

$^{14}\text{C}(^{18}\text{O},2\text{n}\gamma)$  **2010St13**

| Type            | Author                        | History | Citation         | Literature Cutoff Date |
|-----------------|-------------------------------|---------|------------------|------------------------|
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90% enriched  $^{14}\text{C}$  target bombarded with a 37 MeV  $^{18}\text{O}$  beam at ANL Tandem Linear Accelerator System; Fragment Mass Analyzer, parallel-plate gridded avalanche counter (PGAC); Gammasphere array, consists of 101 Compton-suppressed HPGe detectors, Measured:  $E\gamma$ ,  $I\gamma$ ,  $\gamma(\theta)$ , DCO,  $\gamma$ - $\gamma$  coin, time-of-flight parameter, deduced level scheme. Shell model calculations were performed.

 $^{30}\text{Si}$  Levels

| E(level) <sup>†</sup> | $J^\pi$ <sup>‡</sup>           | Comments                                                                                                                                    |
|-----------------------|--------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------|
| 0                     | 0 <sup>+</sup>                 | E(level): from Adopted Level.                                                                                                               |
| 2234.01 10            | 2 <sup>+</sup>                 |                                                                                                                                             |
| 3496.84 18            | 2 <sup>+</sup>                 |                                                                                                                                             |
| 4828.39 16            | 3 <sup>+</sup>                 |                                                                                                                                             |
| 5228.62 18            | 3 <sup>+</sup>                 |                                                                                                                                             |
| 5277.43 13            | 4 <sup>+</sup>                 |                                                                                                                                             |
| 5484.92 15            | 3 <sup>-</sup>                 |                                                                                                                                             |
| 5949.00 17            | 4 <sup>+</sup>                 |                                                                                                                                             |
| 6500.87 16            | 4 <sup>-</sup>                 |                                                                                                                                             |
| 6996.98 15            | 5 <sup>+</sup>                 |                                                                                                                                             |
| 7041.24 15            | 5 <sup>-</sup>                 |                                                                                                                                             |
| 7220.7 4              | 4 <sup>+</sup>                 |                                                                                                                                             |
| 8191.5 4              | 5 <sup>-</sup>                 |                                                                                                                                             |
| 8956.9 8              | (5 <sup>-</sup> )              |                                                                                                                                             |
| 9104.78 17            | 6 <sup>-</sup>                 |                                                                                                                                             |
| 9365.3 4              | 6 <sup>+</sup>                 |                                                                                                                                             |
| 9771.3 5              | 6 <sup>-</sup>                 |                                                                                                                                             |
| 10552.5 3             | 6 <sup>-</sup>                 |                                                                                                                                             |
| 10672.9 12            | (6)                            |                                                                                                                                             |
| 10717.35 20           | 7 <sup>-</sup>                 |                                                                                                                                             |
| 11081.5 22            | (6,7) <sup>-</sup>             | $J^\pi$ : 2010St13 propose $J^\pi$ to be 6 <sup>-</sup> or 7 <sup>-</sup> based on $\gamma$ -ray feeding. 4040 $\gamma$ to 5 <sup>-</sup> . |
| 11537.0 9             | 7 <sup>-</sup>                 |                                                                                                                                             |
| 12391.8 24            |                                |                                                                                                                                             |
| 12508 3               |                                |                                                                                                                                             |
| 12712.9 15            |                                |                                                                                                                                             |
| 12830.04 25           | (8 <sup>-</sup> ) <sup>#</sup> |                                                                                                                                             |
| 13200.9 5             | (8 <sup>-</sup> ) <sup>#</sup> |                                                                                                                                             |
| 15189.4 5             | (9 <sup>-</sup> ) <sup>#</sup> |                                                                                                                                             |
| 15526.9 14            | (9 <sup>-</sup> ) <sup>#</sup> |                                                                                                                                             |

<sup>†</sup> From a least squares fit to the  $\gamma$ -ray energies. In least squares fit, the uncertainty for the 1261.8 $\gamma$ , 539.5 $\gamma$  and 3676.7 $\gamma$ , depopulating the levels 3496, 7041 and 10717 keV, respectively, increased for each by 0.2 keV, i.e. from 0.3, 0.3 and 0.2 to 0.5, 0.5 and 0.4, respectively, to bring the Chi-square value below the critical limit.

<sup>‡</sup> As given in 2010St13, except otherwise noted. 2010St13 note that the  $\gamma(\theta)$  and  $R_{\text{DCO}}$  measurements support the adopted  $J^\pi$ .

<sup>#</sup> Assigned by 2010St13, based on  $\gamma$ -feeding sequence to the lower levels.

$^{14}\text{C}(^{18}\text{O}, 2n\gamma)$  **2010St13 (continued)** $\gamma(^{30}\text{Si})$ 

| $E_\gamma$ | $I_\gamma^\dagger$ | $E_i(\text{level})$ | $J_i^\pi$         | $E_f$    | $J_f^\pi$         | $R_{\text{DCO}}$ | Comments                               |
|------------|--------------------|---------------------|-------------------|----------|-------------------|------------------|----------------------------------------|
| 400.0 2    | 0.42 3             | 5228.62             | 3 <sup>+</sup>    | 4828.39  | 3 <sup>+</sup>    |                  | $A_2=0.30$ 10                          |
| 539.5 3    | 13.9 4             | 7041.24             | 5 <sup>-</sup>    | 6500.87  | 4 <sup>-</sup>    | 0.7 1            | $A_2=-0.21$ 2; DCO=0.7 1               |
| 551.9 11   | 0.12 2             | 6500.87             | 4 <sup>-</sup>    | 5949.00  | 4 <sup>+</sup>    |                  |                                        |
| 914.0 13   | 0.15 6             | 9104.78             | 6 <sup>-</sup>    | 8191.5   | 5 <sup>-</sup>    |                  |                                        |
| 970.3 7    | 0.21 5             | 8191.5              | 5 <sup>-</sup>    | 7220.7   | 4 <sup>+</sup>    |                  |                                        |
| 1016.0 1   | 1.4 1              | 6500.87             | 4 <sup>-</sup>    | 5484.92  | 3 <sup>-</sup>    |                  |                                        |
| 1048.2 2   | 1.7 1              | 6996.98             | 5 <sup>+</sup>    | 5949.00  | 4 <sup>+</sup>    | 0.5 2            | DCO=0.5 2                              |
| 1092.1 2   | 14.3 5             | 7041.24             | 5 <sup>-</sup>    | 5949.00  | 4 <sup>+</sup>    | 0.5 1            | $A_2=-0.20$ 2; DCO=0.5 1               |
| 1261.8 3   | 13.8 5             | 3496.84             | 2 <sup>+</sup>    | 2234.01  | 2 <sup>+</sup>    | 1.2 2            | $A_2=0.36$ 2; $A_4=-0.10$ 3; DCO=1.2 2 |
| 1271.9 2   | 10.8 4             | 6500.87             | 4 <sup>-</sup>    | 5228.62  | 3 <sup>+</sup>    | 0.7 1            | $A_2=-0.22$ 2; DCO=0.7 1               |
| 1330.2 7   | 0.47 7             | 4828.39             | 3 <sup>+</sup>    | 3496.84  | 2 <sup>+</sup>    |                  | $A_2=0.53$ 9                           |
| 1353.2 13  | 0.44 4             | 10717.35            | 7 <sup>-</sup>    | 9365.3   | 6 <sup>+</sup>    |                  |                                        |
| 1447.9 5   | 0.59 5             | 10552.5             | 6 <sup>-</sup>    | 9104.78  | 6 <sup>-</sup>    |                  |                                        |
| 1556.3 1   | 4.3 2              | 7041.24             | 5 <sup>-</sup>    | 5484.92  | 3 <sup>-</sup>    |                  | $A_2=0.32$ 3; $A_4=-0.14$ 4            |
| 1578.7 6   | 0.74 5             | 9771.3              | 6 <sup>-</sup>    | 8191.5   | 5 <sup>-</sup>    |                  |                                        |
| 1612.5 1   | 6.1 2              | 10717.35            | 7 <sup>-</sup>    | 9104.78  | 6 <sup>-</sup>    | 0.8 2            | $A_2=0.10$ 3; DCO=0.8 2                |
| 1672.4 1   | 6.6 2              | 6500.87             | 4 <sup>-</sup>    | 4828.39  | 3 <sup>+</sup>    | 0.7 1            | $A_2=-0.25$ 3; DCO=0.7 1               |
| 1690.2 5   | 0.96 10            | 8191.5              | 5 <sup>-</sup>    | 6500.87  | 4 <sup>-</sup>    |                  |                                        |
| 1719.4 1   | 7.5 3              | 6996.98             | 5 <sup>+</sup>    | 5277.43  | 4 <sup>+</sup>    | 1.1 2            | $A_2=0.33$ 3; DCO=1.1 2                |
| 1731.5 2   | 11.1 4             | 5228.62             | 3 <sup>+</sup>    | 3496.84  | 2 <sup>+</sup>    | 0.7 2            | $A_2=-0.19$ 2; DCO=0.7 2               |
| 1763.8 1   | 6.6 3              | 7041.24             | 5 <sup>-</sup>    | 5277.43  | 4 <sup>+</sup>    | 0.4 1            | $A_2=-0.11$ 2; DCO=0.4 1               |
| 1767.7 10  | 0.56 11            | 6996.98             | 5 <sup>+</sup>    | 5228.62  | 3 <sup>+</sup>    |                  |                                        |
| 1915.6 7   | 0.73 6             | 8956.9              | (5 <sup>-</sup> ) | 7041.24  | 5 <sup>-</sup>    |                  |                                        |
| 1943.0 11  | 0.54 14            | 7220.7              | 4 <sup>+</sup>    | 5277.43  | 4 <sup>+</sup>    |                  |                                        |
| 1988.2 2   | 4.4 2              | 5484.92             | 3 <sup>-</sup>    | 3496.84  | 2 <sup>+</sup>    |                  |                                        |
| 1991.5 4   | 0.34 8             | 7220.7              | 4 <sup>+</sup>    | 5228.62  | 3 <sup>+</sup>    |                  |                                        |
| 2063.4 1   | 17.0 6             | 9104.78             | 6 <sup>-</sup>    | 7041.24  | 5 <sup>-</sup>    | 1.2 2            | $A_2=0.34$ 2; DCO=1.2 2                |
| 2112.7 2   | 2.7 1              | 12830.04            | (8 <sup>-</sup> ) | 10717.35 | 7 <sup>-</sup>    |                  |                                        |
| 2168.9 3   | 3.0 2              | 6996.98             | 5 <sup>+</sup>    | 4828.39  | 3 <sup>+</sup>    |                  | $A_2>0$                                |
| 2233.9 1   | 100 4              | 2234.01             | 2 <sup>+</sup>    | 0        | 0 <sup>+</sup>    |                  | $A_2=0.23$ 1; $A_4=-0.10$ 2            |
| 2242.7 18  | 0.58 17            | 8191.5              | 5 <sup>-</sup>    | 5949.00  | 4 <sup>+</sup>    |                  |                                        |
| 2358.9 6   | 1.0 1              | 15189.4             | (9 <sup>-</sup> ) | 12830.04 | (8 <sup>-</sup> ) |                  |                                        |
| 2368.0 4   | 2.9 2              | 9365.3              | 6 <sup>+</sup>    | 6996.98  | 5 <sup>+</sup>    |                  |                                        |
| 2431.8 11  | 0.53 9             | 11537.0             | 7 <sup>-</sup>    | 9104.78  | 6 <sup>-</sup>    |                  |                                        |
| 2452.6 13  | 0.61 9             | 5949.00             | 4 <sup>+</sup>    | 3496.84  | 2 <sup>+</sup>    |                  |                                        |
| 2483.4 4   | 1.5 1              | 13200.9             | (8 <sup>-</sup> ) | 10717.35 | 7 <sup>-</sup>    |                  |                                        |
| 2594.2 2   | 14.5 6             | 4828.39             | 3 <sup>+</sup>    | 2234.01  | 2 <sup>+</sup>    | 1.0 2            | $A_2=0.38$ 3; DCO=1.0 2                |
| 2696.7 13  | 0.55 10            | 15526.9             | (9 <sup>-</sup> ) | 12830.04 | (8 <sup>-</sup> ) |                  |                                        |
| 2707.5 16  | 0.86 18            | 8191.5              | 5 <sup>-</sup>    | 5484.92  | 3 <sup>-</sup>    |                  |                                        |
| 2730.5 8   | 1.1 1              | 9771.3              | 6 <sup>-</sup>    | 7041.24  | 5 <sup>-</sup>    |                  |                                        |
| 2776.1 16  | 0.82 16            | 9771.3              | 6 <sup>-</sup>    | 6996.98  | 5 <sup>+</sup>    |                  | $A_2<0$                                |
| 2994.5 6   | 1.4 1              | 5228.62             | 3 <sup>+</sup>    | 2234.01  | 2 <sup>+</sup>    |                  | $A_2<0$                                |
| 3043.2 1   | 29.5 11            | 5277.43             | 4 <sup>+</sup>    | 2234.01  | 2 <sup>+</sup>    | 1.2 2            | $A_2=0.34$ 2; $A_4=-0.13$ 2; DCO=1.2 2 |
| 3251.4 4   | 4.9 3              | 5484.92             | 3 <sup>-</sup>    | 2234.01  | 2 <sup>+</sup>    | 0.7 2            | $A_2=-0.21$ 5; DCO=0.7 2               |
| 3271.6 10  | 1.6 2              | 9771.3              | 6 <sup>-</sup>    | 6500.87  | 4 <sup>-</sup>    |                  |                                        |
| 3286.8 24  | 0.47 12            | 12391.8             |                   | 9104.78  | 6 <sup>-</sup>    |                  |                                        |
| 3345.7 13  | 1.5 2              | 11537.0             | 7 <sup>-</sup>    | 8191.5   | 5 <sup>-</sup>    |                  |                                        |
| 3403 3     | 0.38 12            | 12508               |                   | 9104.78  | 6 <sup>-</sup>    |                  |                                        |
| 3418.8 14  | 1.7 3              | 9365.3              | 6 <sup>+</sup>    | 5949.00  | 4 <sup>+</sup>    |                  | $A_2>0$                                |
| 3497.0 4   | 10.0 5             | 3496.84             | 2 <sup>+</sup>    | 0        | 0 <sup>+</sup>    |                  | $A_2=0.36$ 4; $A_4=-0.12$ 5            |
| 3511.0 3   | 0.51 16            | 10552.5             | 6 <sup>-</sup>    | 7041.24  | 5 <sup>-</sup>    |                  |                                        |
| 3607.9 15  | 0.84 13            | 12712.9             |                   | 9104.78  | 6 <sup>-</sup>    |                  | $A_2>0$                                |
| 3631.4 12  | 1.2 2              | 10672.9             | (6)               | 7041.24  | 5 <sup>-</sup>    |                  |                                        |
| 3676.7 2   | 6.4 3              | 10717.35            | 7 <sup>-</sup>    | 7041.24  | 5 <sup>-</sup>    | 1.7 6            | $A_2=0.23$ 3; $A_4=-0.18$ 4; DCO=1.7 6 |
| 3714.9 2   | 20.3 9             | 5949.00             | 4 <sup>+</sup>    | 2234.01  | 2 <sup>+</sup>    | 1.5 3            | $A_2=0.35$ 2; $A_4=-0.15$ 3; DCO=1.5 3 |

Continued on next page (footnotes at end of table)

| <sup>14</sup> C( <sup>18</sup> O,2n $\gamma$ )    2010St13 (continued) |                                         |                                |                             |                         |                             |                                                  |
|------------------------------------------------------------------------|-----------------------------------------|--------------------------------|-----------------------------|-------------------------|-----------------------------|--------------------------------------------------|
| $\gamma(^{30}\text{Si})$ (continued)                                   |                                         |                                |                             |                         |                             |                                                  |
| <u>E<math>\gamma</math></u>                                            | <u>I<math>\gamma</math><sup>†</sup></u> | <u>E<math>_i</math>(level)</u> | <u>J<math>^\pi_i</math></u> | <u>E<math>_f</math></u> | <u>J<math>^\pi_f</math></u> | <u>Comments</u>                                  |
| 3724.7 3                                                               | 1.0 2                                   | 12830.04                       | (8 <sup>-</sup> )           | 9104.78                 | 6 <sup>-</sup>              |                                                  |
| 3725.5 10                                                              | 0.48 12                                 | 7220.7                         | 4 <sup>+</sup>              | 3496.84                 | 2 <sup>+</sup>              |                                                  |
| 4040.0 22                                                              | 0.68 17                                 | 11081.5                        | (6,7) <sup>-</sup>          | 7041.24                 | 5 <sup>-</sup>              |                                                  |
| 4088.7 20                                                              | 2.1 3                                   | 9365.3                         | 6 <sup>+</sup>              | 5277.43                 | 4 <sup>+</sup>              | A <sub>2</sub> =0.51 8; A <sub>4</sub> =-0.16 10 |
| 4472.1 6                                                               | 1.5 1                                   | 15189.4                        | (9 <sup>-</sup> )           | 10717.35                | 7 <sup>-</sup>              | A <sub>2</sub> >0                                |

<sup>†</sup> Relative to I $\gamma$ (2233.9)=100.

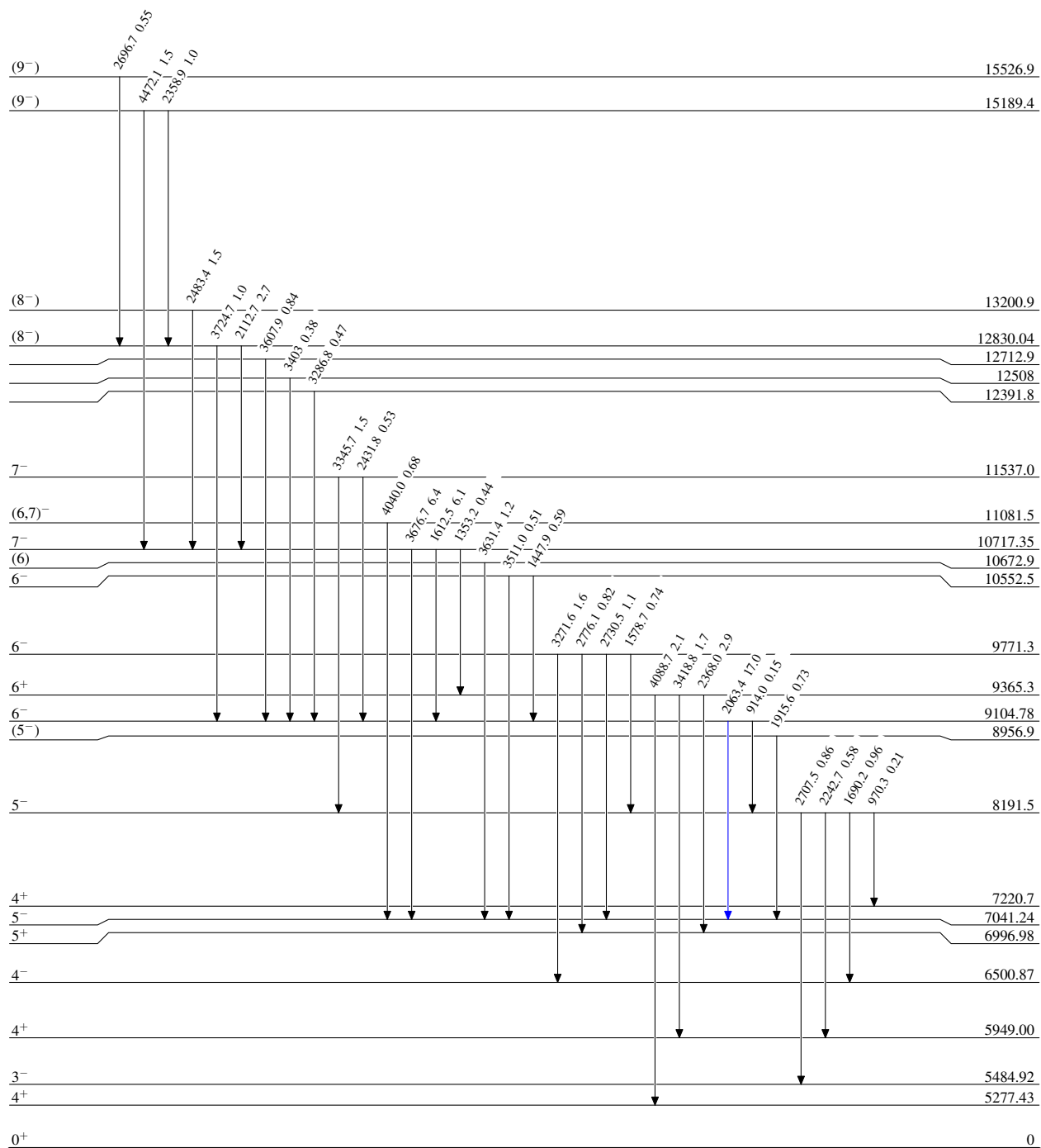
$^{14}\text{C}(^{18}\text{O},2n\gamma)$  2010St13

## Level Scheme

Intensities: Relative  $I_\gamma$ 

## Legend

- $\longrightarrow$   $I_\gamma < 2\% \times I_\gamma^{\max}$   
 $\longrightarrow$   $I_\gamma < 10\% \times I_\gamma^{\max}$   
 $\longrightarrow$   $I_\gamma > 10\% \times I_\gamma^{\max}$



<sup>14</sup>C(18O,2nγ) 2010St13

Level Scheme (continued)

Intensities: Relative I<sub>γ</sub>

Legend

- I<sub>γ</sub> < 2% × I<sub>γ</sub><sup>max</sup>
- I<sub>γ</sub> < 10% × I<sub>γ</sub><sup>max</sup>
- I<sub>γ</sub> > 10% × I<sub>γ</sub><sup>max</sup>

