-5</sup>	<sup>238</sup> U −8.12×10 <sup>-7</sup>	<sup>239</sup> Pu −8.38×10 <sup>-6</sup>	<sup>240</sup> Pu −9.28×10 <sup>-6</sup>	<sup>241</sup> Pu −1.49×10 <sup>-5</sup>
	1 Е <b>FPY</b> <sup>235</sup> U <sup>238</sup> U	<sup>235</sup> U 3.23×10 <sup>-6</sup> −1.22×10 <sup>-5</sup>	<sup>238</sup> U −1.22×10 <sup>-5</sup> 6.41×10 <sup>-5</sup>	239Pu -4.91×10 <sup>-6</sup> 3.65×10 <sup>-6</sup>	<sup>240</sup> Pu -5.07×10 <sup>-6</sup> -8.37×10 <sup>-7</sup>	<sup>241</sup> Pu -5.97×10 <sup>-6</sup> -2.81×10 <sup>-6</sup>	30 Е <b>FPY</b> <sup>235</sup> U <sup>238</sup> U	235U 1.37×10 <sup>-5</sup> −8.12×10 <sup>-7</sup>	<sup>238</sup> U −8.12×10 <sup>-7</sup> 5.77×10 <sup>-5</sup>	239pu -8.38×10 <sup>-6</sup> -1.63×10 <sup>-5</sup>	<sup>240</sup> Pu −9.28×10 <sup>-6</sup> −1.93×10 <sup>-5</sup>	<sup>241</sup> Pu −1.49×10 <sup>-5</sup> −2.48×10 <sup>-5</sup>
	1 Е <b>FPY</b> <sup>235</sup> U <sup>238</sup> U <sup>239</sup> Pu	235U 3.23×10 <sup>-6</sup> -1.22×10 <sup>-5</sup> -4.91×10 <sup>-6</sup>	238U -1.22×10 <sup>-5</sup> 6.41×10 <sup>-5</sup> 3.65×10 <sup>-6</sup>	239Pu -4.91×10 <sup>-6</sup> 3.65×10 <sup>-6</sup> 1.08×10 <sup>-4</sup>	240 Pu -5.07 × 10 <sup>-6</sup> -8.37 × 10 <sup>-7</sup> 1.16 × 10 <sup>-4</sup>	241 <b>Pu</b> -5.97×10 <sup>-6</sup> -2.81×10 <sup>-6</sup> 1.34×10 <sup>-4</sup>	30 Е <b>FPY</b> <sup>235</sup> U <sup>238</sup> U <sup>239</sup> Pu	235U 1.37×10 <sup>-5</sup> −8.12×10 <sup>-7</sup> −8.38×10 <sup>-6</sup>	238U -8.12×10 <sup>-7</sup> 5.77×10 <sup>-5</sup> -1.63×10 <sup>-5</sup>	239pu -8.38×10 <sup>-6</sup> -1.63×10 <sup>-5</sup> 1.26×10 <sup>-5</sup>	<sup>240</sup> Pu −9.28×10 <sup>-6</sup> −1.93×10 <sup>-5</sup> 5.22×10 <sup>-6</sup>	241Pu -1.49×10 <sup>-5</sup> -2.48×10 <sup>-5</sup> 7.38×10 <sup>-6</sup>
	1 EFPY 235U 238U 239Pu 240Pu	235U 3.23×10 <sup>-6</sup> -1.22×10 <sup>-5</sup> -4.91×10 <sup>-6</sup> -5.07×10 <sup>-6</sup>	238U -1.22×10 <sup>-5</sup> 6.41×10 <sup>-5</sup> 3.65×10 <sup>-6</sup> -8.37×10 <sup>-7</sup>	239Pu -4.91×10 <sup>-6</sup> 3.65×10 <sup>-6</sup> 1.08×10 <sup>-4</sup>	240 pu -5.07 × 10 <sup>-6</sup> -8.37 × 10 <sup>-7</sup> 1.16 × 10 <sup>-4</sup> 3.28 × 10 <sup>-4</sup>	241Pu -5.97×10 <sup>-6</sup> -2.81×10 <sup>-6</sup> 1.34×10 <sup>-4</sup> 3.01×10 <sup>-4</sup>	30 EFPY <sup>235</sup> U <sup>238</sup> U <sup>239</sup> Pu <sup>240</sup> Pu	<b>235</b> U 1.37×10 <sup>-5</sup> -8.12×10 <sup>-7</sup> -8.38×10 <sup>-6</sup>	238U -8.12×10 <sup>-7</sup> 5.77×10 <sup>-5</sup> -1.63×10 <sup>-5</sup>	<ul> <li>239Pu</li> <li>-8.38×10<sup>-6</sup></li> <li>-1.63×10<sup>-5</sup></li> <li>1.26×10<sup>-5</sup></li> <li>5.22×10<sup>-6</sup></li> </ul>	<ul> <li>240 Pu</li> <li>-9.28 × 10<sup>-6</sup></li> <li>-1.93 × 10<sup>-5</sup></li> <li>5.22 × 10<sup>-6</sup></li> <li>2.07 × 10<sup>-4</sup></li> </ul>	<ul> <li>241Pu</li> <li>-1.49×10<sup>-5</sup></li> <li>-2.48×10<sup>-5</sup></li> <li>7.38×10<sup>-6</sup></li> <li>1.64×10<sup>-4</sup></li> </ul>
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## Questions

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