

$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Type	Author	History Citation	Literature Cutoff Date
Full Evaluation	M. S. Basunia	NDS 110, 999 (2009)	1-Nov-2008

Target: Enriched ^{173}Yb ; Projectile: ^{18}O , E=78 and 85 MeV; Detector: GEMINI γ -ray detector array consists of 13 HPGe with BGO anti Compton shield; Measured: $E\gamma$, $I\gamma$, x- γ -t and $\gamma\gamma$ -t coin, DCO ratios.

 ^{187}Pt Levels

E(level) [†]	J π [‡]	T _{1/2}	E(level) [†]	J π [‡]	E(level) [†]	J π [‡]
0.0 ^c	3/2 ⁻		1839.8 ^b 8	23/2 ⁻	3039.1 ^f 10	33/2
9.3 7	3/2 ⁻		1869.6 ^c 8	23/2 ⁻	3068.5 ^h 10	35/2 ⁻
25.6 ^d 5	5/2 ⁻		1896.3 ^b 9	25/2 ⁻	3075.7 ^h 11	33/2
57.2 ^a 11	7/2 ⁻		1987.7 ^e 11	25/2 ⁻	3116.3 9	
75.0 7	3/2 ⁻		2006.5 ^a 10	23/2 ⁻	3211.3 ^g 9	33/2
174.4 ^{&} 8	11/2 ⁺	311 ⁱ μs 15	2070.8 ^d 8	25/2 ⁻	3287.1 ^a 12	33/2 ⁻
190.6 5	3/2 ⁻		2091.5 ^{&} 8	27/2 ⁺	3297.4 ^b 11	35/2 ⁻
203.2 [@] 8	13/2 ⁺		2120.4 ^h 9		3332.5 ^{&} 9	35/2 ⁺
204.3 ^c 5	7/2 ⁻		2142.8 [@] 8	29/2 ⁺	3414.7 ^h 12	35/2
225.7 ^a 11	9/2 ⁻		2230.8 ^b 9	27/2 ⁻	3488.5 [@] 9	37/2 ⁺
305.9 ^d 5	9/2 ⁻		2263.6 ^a 11	25/2 ⁻	3506.4 10	
430.7 ^a 10	11/2 ⁻		2322.7 9	25/2 ⁻	3532.1 ^g 10	35/2
465.1 ^{&} 8	15/2 ⁺		2393.4 ^c 9	27/2 ⁻	3552.3 ^b 11	37/2 ⁻
500.3 ^c 5	11/2 ⁻		2424.8 ^g 9	27/2	3573.9 ^e 11	
505.0 [@] 8	17/2 ⁺		2433.6 ^b 9	29/2 ⁻	3574.9 ^f 9	35/2 ⁺
650.9 ^a 10	13/2 ⁻		2482.4 ^d 9	29/2 ⁻	3598.4 10	37/2 ⁺
694.5 ^d 6	13/2 ⁻		2492.9 ^a 11	27/2 ⁻	3606.7 ^d 12	37/2 ⁻
886.8 ^c 5	15/2 ⁻		2518.5 ^e 12	29/2	3613.2 ^g 10	35/2
894.4 ^a 10	15/2 ⁻		2518.9 ^f 9	29/2	3617.2 ^h 11	39/2 ⁻
902.8 ^{&} 8	19/2 ⁺		2608.5 ^h 10	31/2 ⁻	3720.7 ^h 12	37/2
928.1 ^e 9	17/2		2626.4 ^g 9	29/2	3784.5 ^h 13	37/2
942.8 [@] 8	21/2 ⁺		2632.5 ^h 10	31/2 ⁻	3839.0 ^f 11	
1153.1 ^a 9	17/2 ⁻		2654.0 ^e 12	29/2	3847.7 ^{&} 10	(39/2 ⁺)
1161.1 ^d 6	17/2 ⁻		2744.5 ^{&} 9	31/2 ⁺	3889.0 ^b 12	39/2 ⁻
1212.5 ^g 9	19/2		2745.1 ^a 11	29/2 ⁻	3976.5 ^f 10	
1349.8 ^c 6	19/2 ⁻		2781.6 ^h 9	31/2 ⁻	3992.2 ^g 10	37/2
1409.1 8	17/2 ⁻		2792.9 ^b 9	31/2 ⁻	4045.3 [@] 11	41/2 ⁺
1418.0 ^e 9	21/2		2852.0 12		4075.9 ^h 13	39/2
1429.9 ^a 10	19/2 ⁻		2852.4 [@] 9	33/2 ⁺	4249.8 ^b 12	41/2 ⁻
1442.7 7	21/2 ⁻		2871.1 ^f 9	31/2 ⁺	4256.0 ^g 11	
1452.9 ^{&} 8	23/2 ⁺		2900.6 ^g 9	31/2	4307.3 ^d 13	41/2 ⁻
1496.2 [@] 8	25/2 ⁺		2915.0 ^c 11	31/2 ⁻	4318.2 11	41/2 ⁺
1616.1 9			2942.7 ^b 10	33/2 ⁻	4554.5 ^b 13	43/2 ⁻
1657.8 ^b 8	21/2 ⁻ #		2996.2 ^d 11	33/2 ⁻	4723.3 [@] 12	45/2 ⁺
1691.7 ^d 7	21/2 ⁻		3013.0 ^a 12	31/2 ⁻	4986.3 ^b 13	45/2 ⁻
1716.9 ^a 10	21/2 ⁻		3017.4 ^g 10	31/2	5274.0 ^b 14	47/2 ⁻
1789.8 ^g 9	23/2		3038.8 ^e 10	33/2	5510.3 [@] 13	49/2 ⁺

[†] From a least-squares adjustment to the γ -ray energies.

[‡] Assigned by 2007Zh09 from γ -ray multiplicities and previously known J π of the lower levels.

Continued on next page (footnotes at end of table)

¹⁷³Yb(¹⁸O,4nγ) **2007Zh09 (continued)**

¹⁸⁷Pt Levels (continued)

The DCO ratio=0.96 9 of the 715γ, feeding the 21/2⁺ state, indicates that the transition would be a stretched Q transition or a dipole transition that would connect levels with same spin values. Considering the observation of parallel 755.2γ feeding to the 19/2⁺ state, J^π=21/2⁻ is assigned for this level (2007Zh09).

@ Band 1:configuration=ν I_{13/2}: α=1/2⁺.

& Band 1:configuration=ν I_{13/2}: α=1/2⁻.

^a Band 2:configuration=ν 7/2⁻[503].

^b Band 3:configuration=ν i_{13/2}² ν J(p_{3/2} or f_{5/2}).

^c Band 4:configuration=ν 3/2⁻[512].

^d Band 5:configuration=ν 1/2⁻[521].

^e Band Structure 1.

^f Band Structure 2.

^g Band Structure 3.

^h Band Structure 4.

ⁱ From Adopted Levels.

γ(¹⁸⁷Pt)

<u>E_γ[†]</u>	<u>I_γ[†]</u>	<u>E_i(level)</u>	<u>J_i^π</u>	<u>E_f</u>	<u>J_f^π</u>	<u>Mult.[#]</u>	<u>DCO ratio[‡]</u>	<u>Comments</u>
(56.6)		1896.3	25/2 ⁻	1839.8	23/2 ⁻			
115.6 5	4 1	190.6	3/2 ⁻	75.0	3/2 ⁻			
164.9 5	5 2	190.6	3/2 ⁻	25.6	5/2 ⁻			RADO=0.56 17.
168.4 5	81 24	225.7	9/2 ⁻	57.2	7/2 ⁻	D	0.65 9	RADO=0.56 3.
178.8 5	19 6	204.3	7/2 ⁻	25.6	5/2 ⁻	D	0.67 10	RADO=0.61 7.
181.3 5	18 5	190.6	3/2 ⁻	9.3	3/2 ⁻			
182.0 2	142 21	1839.8	23/2 ⁻	1657.8	21/2 ⁻		0.84 6	RADO=0.87 4.
190.7 5	26 8	190.6	3/2 ⁻	0.0	3/2 ⁻		0.96 16	RADO=1.4 7.
194.5 5	13 4	500.3	11/2 ⁻	305.9	9/2 ⁻	D	0.69 21	RADO=0.70 13.
201.6 5	61 18	2626.4	29/2	2424.8	27/2		1.49 20	RADO=1.62 12.
202.6 5	14 4	2433.6	29/2 ⁻	2230.8	27/2 ⁻			RADO=1.00 15.
204.2 5	42 13	204.3	7/2 ⁻	0.0	3/2 ⁻	Q	1.14 12	RADO=1.31 9.
205.0 5	85 25	430.7	11/2 ⁻	225.7	9/2 ⁻	D	0.57 7	I _γ : I _γ (205.0):I _γ (373.5)=100:66(5) from Branching ratio. RADO=0.59 4.
207.0 5	28 8	1616.1		1409.1	17/2 ⁻			RADO=1.1 4.
220.1 5	72 22	650.9	13/2 ⁻	430.7	11/2 ⁻	D	0.61 6	I _γ : I _γ (220.1):I _γ (425.1)=100:125(9) from Branching ratio. RADO=0.61 7.
223.7 5	31 9	1839.8	23/2 ⁻	1616.1				
224.0 5	42 13	2120.4		1896.3	25/2 ⁻		0.75 11	RADO=0.90 13.
225.8 5	12 4	2744.5	31/2 ⁺	2518.9	29/2			
229.2 5	3 1	2492.9	27/2 ⁻	2263.6	25/2 ⁻			I _γ : I _γ (229.2):I _γ (486.6)=100:267(45) from Branching ratio. RADO=0.85 18.
238.6 5	82 25	1896.3	25/2 ⁻	1657.8	21/2 ⁻	Q	1.13 13	RADO=1.30 11.
243.5 5	41 12	894.4	15/2 ⁻	650.9	13/2 ⁻	D	0.66 10	I _γ : I _γ (243.5):I _γ (463.8)=100:249(20) from Branching ratio. RADO=0.76 5.
248.8 5	54 16	1657.8	21/2 ⁻	1409.1	17/2 ⁻	Q	1.16 23	RADO=1.16 18.
252.2 5	4 1	2745.1	29/2 ⁻	2492.9	27/2 ⁻			
257.0 5	9 3	2263.6	25/2 ⁻	2006.5	23/2 ⁻	D	0.71 23	I _γ : I _γ (257.0):I _γ (546.6)=100:400(44) from Branching ratio. RADO=0.59 11.
258.7 5	37 11	1153.1	17/2 ⁻	894.4	15/2 ⁻	D	0.43 13	I _γ : I _γ (258.7):I _γ (502.2)=100:276(42) from

Continued on next page (footnotes at end of table)

$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09 (continued) $\gamma(^{187}\text{Pt})$ (continued)

E_γ †	I_γ †	$E_i(\text{level})$	J_i^π	E_f	J_f^π	Mult. #	DCO ratio‡	Comments
								Branching ratio. $R_{\text{ADO}}=0.81$ 11. $R_{\text{ADO}}=0.52$ 15.
262.0 1	381 19	465.1	15/2 ⁺	203.2	13/2 ⁺	D	0.50 4	
263.8 5	45 13	4256.0		3992.2	37/2			
264.0 5	17 5	3116.3		2852.4	33/2 ⁺			
264.1 5	30 9	3839.0		3574.9	35/2 ⁺			
267.9 5	3 1	3013.0	31/2 ⁻	2745.1	29/2 ⁻			$R_{\text{ADO}}=0.65$ 18.
274.0 5	46 14	2900.6	31/2	2626.4	29/2		1.54 22	$R_{\text{ADO}}=1.59$ 20.
276.7 5	22 7	1429.9	19/2 ⁻	1153.1	17/2 ⁻	D	0.61 23	I_γ : $I_\gamma(276.7)$: $I_\gamma(535.5)=100:395(38)$ from Branching ratio. $R_{\text{ADO}}=0.58$ 9.
280.3 1	320 16	305.9	9/2 ⁻	25.6	5/2 ⁻	Q	1.06 5	$R_{\text{ADO}}=1.34$ 22.
281.6 5	13 4	1442.7	21/2 ⁻	1161.1	17/2 ⁻	Q	0.94 13	$R_{\text{ADO}}=1.29$ 20.
287.0 5	17 5	1716.9	21/2 ⁻	1429.9	19/2 ⁻			I_γ : $I_\gamma(287.0)$: $I_\gamma(563.8)=100:435(44)$ from Branching ratio. $R_{\text{ADO}}=0.70$ 14.
289.6 5	10 3	2006.5	23/2 ⁻	1716.9	21/2 ⁻			I_γ : $I_\gamma(289.6)$: $I_\gamma(576.7)=100:700(81)$ from Branching ratio. $R_{\text{ADO}}=0.49$ 13.
290.7 2	119 18	465.1	15/2 ⁺	174.4	11/2 ⁺	Q	1.07 8	$R_{\text{ADO}}=1.25$ 11.
294.1 5	24 7	3075.7	33/2	2781.6	31/2 ⁻	D	0.40 10	$R_{\text{ADO}}=0.59$ 4.
294.6 5	52 16	3039.1	33/2	2744.5	31/2 ⁺	D	0.60 10	$R_{\text{ADO}}=0.60$ 7.
296.0 2	160 24	500.3	11/2 ⁻	204.3	7/2 ⁻	Q	1.31 16	$R_{\text{ADO}}=1.44$ 10.
301.8 1	1000 50	505.0	17/2 ⁺	203.2	13/2 ⁺	Q	1.13 3	$R_{\text{ADO}}=1.23$ 3.
306.0 5	8 2	3720.7	37/2	3414.7	35/2	D	0.71 21	$R_{\text{ADO}}=0.61$ 9.
310.5 5	31 9	3211.3	33/2	2900.6	31/2	D	0.68 12	$R_{\text{ADO}}=0.88$ 23.
313.1 5	17 5	2433.6	29/2 ⁻	2120.4				
320.6 5	11 3	3532.1	35/2	3211.3	33/2			$R_{\text{ADO}}=0.9$ 3.
334.4 1	208 10	2230.8	27/2 ⁻	1896.3	25/2 ⁻	D	0.73 9	$R_{\text{ADO}}=1.02$ 8.
339.0 5	16 5	3414.7	35/2	3075.7	33/2	D	0.40 13	$R_{\text{ADO}}=0.54$ 3.
348.2 5	5 2	2781.6	31/2 ⁻	2433.6	29/2 ⁻			
355.2 5	4 1	4075.9	39/2	3720.7	37/2	D	0.5 3	$R_{\text{ADO}}=0.53$ 22.
359.1 5	4 1	2852.0		2492.9	27/2 ⁻			
359.3 5	10 3	3847.7	(39/2 ⁺)	3488.5	37/2 ⁺			
359.4 5	32 10	2792.9	31/2 ⁻	2433.6	29/2 ⁻	D	0.6 3	$R_{\text{ADO}}=0.8$ 3.
369.8 5	6 2	3784.5	37/2	3414.7	35/2			$R_{\text{ADO}}=0.36$ 14.
372.2 5	8 3	3488.5	37/2 ⁺	3116.3				
373.5 5	56 17	430.7	11/2 ⁻	57.2	7/2 ⁻	Q	1.06 18	$R_{\text{ADO}}=1.24$ 23.
377.8 5	38 11	2608.5	31/2 ⁻	2230.8	27/2 ⁻			$R_{\text{ADO}}=1.11$ 8.
379.0 5	53 16	3992.2	37/2	3613.2	35/2	D	0.50 18	$R_{\text{ADO}}=0.42$ 14.
379.1 5	76 23	2070.8	25/2 ⁻	1691.7	21/2 ⁻	Q	1.10 9	$R_{\text{ADO}}=1.25$ 8.
386.5 2	167 25	886.8	15/2 ⁻	500.3	11/2 ⁻	Q	0.92 12	$R_{\text{ADO}}=1.50$ 9.
388.6 2	141 21	694.5	13/2 ⁻	305.9	9/2 ⁻	Q	1.11 12	$R_{\text{ADO}}=1.22$ 4.
390.1 5	9 3	3506.4		3116.3				
390.9 5	33 10	3017.4	31/2	2626.4	29/2			$R_{\text{ADO}}=0.80$ 21.
397.6 2	100 15	902.8	19/2 ⁺	505.0	17/2 ⁺	D	0.35 4	$R_{\text{ADO}}=0.36$ 4.
400.0 5	12 4	1896.3	25/2 ⁻	1496.2	25/2 ⁺			
401.7 5	31 9	2632.5	31/2 ⁻	2230.8	27/2 ⁻			$R_{\text{ADO}}=1.3$ 4.
402.0 5	15 4	3613.2	35/2	3211.3	33/2			$R_{\text{ADO}}=0.7$ 3.
411.6 5	57 17	2482.4	29/2 ⁻	2070.8	25/2 ⁻	Q	1.07 12	$R_{\text{ADO}}=1.21$ 7.
425.1 5	90 27	650.9	13/2 ⁻	225.7	9/2 ⁻	Q	0.93 7	$R_{\text{ADO}}=1.24$ 7.
427.2 5	35 10	2518.9	29/2	2091.5	27/2 ⁺	D	0.71 25	$R_{\text{ADO}}=0.51$ 14.
436.0 5	22 7	3068.5	35/2 ⁻	2632.5	31/2 ⁻			$R_{\text{ADO}}=1.41$ 21.
437.7 1	263 13	902.8	19/2 ⁺	465.1	15/2 ⁺	Q	0.94 7	$R_{\text{ADO}}=1.21$ 5.
437.8 1	706 35	942.8	21/2 ⁺	505.0	17/2 ⁺	Q	0.93 5	$R_{\text{ADO}}=1.20$ 6.
445.3 5	33 10	1657.8	21/2 ⁻	1212.5	19/2		0.9 3	$R_{\text{ADO}}=1.1$ 3.

Continued on next page (footnotes at end of table)

$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09 (continued) $\gamma(^{187}\text{Pt})$ (continued)

E_γ^\dagger	I_γ^\dagger	$E_i(\text{level})$	J_i^π	E_f	J_f^π	Mult. #	DCO ratio \ddagger	Comments
460.0 5	24 7	3068.5	35/2 ⁻	2608.5	31/2 ⁻			R _{ADO} =1.18 11.
463.0 @ 5	74 @ 22	928.1	17/2	465.1	15/2 ⁺		0.35 8	R _{ADO} =0.45 6.
463.0 @ 2	129 @ 19	1349.8	19/2 ⁻	886.8	15/2 ⁻	Q	1.02 4	R _{ADO} =1.22 6.
463.8 2	102 15	894.4	15/2 ⁻	430.7	11/2 ⁻	Q	1.09 17	R _{ADO} =1.22 3.
466.6 2	121 18	1161.1	17/2 ⁻	694.5	13/2 ⁻	Q	1.15 7	R _{ADO} =1.22 4.
475.8 5	20 6	2900.6	31/2	2424.8	27/2			R _{ADO} =1.5 3.
480.1 5	10 3	3332.5	35/2 ⁺	2852.4	33/2 ⁺			
481.4 5	4 1	2745.1	29/2 ⁻	2263.6	25/2 ⁻			R _{ADO} =1.15 16.
486.6 5	8 2	2492.9	27/2 ⁻	2006.5	23/2 ⁻			R _{ADO} =1.4 3.
489.9 5	36 11	1418.0	21/2	928.1	17/2			R _{ADO} =1.4 4.
490.0 5	67 20	1839.8	23/2 ⁻	1349.8	19/2 ⁻	Q	0.93 15	R _{ADO} =1.25 11.
502.2 5	102 31	1153.1	17/2 ⁻	650.9	13/2 ⁻	Q	1.0 3	R _{ADO} =1.20 14.
504.5 5	54 16	3297.4	35/2 ⁻	2792.9	31/2 ⁻	Q	1.0 5	R _{ADO} =1.5 5.
504.7 5	46 14	1657.8	21/2 ⁻	1153.1	17/2 ⁻			
509.1 5	78 23	2942.7	33/2 ⁻	2433.6	29/2 ⁻	Q	1.02 12	R _{ADO} =1.29 13.
510.0 5	50 15	1452.9	23/2 ⁺	942.8	21/2 ⁺	D	0.46 16	R _{ADO} =0.41 7.
513.8 5	40 12	2996.2	33/2 ⁻	2482.4	29/2 ⁻	Q	1.0 3	R _{ADO} =1.25 12.
515.1 5	30 9	3847.7	(39/2 ⁺)	3332.5	35/2 ⁺			
515.2 5	60 18	1418.0	21/2	902.8	19/2 ⁺	D	0.41 6	R _{ADO} =0.41 6.
519.6 5	48 14	3038.8	33/2	2518.9	29/2	Q	1.2 4	R _{ADO} =1.6 3.
519.8 5	49 15	1869.6	23/2 ⁻	1349.8	19/2 ⁻	Q	1.08 13	R _{ADO} =1.39 11.
520.1 5	8 2	3013.0	31/2 ⁻	2492.9	27/2 ⁻			R _{ADO} =1.5 4.
521.6 5	9 3	2915.0	31/2 ⁻	2393.4	27/2 ⁻	Q	0.9 5	R _{ADO} =1.2 4.
523.8 5	26 8	2393.4	27/2 ⁻	1869.6	23/2 ⁻	Q	1.01 12	R _{ADO} =1.19 16.
530.6 5	80 24	1691.7	21/2 ⁻	1161.1	17/2 ⁻	Q	0.96 9	R _{ADO} =1.21 8.
530.8 5	50 15	2518.5	29/2	1987.7	25/2	Q	1.17 20	R _{ADO} =1.5 3.
534.8 5	47 14	3573.9		3039.1	33/2			
535.5 5	87 26	1429.9	19/2 ⁻	894.4	15/2 ⁻	Q	1.16 21	R _{ADO} =1.34 13.
535.8 5	10 3	3574.9	35/2 ⁺	3038.8	33/2	D	0.4 9	R _{ADO} =0.6 3.
537.3 2	108 16	2433.6	29/2 ⁻	1896.3	25/2 ⁻	Q	0.93 12	R _{ADO} =1.19 18.
542.0 5	4 1	3287.1	33/2 ⁻	2745.1	29/2 ⁻			R _{ADO} =1.3 5.
546.6 5	36 11	2263.6	25/2 ⁻	1716.9	21/2 ⁻	Q	1.2 4	R _{ADO} =1.36 9.
548.7 5	27 8	3617.2	39/2 ⁻	3068.5	35/2 ⁻			R _{ADO} =1.27 24.
550.1 2	168 25	1452.9	23/2 ⁺	902.8	19/2 ⁺	Q	1.06 15	R _{ADO} =1.30 10.
550.7 5	15 4	2781.6	31/2 ⁻	2230.8	27/2 ⁻			R _{ADO} =1.4 4.
553.4 1	362 18	1496.2	25/2 ⁺	942.8	21/2 ⁺	Q	0.97 5	R _{ADO} =1.27 6.
556.8 5	30 9	4045.3	41/2 ⁺	3488.5	37/2 ⁺	Q	1.15 25	R _{ADO} =1.34 17.
562.1 5	55 16	2792.9	31/2 ⁻	2230.8	27/2 ⁻			R _{ADO} =1.5 3.
563.8 5	74 22	1716.9	21/2 ⁻	1153.1	17/2 ⁻	Q	0.96 20	R _{ADO} =1.36 14.
569.7 5	94 28	1987.7	25/2	1418.0	21/2	Q	0.98 15	R _{ADO} =1.4 3.
576.7 5	70 21	2006.5	23/2 ⁻	1429.9	19/2 ⁻	Q	0.92 17	R _{ADO} =1.45 19.
577.4 5	31 9	1789.8	23/2	1212.5	19/2			R _{ADO} =1.19 23.
585.0 5	24 7	3211.3	33/2	2626.4	29/2			
587.9 5	55 16	3332.5	35/2 ⁺	2744.5	31/2 ⁺	Q	1.00 19	R _{ADO} =1.32 21.
591.6 5	15 4	3889.0	39/2 ⁻	3297.4	35/2 ⁻			R _{ADO} =1.2 3.
595.6 5	43 13	2091.5	27/2 ⁺	1496.2	25/2 ⁺	D	0.38 8	R _{ADO} =0.64 10.
595.7 5	34 10	3613.2	35/2	3017.4	31/2			
601.5 5	26 8	2744.5	31/2 ⁺	2142.8	29/2 ⁺			
609.6 5	51 15	3552.3	37/2 ⁻	2942.7	33/2 ⁻			R _{ADO} =1.33 22.
610.5 5	20 6	3606.7	37/2 ⁻	2996.2	33/2 ⁻			R _{ADO} =1.3 4.
628.1 5	22 7	2070.8	25/2 ⁻	1442.7	21/2 ⁻	Q	0.92 8	R _{ADO} =1.17 12.
631.0 5	18 5	2322.7	25/2 ⁻	1691.7	21/2 ⁻	Q	0.95 22	R _{ADO} =1.4 3.
631.7 5	21 6	3532.1	35/2	2900.6	31/2			R _{ADO} =1.29 19.
635.0 2	103 15	2424.8	27/2	1789.8	23/2			R _{ADO} =1.18 12.
636.2 5	46 14	3488.5	37/2 ⁺	2852.4	33/2 ⁺	Q	0.96 21	R _{ADO} =1.19 12.

Continued on next page (footnotes at end of table)

$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ **2007Zh09 (continued)** $\gamma(^{187}\text{Pt})$ (continued)

E_γ †	I_γ †	$E_i(\text{level})$	J_i^π	E_f	J_f^π	Mult. #	DCO ratio ‡	Comments
638.6 2	177 27	2091.5	27/2 ⁺	1452.9	23/2 ⁺	Q	1.02 12	$R_{\text{ADO}}=1.24$ 15.
644.0 5	26 8	3976.5		3332.5	35/2 ⁺			
645.0 5	9 3	3720.7	37/2	3075.7	33/2			
646.5 2	196 29	2142.8	29/2 ⁺	1496.2	25/2 ⁺	Q	0.94 9	$R_{\text{ADO}}=1.23$ 11.
653.0 2	128 19	2744.5	31/2 ⁺	2091.5	27/2 ⁺	Q	1.09 11	$R_{\text{ADO}}=1.24$ 7.
665.5 5	8 2	4554.5	43/2 ⁻	3889.0	39/2 ⁻			$R_{\text{ADO}}=1.33$ 25.
666.3 5	31 9	2654.0	29/2	1987.7	25/2	Q	1.0 3	$R_{\text{ADO}}=1.3$ 3.
678.0 5	16 5	4723.3	45/2 ⁺	4045.3	41/2 ⁺			$R_{\text{ADO}}=1.3$ 3.
697.5 5	20 6	4249.8	41/2 ⁻	3552.3	37/2 ⁻			$R_{\text{ADO}}=1.5$ 7.
700.6 5	8 2	4307.3	41/2 ⁻	3606.7	37/2 ⁻			$R_{\text{ADO}}=1.4$ 4.
704.0 5	22 7	3574.9	35/2 ⁺	2871.1	31/2 ⁺	Q	1.0 6	
707.4 5	79 24	1212.5	19/2	505.0	17/2 ⁺		0.30 6	$R_{\text{ADO}}=0.50$ 4.
709.6 2	116 17	2852.4	33/2 ⁺	2142.8	29/2 ⁺	Q	0.99 10	$R_{\text{ADO}}=1.19$ 8.
712.5 5	13 4	3613.2	35/2	2900.6	31/2	Q	1.2 6	$R_{\text{ADO}}=1.3$ 5.
715.0 2	158 24	1657.8	21/2 ⁻	942.8	21/2 ⁺		0.94 8	$R_{\text{ADO}}=1.27$ 4.
719.5 5	5 2	5274.0	47/2 ⁻	4554.5	43/2 ⁻			$R_{\text{ADO}}=1.3$ 4.
719.8 5	8 2	4318.2	41/2 ⁺	3598.4	37/2 ⁺			$R_{\text{ADO}}=1.4$ 4.
736.5 5	7 2	4986.3	45/2 ⁻	4249.8	41/2 ⁻			
746.0 5	26 8	3598.4	37/2 ⁺	2852.4	33/2 ⁺	Q	1.0 3	$R_{\text{ADO}}=1.23$ 20.
755.2 5	31 9	1657.8	21/2 ⁻	902.8	19/2 ⁺	D	0.79 16	$R_{\text{ADO}}=0.74$ 15.
779.7 5	78 23	2871.1	31/2 ⁺	2091.5	27/2 ⁺	Q	0.89 15	$R_{\text{ADO}}=1.19$ 13.
781.0 5	15 5	3992.2	37/2	3211.3	33/2			
787.0 5	13 4	5510.3	49/2 ⁺	4723.3	45/2 ⁺			$R_{\text{ADO}}=1.4$ 3.
830.5 5	24 7	3574.9	35/2 ⁺	2744.5	31/2 ⁺			
847.0 5	87 26	1789.8	23/2	942.8	21/2 ⁺	D	0.43 5	$R_{\text{ADO}}=0.58$ 6.
904.0 5	39 12	1409.1	17/2 ⁻	505.0	17/2 ⁺			
928.5 5	62 19	2424.8	27/2	1496.2	25/2 ⁺	D	0.37 5	$R_{\text{ADO}}=0.48$ 6.
944.0 5	18 5	1409.1	17/2 ⁻	465.1	15/2 ⁺			$R_{\text{ADO}}=0.94$ 20.
973.6 5	13 4	3116.3		2142.8	29/2 ⁺			
1130.2 5	11 3	2626.4	29/2	1496.2	25/2 ⁺	Q	0.87 21	$R_{\text{ADO}}=1.13$ 20.

† In **2007Zh09**, ΔE and ΔI_γ of the γ -rays quoted as 0.1 to 0.5 keV and 5 to 30%, respectively. Evaluator assigned $\Delta E=0.5$ keV and ΔI_γ 30% for $I_\gamma<100$; ΔE 0.2 keV and ΔI_γ 15% for I_γ 100 to 200; and ΔE 0.1 keV and ΔI_γ 5% for $I_\gamma>200$ – from a private communication with **2007Zh09**.

‡ Detectors at $\theta_1=\pm 40^\circ$ and $\theta_2=90^\circ$. Gated on $\Delta J=2$, stretched quadrupole.

Assigned by the evaluator based on the DCO and ADO ratios. Typical values of DCO ratios are 1.0 and ≈ 0.7 for quadrupole (Q, $\Delta=2$) and dipole (D, $\Delta=1$ or sometimes $\Delta=0$) transitions, respectively. Typical values of R_{ADO} are ≈ 1.3 and ≈ 0.7 for quadrupole and dipole transitions, respectively. Asymmetry ratio R_{ADO} corresponds to 40° and 90° (**2007Zh09**).

@ Multiply placed with intensity suitably divided.

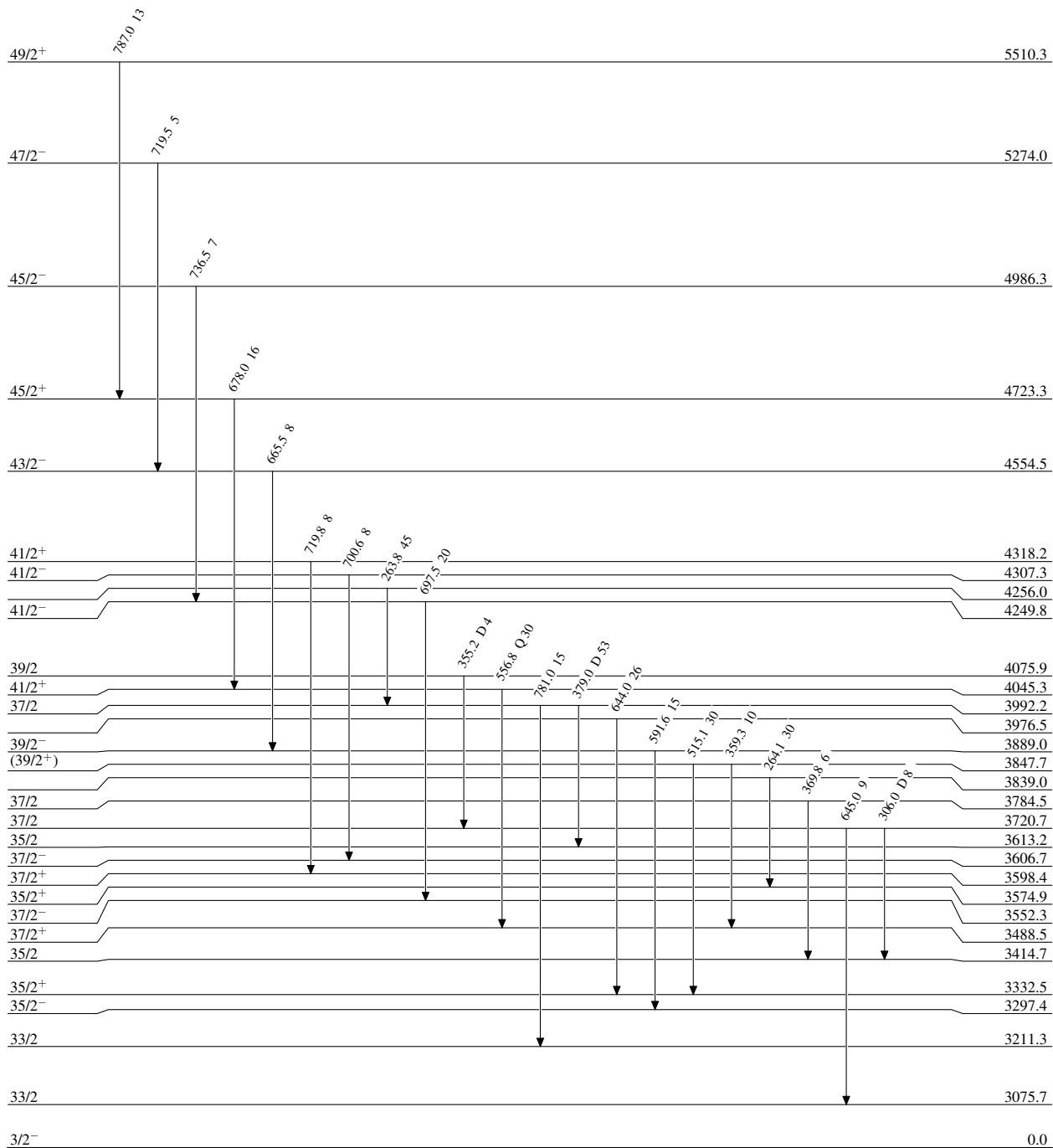
$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Level Scheme

Intensities: Relative I_γ

Legend

- $I_\gamma < 2\% \times I_\gamma^{max}$
- $I_\gamma < 10\% \times I_\gamma^{max}$
- $I_\gamma > 10\% \times I_\gamma^{max}$



$^{187}_{78}\text{Pt}_{109}$

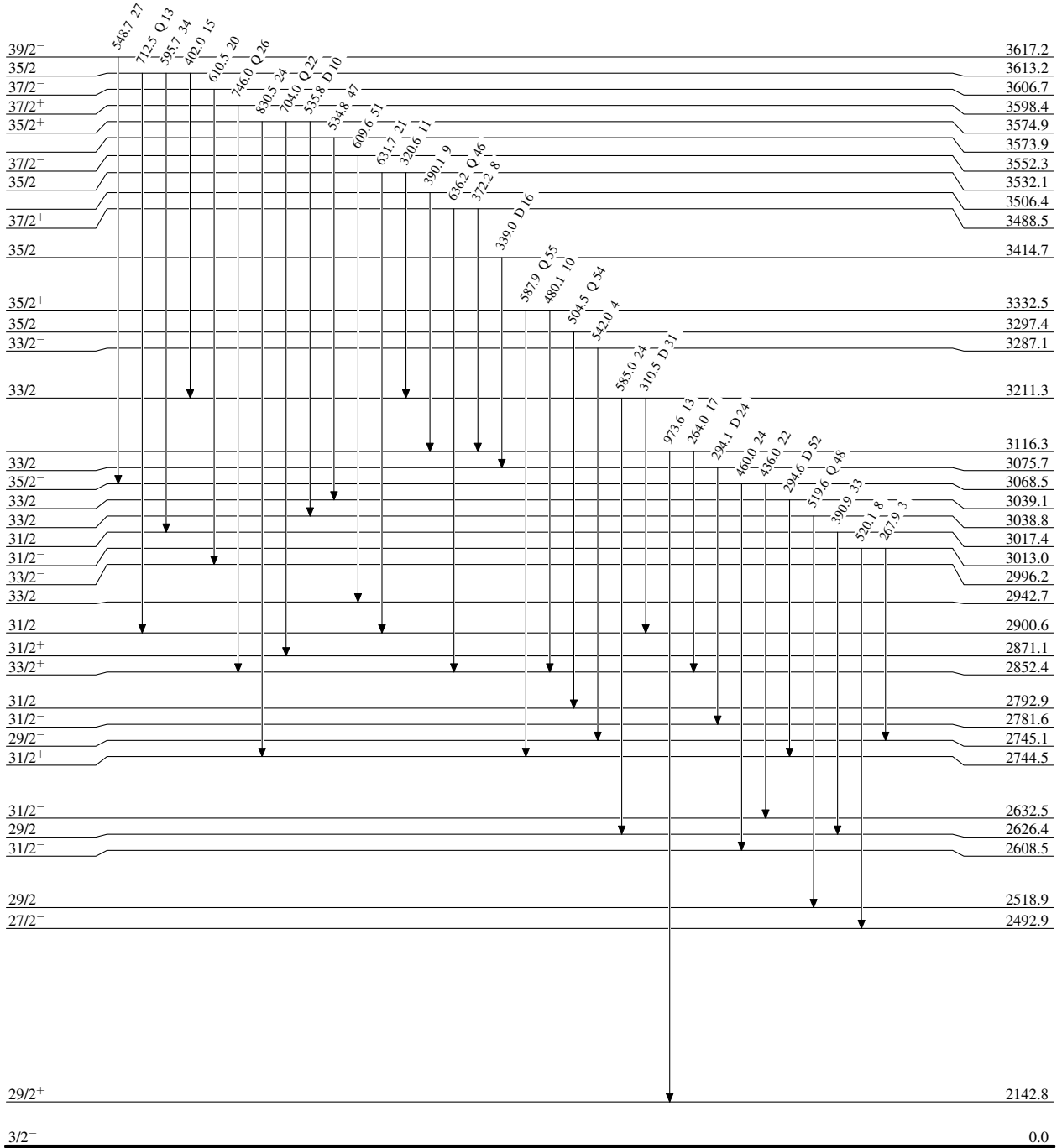
¹⁷³Yb(¹⁸O,4n γ) 2007Zh09

Level Scheme (continued)

Intensities: Relative I γ

Legend

- I γ < 2% × I γ ^{max}
- I γ < 10% × I γ ^{max}
- I γ > 10% × I γ ^{max}



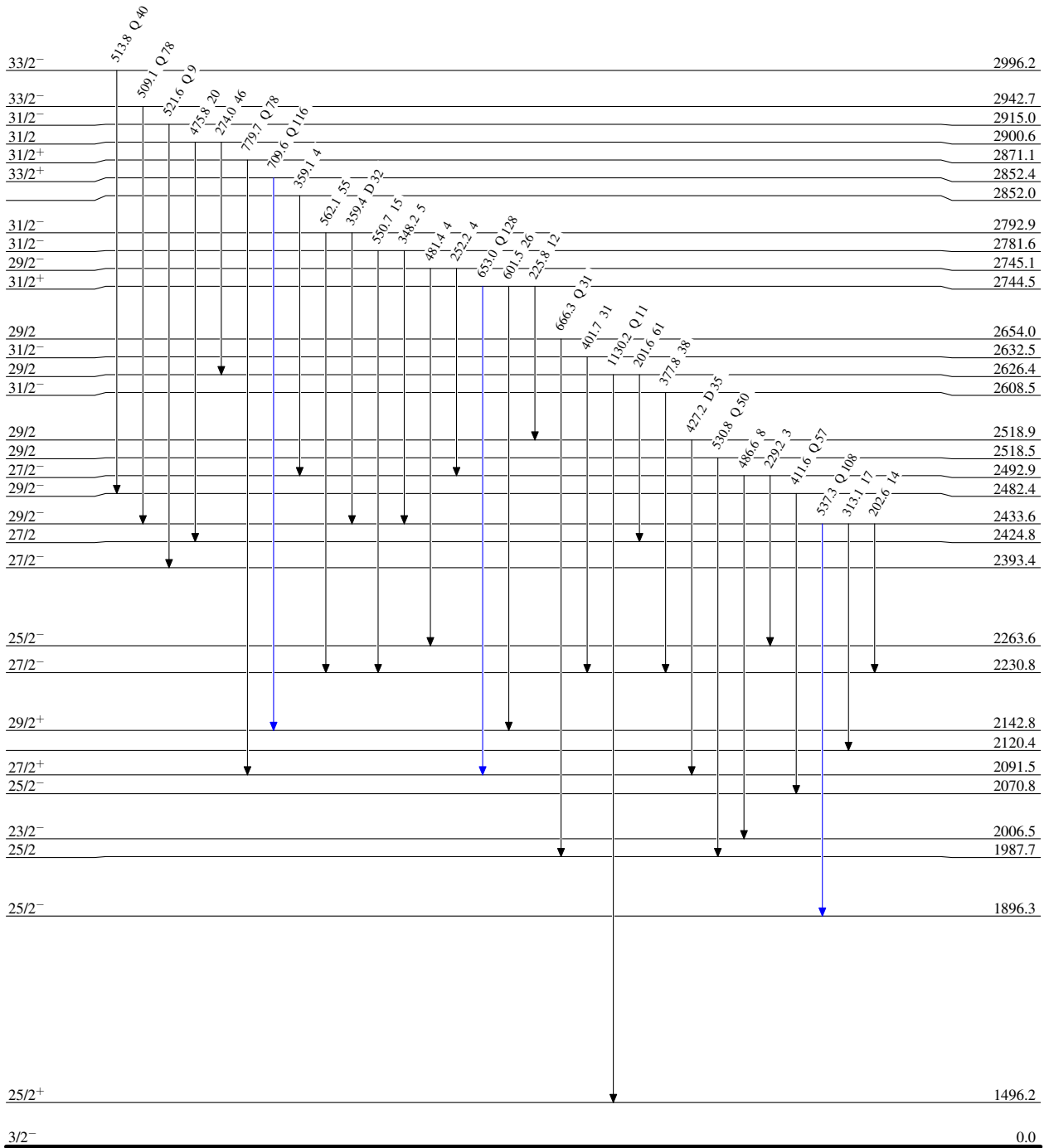
$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Level Scheme (continued)

Intensities: Relative I_γ

Legend

- $I_\gamma < 2\% \times I_\gamma^{max}$
- $I_\gamma < 10\% \times I_\gamma^{max}$
- $I_\gamma > 10\% \times I_\gamma^{max}$



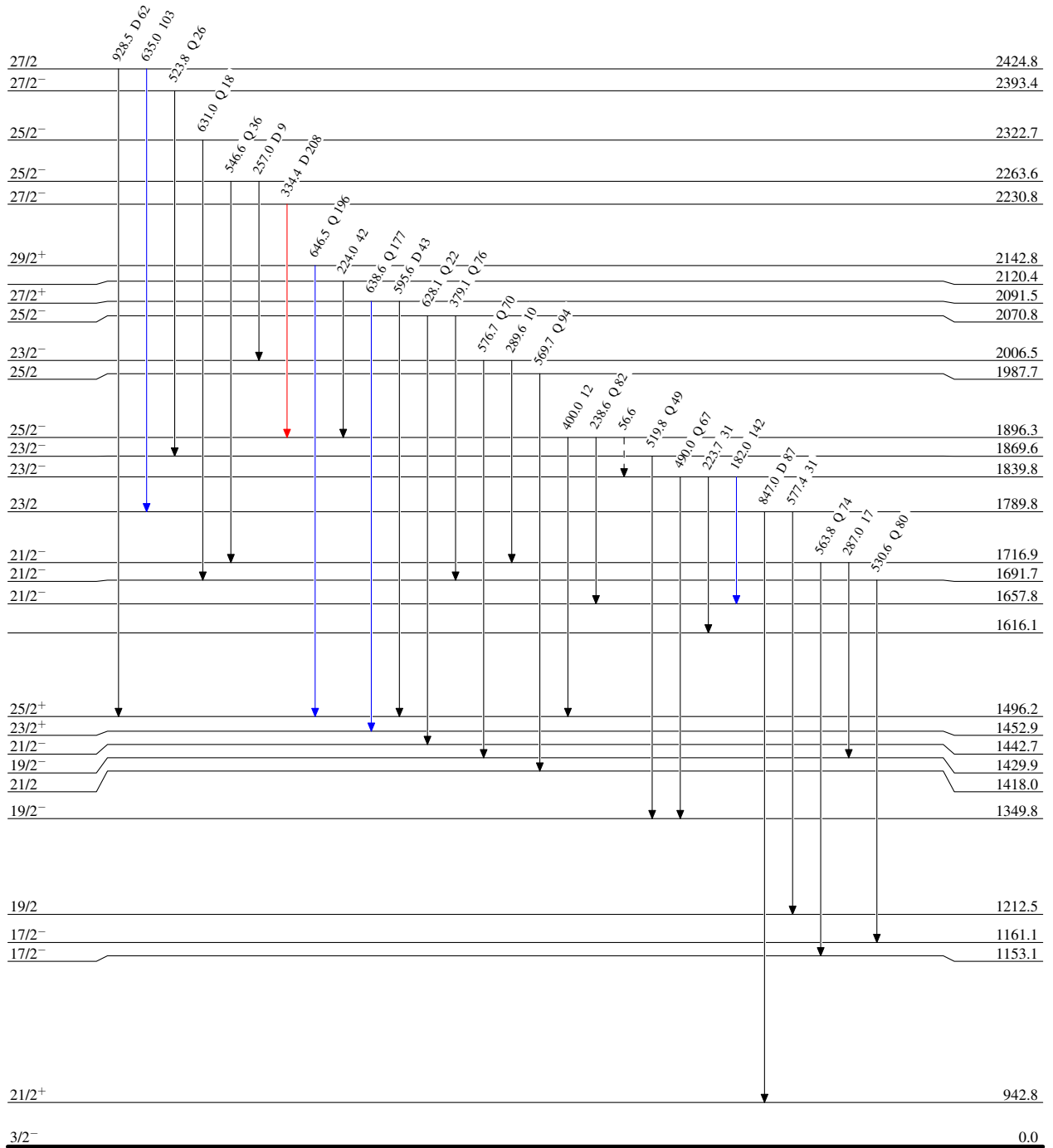
$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Legend

Level Scheme (continued)

Intensities: Relative I_γ

- ▶ $I_\gamma < 2\% \times I_\gamma^{max}$
- ▶ $I_\gamma < 10\% \times I_\gamma^{max}$
- ▶ $I_\gamma > 10\% \times I_\gamma^{max}$
- - - -▶ γ Decay (Uncertain)



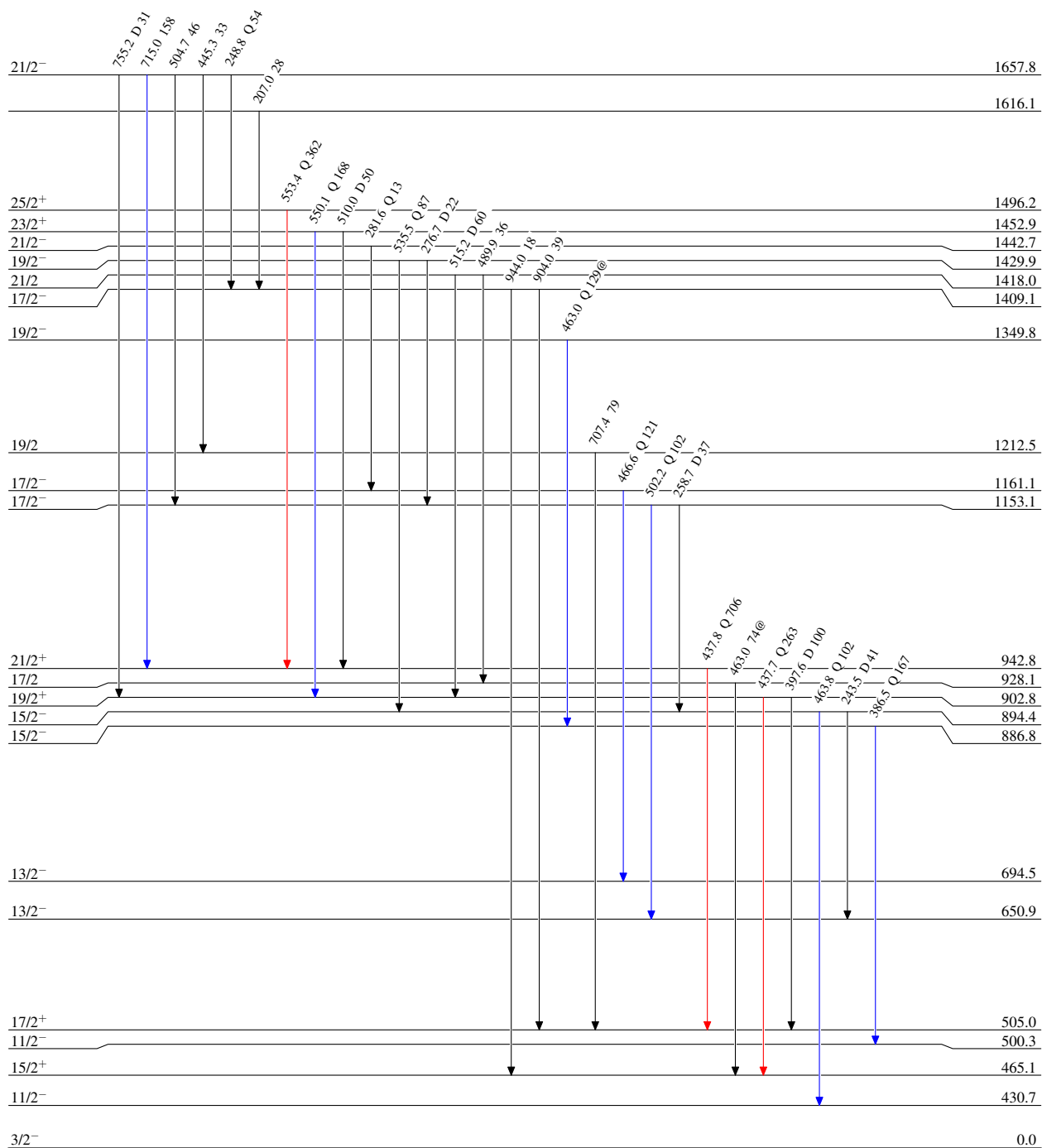
$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Level Scheme (continued)

Intensities: Relative I_γ
 @ Multiply placed: intensity suitably divided

Legend

→ $I_\gamma < 2\% \times I_\gamma^{\max}$
 → $I_\gamma < 10\% \times I_\gamma^{\max}$
 → $I_\gamma > 10\% \times I_\gamma^{\max}$

 $^{187}_{78}\text{Pt}_{109}$

$^{173}\text{Yb}(^{18}\text{O},4n\gamma)$ 2007Zh09

Level Scheme (continued)

Intensities: Relative I_γ
 @ Multiply placed: intensity suitably divided

Legend

—▶ $I_\gamma < 2\% \times I_\gamma^{\max}$
 —▶ $I_\gamma < 10\% \times I_\gamma^{\max}$
 —▶ $I_\gamma > 10\% \times I_\gamma^{\max}$

