The Problem with the Nuclear Data for Deuterium-Uranium Systems



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Outline

- International <u>Criticality Safety Benchmark Evaluation</u> <u>Project (ICSBEP) HEU D₂O Solution Thermal critical</u> experiments (HST-004 & -020)
- AECL Chalk River Laboratories (CRL) ZED-2 (Zero Energy Deuterium) critical experiments
 - <u>Existing</u>: NU (Natural Uranium) in hexagonal lattices; D₂O & air 'cooled' fuel channels
 - <u>Recent</u>: SEU (Slightly Enriched Uranium) CANFLEX bundles in square lattices; H₂O & air cooled
- Numerical benchmark studies
 - CANDU-SCWR (<u>CAN</u>ada <u>D</u>euterium <u>U</u>ranium <u>Superc</u>ritical <u>W</u>ater <u>R</u>eactor) lattice
 - ²H-reflected U-metal sphere
- Summary/Conclusions

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Background:

Changes to ENDF/B-VI²H cross-section data

- ENDF/B-VI.4 [MCNP ZAID=1002.60c & .64c processed by LANL]
- ENDF/B-VI.5 (through ENDF/B-VI.8) [ZAID=1002.66c]
 - data range extended from 100 to 150 MeV
 - (n,2n), elastic & inelastic cross sections revised slightly above 10 MeV to match experimental data better
 - angular distributions for elastic scattering revised slightly >20 MeV & <3.2 MeV to improve agreement with measurement
 - <u>Surprisingly large reactivity change</u> (~9.7 mk) observed by LANL & KAPL for HEU D₂O solution benchmarks HEU-SOL-THERM (HST-004 & 020)
- <u>Ouestions raised</u>:
 - What is the impact for other D_2O critical systems?
 - Which is better: ENDF/B-VI.4 [1002.60c,.64c] or -VI.5 [1002.66c]?
 - Are there indications of additional problems with ²H data?



Comparison of ²H angular scattering distributions









Limited ²H data: HST-004 & -020 ICSBEP benchmarks

- High leakage (~40%); HEU; homogeneous uranyl fluoride solutions in D₂O; large experimental uncertainties for k; thermal fission fraction 38-97%
- HST-004
 - 6 expts. with inner sphere of HEU uranyl fluoride in D_2O reflected by outer annulus of D_2O
 - LANL believes HST-004 results are more reliable than HST-020
- HST-020
 - 5 expts. with unreflected cylinders of HEU uranyl fluoride in D_2O
 - have reactivity biases of approximately
 -4 mk, due to the <u>calculated</u> omission of room return



CRL HST MCNP5 results

- *k*_{Calc.} *k*_{Meas.} shows a large spread of ~37 mk & rising trend with calculated leakage
- Using ENDF/B-IV [1002.60c] increases k by ~9.7 mk



CRL HST MCNP5 results

• Δk [1002.60c – 1002.66c] depends on change in calculated leakage



CRL HST results: dependence on ²H-to-²³⁵U atom ratio

MCNP5: k_{calc}. -k_{meas}.vs ²H-to-²³⁵U atom ratio [excluding reflector]: 1002.66c & ENDF/B-VI.8



Comparison of HST & ZED-2 critical experiments

HST & ZED-2 experiments are complementary

Characteristic	*	
Neutron leakage	Low (~11% from D ₂ O moderator surface)	High (~40%)
Enrichment	Natural Uranium (NU; 0.7% ²³⁵ U)	HEU (> 90% ²³⁵ U)
Physical form	Heterogeneous rod lattices	Homogeneous solutions

- HST experiments feature simple geometry & materials
- ZED-2 results potentially more directly relevant to existing reactor applications

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ZED-2 Reactor at Chalk River Laboratories

- Tank-type critical facility, 3.3 m in diameter & depth
 - D₂O moderator height increased to bring critical; some fuel protrudes above
 - runs at a few Watts; first criticality 1960
- Flexible facility that allows testing of a variety of fuels, different pitches (hex. or square), different coolants: D₂O, H₂O, air (voided)
- D₂O moderated; graphite radial & bottom reflector
- Typical lattice arrangement is 31-cm hexagonal pitch, with 55 channels, each containing 5 fuel bundles
- Mainly used for CANDU reactor physics validation experiments, e.g., coolant void reactivity (CVR)
- Hope to include some results in IRPhEP (AECL/Canada now involved)





CANDU fuel lattice cell

Figure 1. Cross section of a 37-element CANDU fuel lattice cell

ZED-2 MCNP5 hex. reference-lattice simulations

In order of increasing ²³⁸U capture:

- 1. 91 ZEEP U-metal rods; lattice pitch = 22.86 cm
- 2. 91 ZEEP U-metal rods; lattice pitch = 21.59 cm
- 3. 91 ZEEP U-metal rods; lattice pitch = 20.00 cm
- 55 <u>air-cooled</u> (i.e., voided) 28-element UO₂ assemblies (i.e., 5 Pickering-type bundles each) plus 30 ZEEP U-metal rods; lattice pitch = 31.00 cm
- 5. 55 <u>air-cooled</u> 28-element UO₂ assemblies plus 30 19element U-metal assemblies; lattice pitch = 31.00 cm
- 6. 55 <u>heavy-water-cooled</u> 28-element UO₂ assemblies plus 30 ZEEP U-metal rods; lattice pitch = 31.00 cm
- 55 <u>heavy-water-cooled</u> 28-element UO₂ assemblies plus 30 19-element U-metal assemblies; lattice pitch = 31.00 cm

Critical heights ranged from 155.8 to 213.3 cm (14% to 9% calculated leakage from D_2O surfaces)



ZEEP (1945)



19-el. U-metal



28- ROD U02

28-el. UO₂

Dependence of MCNP5 ZED-2 k_{eff} on nuclear data

- 4 data sets:
 - Deuterium from ENDF/B-VI.8 (1002.66c) & ENDF/B-VI.4 (1002.64c)
 - Uranium from ENDF/B-VI.8 & Pre-ENDF/B-VII



- Decreasing trend with increasing ²³⁸U captures
- Small reactivity impact (<1 mk) due to different ²H data; CVR bias worse with 1002.64c
- Behaviour of D₂O-cooled cases differs from air-cooled cases
- Main impact is a gain of ~4 mk due to pre-ENDF/B-VII ²³⁸U,²³⁵U

ZED-2 MCNP5 simulations: IAEA-S(α , β) for D₂O

- Small increase in k (<1 mk)
- CVR bias slightly worse (~0.2mk)



ZED-2 MCNP5 *k*_{eff} also increases with neutron leakage

- Neutron leakage from D₂O moderator is predominantly thermal (~87% <0.625 eV)
- Small net in-leakage of fast neutrons (>0.1 MeV) at top moderator surface due to fissions in exposed fuel above
- Axial leakage ~1/(critical height)²



MCNP5 CANDU-SCWR (Supercritical Water Reactor) benchmark

(Proc. Int. Workshop on Nucl. Data Needs for Generation-IV Nucl. Energy Systems, Antwerp, 2005)

- 2005}
 21-cm square lattice pitch; 4.25 wt% ²³⁵U
 - Uniform lattice of mid-life (22.3 MWd/kgU) fuel [composition from WIMS-AECL] & "mixed" lattice (0.2 & 44.2 MWd/kgU)
 - H_2O cooled [inlet density = 0.44 g/cm³] & voided configurations
 - Nuclear data at 294 or 300 K
 - Reactivity sensitivity to ²H data calculated as a function of axial-neutronleakage (i.e., finite core length with a vacuum boundary)

2-by-2 MCNP5 model



Sensitivity of CANDU-SCWR numerical benchmark to ²H data

- Δk -[1002.64c 1002.66c] increases with axial leakage & depends on coolant state
- Essentially a 1:1 correspondence between Δk & the change in calculated leakage



~HST-004,020 leakage

Simplified ²H benchmark to highlight reactivity impact of angular scattering

• ²H-(at D₂O # density)reflected 8.4-cm radius U-metal sphere; no $S(\alpha,\beta)$



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Recent ZED-2 results

- <u>Slightly</u> Enriched <u>Uranium</u> (SEU): 0.95 wt% ²³⁵U
- 43-element CANFLEX fuel geometry (greater subdivision)
- Square vs. hexagonal lattices; pitch = 20 to 24.5 cm
- H₂O & air 'coolant'



Recent ZED-2 H₂O CVR results for SEU CANFLEX fuel

- MCNP5 H_2O CVR bias increases to ~+8 mk with square lattice pitch
- Hexagonal-pitch data plotted at equivalent square lattice pitch
- MCNP5 shows different hex & sq. results, but expt. critical bucklings the same CANFLEX SEU in ZED-2



Dependence of ZED-2 MCNP5 k_{eff} on axial leakage

- New SEU ZED-2 H₂O CVR measurements involve relatively large changes in axial leakage
- MCNP5 k_{eff} increases with axial leakage, as before



Summary/Conclusions

- Big difference in reactivity sensitivity of HST (~10 mk) & ZED-2 (<1 mk) NU results to ENDF/B-VI.5 & VI.4 ²H data
- ZED-2 results show lower D₂O CVR bias (by ~0.6 mk) with newer ENDF/B-VI.5 ²H data relative to ENDF/B-VI.4
- <u>But</u>, still a significant rising trend of (k_{eff} –1) with leakage for both ZED-2 & HST criticals
- Numerical benchmarks with different ²H data show
 - <u>CANDU-SCWR</u>: reactivity sensitivity depends on leakage & presence/absence of low-density H₂O coolant
 - <u>²H-reflected U-metal sphere</u>: reactivity sensitivity depends on
 ²³⁵U enrichment (²³⁵U # density & offset due to ²³⁸U captures)
 & reflector thickness (reduced leakage)
- MCNP5 results for new SEU CANFLEX ZED-2 measurements show a large (up to ~+8 mk) H₂O CVR bias that depends on lattice pitch & arrangement (square vs. hexagonal)
- New ²H evaluation &/or angular scattering measurements needed?

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Acknowledgments

- <u>Russ Mosteller</u> (LANL) provided pre-ENDF/B-VII for U & 1002.64c data in ACE format
- <u>Andre Trkov</u> (IAEA) provided new $S(\alpha,\beta)$ for D_2O & H_2O
- <u>Radoslav Zajac</u> (BNL-NNDC) provided pre-ENDF/B-VIIbeta1 1002.00c data
- CRL ZED-2 experiment & analysis crew, particularly, Mike Zeller, Benoit Arsenault & Bruce Wilkin



<u>Reminder</u>

- PHYSOR-2006 is 10 months away: Sept. 10-14, Vancouver, BC, Canada
- Key dates:
 - Jan. 7, 2006, 1000-word reduced-length paper due
 - June 15, 2006, full-length papers due
- See http://www.cns-snc.ca/physor2006
- Technical Program includes:
 - <u>Plenary</u>: Advances in Nuclear Data Libraries
 - Covariance Data Generation for Nuclear Applications (Luiz Leal, ORNL)
 - Nuclear Safety Validation & Performance of ENDF/B-VII (Richard McKnight, ANL)
 - Nuclear Data (Mike Dunn, ORNL)
 - The International Reactor Physics Experiment Evaluation Project (IRPhEP) (J. Blair Briggs, INL; Ibrahim Attieh, AECL)



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Important Dates:

January 7, 2006 Electronic Submission of 1,000-Word Reduced-Length Paper February 17, 2006 Notification of Acceptance to Authors June 15, 2006 Deadline for Submission of Final Full-Length Paper July 31, 2006 Early Registration Deadline

Instructions for Reduced-Length Papers: – Describe work that is NEW, SIGNIFICANT, and RELEVANT to the nuclear industry – Use ~1,000 words, including Figures and Tables – Electronic submission via: http://www.cns-snc.ca/physor2006

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