ENDF/B-VIIß3 Data Testing

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Introduction

- Data testing at LANL has concentrated on MCNP5 eigenvalue calculations for a variety of critical benchmarks defined in the 2005 Edition of the International Criticality Safety Benchmark Evaluation Project (ICSBEP) Handbook.
 - xxx-MET-FAST (HEU, PU, MIX; bare, water and/or polyethylene reflected, metallic reflectors);
 - xxx-SOL-THERM (HEU, LEU, ²³³U or Pu; bare and water, polyethylene or beryllium reflected);
 - LEU-COMP-THERM (water moderated, with and without lead reflectors).
- Eigenvalues are determined based upon tracking 25 million to 50 million neutron histories.
 - The uncertainty in the MCNP5 eigenvalue is typically less than 25 pcm.





"LANL"-MET-FAST Benchmarks

- "Traditional" LANL Fast Benchmarks are significantly improved with ENDF/B-VIIβ3 cross sections.
 - HEU-MET-FAST-001 (Godiva)
 - HEU-MET-FAST-028 (Flattop-28)
 - IEU-MET-FAST-007 (Big-10)
 - PU-MET-FAST-001 (Jezebel)
 - PU-MET-FAST-002 (Jezebel-240)
 - PU-MET-FAST-006 (Flattop-Pu)
 - PU-MET-FAST-008c (Thor)
 - U233-MET-FAST-001 (Jezebel-23)
 - U233-MET-FAST-006 (Flattop-23)





"LANL"-MET-FAST Benchmarks



- With ENDF/B-VI.8:
 - Reflector bias is evident.
 - Average k_{eff} C/E is 1.0008.
 - Not bad, but lucky.
 - Population standard deviation is ±0.0056.
 - Large deviations from unity in calculated eigenvalues.





"LANL"-MET-FAST Benchmarks



- With ENDF/B-VIIβ3:
 - Reflector bias is virtually eliminated.
 - Average k_{eff} C/E is 1.0001.
 - Population standard deviation is ±0.0014.





Other HEU & PU-MET-FAST Benchmarks

Other xxx-MET-FAST Benchmarks

- HEU-MET-FAST bare systems:
 - HEU-MET-FAST-008
 - HEU-MET-FAST-015 & -065
 - HEU-MET-FAST-018
 - HEU-MET-FAST-051
- HEU-MET-FAST reflected systems
 - HEU-MET-FAST-004
 - HEU-MET-FAST-007, -011
 - HEU-MET-FAST-012, -022
 - HEU-MET-FAST-013, -021
 - HEU-MET-FAST-027, -057, -064
 - HEU-MET-FAST-014

- (water)
- (polyethylene)
- (aluminum)
- (steel)
- (lead)
- (uranium)





Other HEU & PU-MET-FAST Benchmarks



- With ENDF/B-VI.8:
 - Most calculated eigenvalues are biased low.
 - Small reflector bias for low-Z materials.
 - Lead reflector bias is large.
 - Average k_{eff} C/E and the population standard deviation are 0.9955 ± 0.0030.





Other HEU & PU-MET-FAST Benchmarks



- With ENDF/B-VIIβ3:
 - Calculated eigenvalues are closer to unity and many are within the experimental uncertainty.
 - Small reflector bias for low-Z materials.
 - Lead reflector bias is significantly reduced.
 - Average k_{eff} C/E and the population standard deviation are 0.9984 ± 0.0016.





Other HEU & PU-MET-FAST Benchmarks

- Other xxx-MET-FAST Benchmarks (con't)
 - PU-MET-FAST bare systems
 - PU-MET-FAST-022, -029
 - PU-MET-FAST Reflected Systems
 - PU-MET-FAST-011 (water)
 - PU-MET-FAST-024 (polyethylene)
 - PU-MET-FAST-018, -019 (beryllium)
 - PU-MET-FAST-023 (graphite)
 - PU-MET-FAST-009 (aluminum)
 - PU-MET-FAST-025, -026 (steel)
 - PU-MET-FAST-035 (lead)
 - PU-MET-FAST-010, -020 (uranium)





Other HEU & PU-MET-FAST Benchmarks



- With ENDF/B-VI.8:
 - Calculated eigenvalues are generally biased low.
 - Reflector bias for low-Z materials is observed.
 - Lead reflector bias is large.
 - Average k_{eff} C/E and the population standard deviation are 0.9989 ± 0.0039.





Other HEU & PU-MET-FAST Benchmarks



- With ENDF/B-VIIβ3:
 - Calculated eigenvalues are closer to unity and most are within the experimental uncertainty.
 - Reflector bias for low-Z materials is reduced.
 - Lead reflector bias is eliminated.
 - Average k_{eff} C/E and the population standard deviation are 0.9995 ± 0.0025.





HEU-, Pu- and U233-MET-FAST Benchmarks

- k_{eff} C/E values are significantly more accurate when using ENDF/B-VIIβ3 cross sections, compared to the corresponding values obtained with ENDF/B-VI.8 cross sections.
 - The historical uranium reflector bias has been eliminated.
- Subsequent slides expand on this conclusion, examining k_{eff} C/E for FAST systems with polyethylene, beryllium and lead reflectors.





HEU-MET-FAST Benchmarks Polyethylene Reflected & Moderated



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- HEU-MET-FAST-007
 - 10" x 10" HEU slabs interleaved with polyethylene (cases 1 18).
 - 5" x 10" HEU slabs interleaved with polyethylene (cases 19 – 26).
 - 5" x 10" HEU slabs interleaved with polyethylene and surrounded by 6" of polyethylene (cases 35 – 43).
- Average ENDF/B-VI.8 k_{eff} C/E's are:
 - 0.9983 ± 0.0016
 - 0.9990 ± 0.0007
 - 0.9994 ± 0.0008



HEU-MET-FAST Benchmarks Polyethylene Reflected & Moderated



FST 1943

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 - 5" x 10" HEU slabs interleaved with polyethylene (cases 19 – 26).
 - 5" x 10" HEU slabs interleaved with polyethylene and surrounded by 6" of polyethylene (cases 35 – 43).
- Average ENDF/B-VIIβ3 k_{eff} C/E's are:
 - 1.0018 ± 0.0017
 - -1.0028 ± 0.0008
 - -1.0025 ± 0.0013



HEU-MET-FAST Benchmarks Polyethylene Reflected & Moderated

- Average calculated eigenvalue increase is ~0.3%.
 - Consistent with the general increase seen for other HEU benchmarks.
- ENDF/B-VI.8 results are 0.1% to 0.2% too low.
- ENDF/B-VIIβ3 results are 0.2% to 0.3% too high.
 - For Crit Safety its better to calculate high, but decease in absolute accuracy is disappointing.





- Fast, beryllium reflected benchmarks
 - HEU-MET-FAST-009
 - HEU-MET-FAST-010
 - HEU-MET-FAST-016
 - HEU-MET-FAST-017
 - HEU-MET-FAST-041
 - HEU-MET-FAST-058
 - HEU-MET-FAST-066
 - HEU-MET-FAST-077 (preliminary model)
 - Approved for publication in the 2006 edition of the ICSBEP Handbook.
 - MIX-MET-FAST-007







- ENDF/B-VI.8.
- HEU-MET-FAST-008 is the base case for HEU-MET-FAST-009 & -010.
 - Be reflector surrounding an HEU sphere.
- HEU-MET-FAST-015 & -065 are the base case for HEU-MET-FAST-016 & -017.
 - Be reflectors and interleaved plates in a cylindrical stack.







- ENDF/B-VIIβ3.
- HEU-MET-FAST-008 is the base case for HEU-MET-FAST-009 & -010.
 - Be reflector surrounding an HEU sphere.
- HEU-MET-FAST-015 & -065 are the base case for HEU-MET-FAST-016 & -017.
 - Be reflectors and interleaved plates in a cylindrical stack.







- HMF41 (2 cases)
 - LANL experiment.
 - HEU spherical core.
 - HEU radii are 6.73 cm and 5.64
 - Be reflector.
 - Be reflector thicknesses are 4.70 cm and 11.79 cm.







- HMF58 (5 cases)
 - LLNL experiment (Nimbus).
 - HEU spherical core.
 - HEU Core radii varied from 5.2 cm to 7.48 cm.
 - Be reflector.
 - Be reflector thickness varied from 20.26 cm to 2.22 cm.









- LLNL experiment (Nimbus).
- HEU spherical core.
 - HEU Core inner cavity radii varied from 3.15 cm to 6.54 cm.
 - HEU Core outer radii varied from 6.54 cm to 9.13 cm.
- Be moderator and reflector.
 - Be moderator placed within inner HEU cavity.
 - Be reflector thickness varied from 13.20 cm to 3.86 cm.
- Different biases and impurities.



HEU-MET-FAST Benchmarks – Be Reflected



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- HMF77 (8 cases)
 - Preliminary model.
 - LLNL experiment (Nimbus).
 - HEU spherical core.
 - HEU Core inner cavity radii varied from 3.15 cm to 6.54 cm.
 - HEU Core outer radii varied from 6.54 cm to 9.13 cm.
 - Be reflector.
 - Inner HEU cavity is void.
 - Be reflector thickness varied from 14.73 cm to 4.47 cm.

• ENDF/B-VIIβ2 results





- MMF7 (23 cases)
 LLNL experiment.
 - Pu core (one of five radii from 3.13 cm to 4.07 cm).
 - HEU inner reflector (various thickness, from ~0.6 cm to ~3.4 cm).
 - Be outer reflector (various thickness, from ~20.0 cm to ~0.7 cm).







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- ENDF/B-VI.8
- Previous figures showed k_{eff} C/E versus Be reflector thickness.
- What about another parameter, such as spectrum (Above-Thermal Fission Fraction).





- ENDF/B-VIIβ3
- Previous figures showed k_{eff} C/E versus Be reflector thickness.
- What about another parameter, such as spectrum (Above-Thermal Fission Fraction).





Thermal ²³³U Benchmarks with Beryllium



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- Thermal ²³³U solution benchmarks with beryllium or polyethylene reflectors.
- Decreasing k_{eff} C/E trend with increasing spectrum hardness.
- This is opposite the k_{eff} C/E trend observed with ²³³U water only assemblies.



Thermal ²³³U Benchmarks -Bare or Water Reflected



- Thermal ²³³U solution benchmarks, bare or water reflected.
- Increasing k_{eff} C/E trend with increasing spectrum hardness.
- This is opposite the k_{eff} C/E trend observed with ²³³U polyethylene or beryllium reflected assemblies.



Benchmarks with Beryllium

- Overall accuracy of k_{eff} C/E calculations with the revised beryllium cross sections is inconsistent, as the
 - revised beryllium cross sections have lead to more accurate calculated eigenvalues for the HEU-MET-FAST-009, -010, -016, -041, -058 and MIX-MET-FAST-007 benchmarks.
 - but the revised beryllium cross sections have lead to less accurate calculated eigenvalues for the HEU-MET-FAST-066 and HEU-MET-FAST-077 benchmarks.
- Results for ²³³U critical systems are also contradictory.
 - Positive k_{eff} C/E trend in water reflected assemblies; negative k_{eff} C/E trend in polyethylene or beryllium reflected assemblies.
- We look forward to including new RPI data in future analyses.





FAST & Thermal Benchmarks – Pb Reflected

- HEU, lead reflected benchmarks
 - HEU-MET-FAST-027
 - HEU-MET-FAST-018 is the "base case".
 - HEU-MET-FAST-064
 - HEU-MET-FAST-015 is the "base case".
 - HEU-MET-FAST-057
- Pu, lead reflected benchmarks
 - HEU-MET-FAST-035
 - Pu-MET-FAST-022 is the "base case".
- LEU, lead reflected benchmarks
 - LEU-COMP-THERM-010
 - LEU-COMP-THERM-002 is the "base case".





FAST & Thermal Benchmarks – Pb Reflected



• ENDF/B-VI.8

- There is an obvious lead reflector bias in k_{eff} C/E values.
- HMF18 is a base case for HMF27.
- HMF15 is a base case for HMF64.
- PMF22 is a base case for PMF35.
- LCT2 is a base case for LCT10.





FAST & Thermal Benchmarks – Pb Reflected



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- The lead reflector bias is virtually eliminated for fast systems; there is little improvement for thermal systems.
- HMF18 is a base case for HMF27.
- HMF15 is a base case for HMF64.
- PMF22 is a base case for PMF35.
- LCT2 is a base case for LCT10.





FAST & Thermal Benchmarks – Pb Reflected

- Fast, lead reflected critical assembly k_{eff} C/E values are significantly more accurate when ENDF/B-VIIb3 cross sections are used.
- These same k_{eff} C/E improvements are not seen for thermal, lowenriched uranium critical systems.





LEU-COMP-THERM Benchmarks

- We have calculated k_{eff} for a suite of seven LEU-COMP-THERM evaluations representing experimental programs from five countries:
 - LEU-COMP-THERM-001 (2.35 w/o²³⁵U, United States PNL)
 - LEU-COMP-THERM-002 (4.31 w/o²³⁵U, United States PNL)
 - LEU-COMP-THERM-006 (2.6 w/o²³⁵U, Japan)
 - LEU-COMP-THERM-007 (4.74 w/o²³⁵U, France, Valduc)
 - LEU-COMP-THERM-022 (9.8 w/o ²³⁵U, Russia Kurchatov)
 - LEU-COMP-THERM-024 (9.8 w/o ²³⁵U, Russia Kurchatov)
 - LEU-COMP-THERM-039 (4.74 w/o²³⁵U, France, Valduc)





LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-001 (8 cases)
- 2.35 w/o ²³⁵UO₂
- 1.27 cm rod OD
- 1.118 cm fuel OD
- Rectangular, 2.03 cm rod pitch.
- Nearly square array of rods, or three nearly square clusters.



LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-002 (5 cases)
- 4.31 w/o ²³⁵UO₂
- 1.415 cm rod OD
- 1.265 cm fuel OD
- Rectangular, 2.54 cm rod pitch.
- Nearly square arrays, or three groups of either 15 x 8 (case 4) or 13 x 8 (case 5) clusters.
- Cases 4 & 5 are "base case" for LEU-COMP-THERM-010.



LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-006 (18 cases)
- 2.6 w/o ²³⁵UO₂
- 1.417 cm rod OD
- 1.25 cm fuel OD
- Square array, set on one of 1.849 cm, 1.956 cm, 2.150 cm or 2.293 cm pitch
- Array size is one of 15 x 15 up to 21 x 21.

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LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-006 (18 cases)
- 2.6 w/o ²³⁵UO₂
- 1.417 cm rod OD
- 1.25 cm fuel OD
- Square array, set on one of 1.849 cm, 1.956 cm, 2.150 cm or 2.293 cm pitch
- Array size is one of 15 x 15 up to 21 x 21.





LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-007 (10 cases)
- 4.738 w/o ²³⁵UO₂
- 0.94 cm rod OD
- 0.79 cm fuel OD
- Rectangular or hexagonal rod pitch, from ~1.26 cm to ~2.52 cm pitch.
- Square, Hexagonal and Cylindrical array patterns.

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LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-007 (10 cases)
- 4.738 w/o ²³⁵UO₂
- 0.94 cm rod OD
- 0.79 cm fuel OD
- Rectangular or hexagonal rod pitch, from ~1.26 cm to ~2.52 cm pitch.
- Square, Hexagonal and Cylindrical array patterns.

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LEU-COMP-THERM Benchmarks



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- LEU-COMP-THERM-022 (7 cases)
- 10 w/o ²³⁵UO₂
- 0.51 cm rod OD
- 0.416 cm fuel OD
- Hexagonal pitch, to produce a cylindrical shape.
- Rod pitch is 0.7cm, 0.8cm, 1.0cm, 1.22cm, 1.4cm, 1.83cm and 1.85 cm.



LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-024 (2 cases)
- 10 w/o ²³⁵UO₂
- 0.51 cm rod OD
- 0.416 cm fuel OD
- Case 1 is nearly square rectangular array of 2625 rods set on a 0.62 cm pitch.
- Case 2 is long, narrow hexagonal array of 1297 rods set on a 0.62/√2 cm pitch.





LEU-COMP-THERM Benchmarks



- LEU-COMP-THERM-039 (10 cases)
- 4.738 w/o ²³⁵UO₂
- 0.94 cm rod OD
- 0.79 cm fuel OD
- Rectangular, 1.26 cm pitch.
- Square arrays (22 x 22 rods or 21 x 21 rods) with "water holes".





LEU-COMP-THERM Benchmarks



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 Summary of all LEU-COMP-THERM results.





LEU-COMP-THERM Benchmarks

- LEU-COMP-THERM eigenvalues are generally low, by 500 pcm to 1000 pcm, with ENDF/B-VI.8 cross sections.
 - Average eigenvalue for 45 critical configurations from seven LEU-COMP-THERM evaluations is 0.9945 ± 0.0005 (mean) ± 0.0036 (population).
- LEU-COMP-THERM eigenvalues have increased to near unity with ENDF/B-VIIβ3 cross sections.
 - Average eigenvalue for 53 critical configurations from seven LEU-COMP-THERM evaluations is 1.0001 ± 0.0003 (mean) ± 0.0025 (population).





HEU-SOL-THERM Benchmarks

- Homogenous solution benchmark k_{eff} C/Es have been correlated against Above-Thermal Leakage Fraction (ATLF).
- The benchmark suite consists of 42 critical configurations defined in ten HEU-SOL-THERM evaluations.
 - All Rocky Flats and ORNL benchmarks used on past data testing efforts are now incorporated in the ICSBEP Handbook.
- HEU-SOL-THERM results are supplemented with calculations of Japanese LEU-SOL-THERM benchmarks.
 - LEU-SOL-THERM-004, -007, -020 & -021.
 - Bare and water reflected (cylindrical) assemblies are represented.





HEU-SOL-THERM Benchmarks



- HEU(&LEU)-SOL-THERM-xxx
- Experiments from ORNL, Rocky Flats and Japan.
- With ENDF/B-VI.8 Cross Sections:
 - ATLF Correlation shows no bias nor trend in k_{eff} C/E.
 - No bias nor trend versus other parameters:
 - ATFF,
 - Hydrogen abs,
 - Bare versus Reflected,
 - N versus F.



HEU-SOL-THERM Benchmarks



- HEU(&LEU)-SOL-THERM-xxx
- Experiments from ORNL, Rocky Flats and Japan.
- With ENDF/B-VIIβ3 Cross Sections:
 - ATLF Correlation shows no bias nor trend in k_{eff} C/E.
 - No bias nor trend versus other parameters
 - ATFF,
 - Hydrogen abs,
 - Bare versus Reflected,
 - N versus F.



HEU-SOL-THERM Benchmarks

- ENDF/B-VI.8 HST & LST k_{eff} C/E values are very accurate.
 - There is no trend with ATLF or other parameters (such as Above-Thermal Fission Fraction, ATFF; Hydrogen absorption fraction, ...).
 - The average eigenvalue for 42 HST critical configurations from ten HST evaluations is 1.0002 ± 0.0007 (mean) ± 0.0046 (population); and from 62 HST & LST critical configurations is 1.0001 ± 0.0005 (mean) ± 0.0039 (population).
- ENDF/B-VIIβ3 HST & LST k_{eff} C/E values are also very accurate.
 - There is no trend with ATLF or other parameters.
 - The Above-Thermal Leakage Fraction (ATLF) correlation is insensitive to weighting of the individual HST eigenvalues.
 - The average eigenvalue for 42 HST critical configurations from ten HST evaluations is 1.0003 ± 0.0007 (mean) ± 0.0047 (population); and from 62 HST & LST critical configurations is 1.0003 ± 0.0005 (mean) ± 0.0039





HEU Benchmarks – Fast to Thermal



 The combination of HEU-MET-FAST-007 & the HEU-SOL-THERM-xxx benchmarks span the complete fission energy space.

 k_{eff} trend is close to but slightly greater than unity.





PU-SOL-THERM Benchmarks

- We have calculated k_{eff} for a suite of nine PU-SOL-THERM evaluations (109 cases) with ENDF/B-VIIβ2 cross sections.
 - Replicate calculations have been performed for 26 configurations with ENDF/B-VIIβ3 cross sections.
 - The average difference in k_{eff} is 2 pcm.
 - PU-SOL-THERM-001 (11.5" diameter water reflected sphere)
 - PU-SOL-THERM-002 (12" diameter water reflected sphere)
 - PU-SOL-THERM-003 (13" diameter water reflected sphere)
 - PU-SOL-THERM-004 (14" diameter water reflected sphere)
 - PU-SOL-THERM-005 (more 14" diameter ...)
 - PU-SOL-THERM-006 (15" diameter water reflected sphere)
 - PU-SOL-THERM-009 (48" diameter sphere, bare)
 - PU-SOL-THERM-011 (16", 18" diameter spheres, bare)
 - PU-SOL-THERM-018 (24" diameter water reflected cylinder)

Published in the 2006 edition of the ICSBEP Handbook)

PU-SOL-THERM Benchmarks – ENDF/B-VI.8



PU-SOL-THERM-xxx

- USA & French experiments.
- 15 evaluations, 109 configurations.
- Benchmark uncertainties range from 0.0012 to 0.0058.
- Highly thermal

 82% to 99%
 thermal fission.
- k_{eff} C/E ranges from 0.9941 to 1.0194.
- Average k_{eff} C/E is 1.0039.
- Population standard deviation is 0.0043.





PU-SOL-THERM Benchmarks – ENDF/B-VIIβ2



• PU-SOL-THERM-xxx

- USA & French experiments.
- 15 evaluations, 109 configurations.
- Benchmark uncertainties range from 0.0012 to 0.0058.
- Highly thermal

 82% to 99%
 thermal fission.
- k_{eff} C/E ranges from 0.9938 to 1.0189.
- Average k_{eff} C/E is 1.0048.
- Population standard deviation is 0.0044.







- PU-SOL-THERM-xxx
- PST18 is new in 2006.
- k_{eff} C/E for PST18 are in line with those obtained with higher
 ²³⁹Pu enrichments.
- Therefore, no k_{eff} C/E trend with ²³⁹Pu enrichment.







- PU-SOL-THERM-xxx
- No k_{eff} C/E trend with Pu concentration.
- Not shown, but no k_{eff} C/E trend with Above-Thermal Fission Fraction (ATFF).
- Not shown, but no k_{eff} C/E trend with ²³⁹Pu absorption fraction.
- Not shown, but no k_{eff} C/E trend with Neutron Lethargy.





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- PU-SOL-THERM-xxx
- No k_{eff} C/E trend with Above-Thermal Fission Fraction (ATFF).





- PU-SOL-THERM-xxx
- No k_{eff} C/E trend with ²³⁹Pu absorption fraction.



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- PU-SOL-THERM-xxx
- No k_{eff} C/E trend with Neutron Lethargy.





PU-SOL-THERM Benchmarks

- Little to no changes have been made to low energy ²³⁹Pu cross sections for ENDF/B-VII.
- Modest changes in hydrogen and oxygen cross sections result in a small (~0.1%) increase in k_{eff} C/E.
- Additional work seemed to be needed to improve calculations of thermal Pu system eigenvalues.





HEU/D₂O Benchmarks

- HEU-SOL-THERM-004
 - Heavy water reflected benchmarks

- HEU-SOL-THERM-020
 - Heavy water unreflected benchmarks
- Significant biases are observed in calculated eigenvalues for both ENDF/B-VI.8 and ENDF/B-VIIβ2 cross section data sets.
 - Unreflected benchmark eigenvalues exhibit an increasing trend with increasing D/²³⁵U.





HEU/D₂O Benchmarks





Comparison Between MCNP5 (LANL) and Tripoli 4.4.1 (Sublet)

- Excellent agreement in calculated eigenvalues is observed for MCNP5 and Tripoli-4.4.1 for a variety of benchmarks.
 - Previous differences in LEU-COMP-THERM-006 have been attributed to slightly different fuel compositions.
 - Previous differences in selected HEU-SOL-THERM-001 eigenvalues are attributed to different normalizations.





Comparison Between MCNP5 (LANL) and Tripoli 4.4.1 (Sublet)



- Excellent agreement observed in calculated eigenvalues for all benchmark types.
- MCNP/Tripoli k_{eff} for unmoderated systems is 0.9999.
- MCNP/Tripoli k_{eff} for LEU-COMP-THERM systems is 1.0001.
- MCNP/Tripoli k_{eff} for LEU-COMP-THERM systems is 1.0003.



