

# Resonance Evaluation at ORNL



**L. Leal (ORNL)**

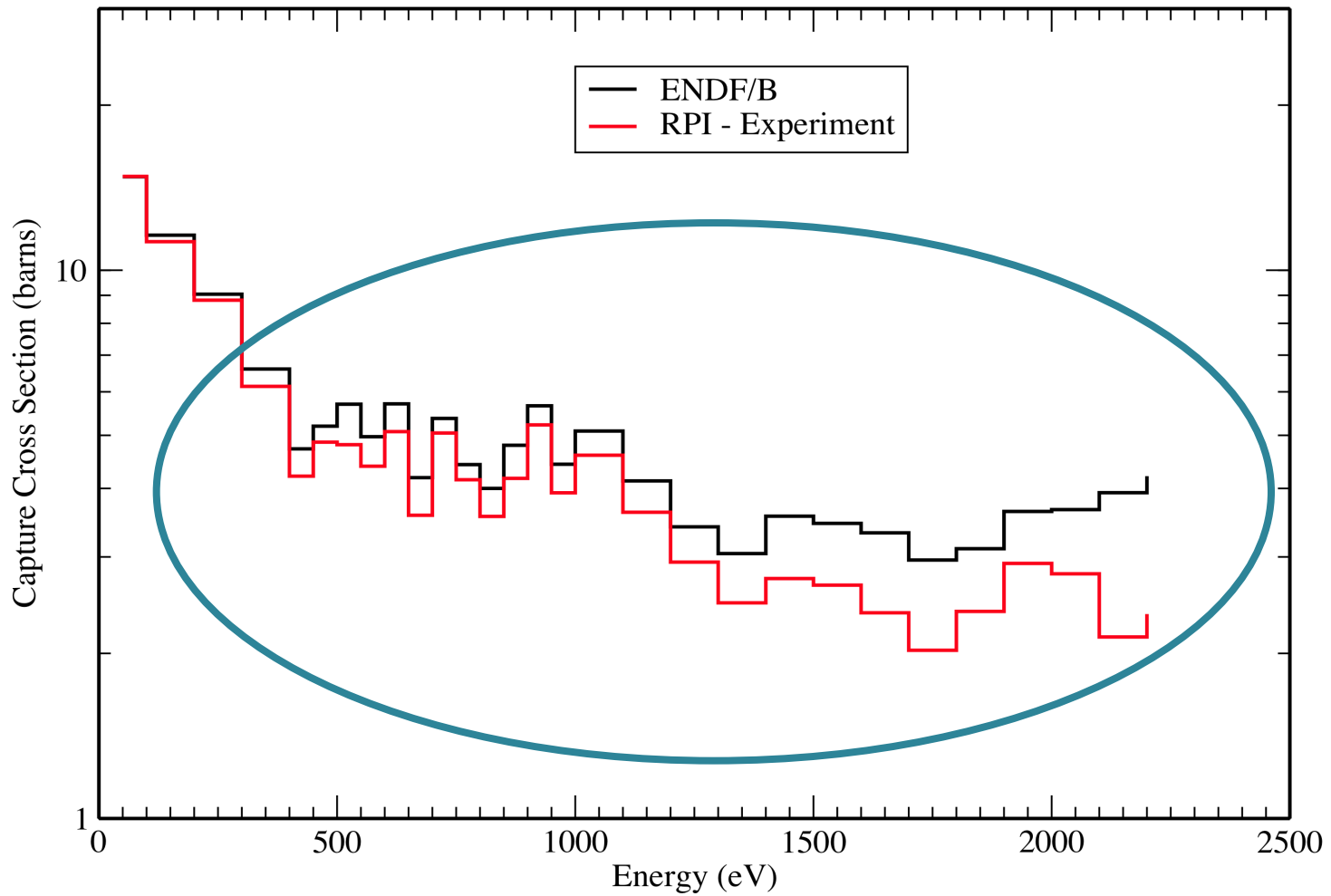
**Y. Danon (RPI)**

**CSEWG, Nov 5-9, 2012**

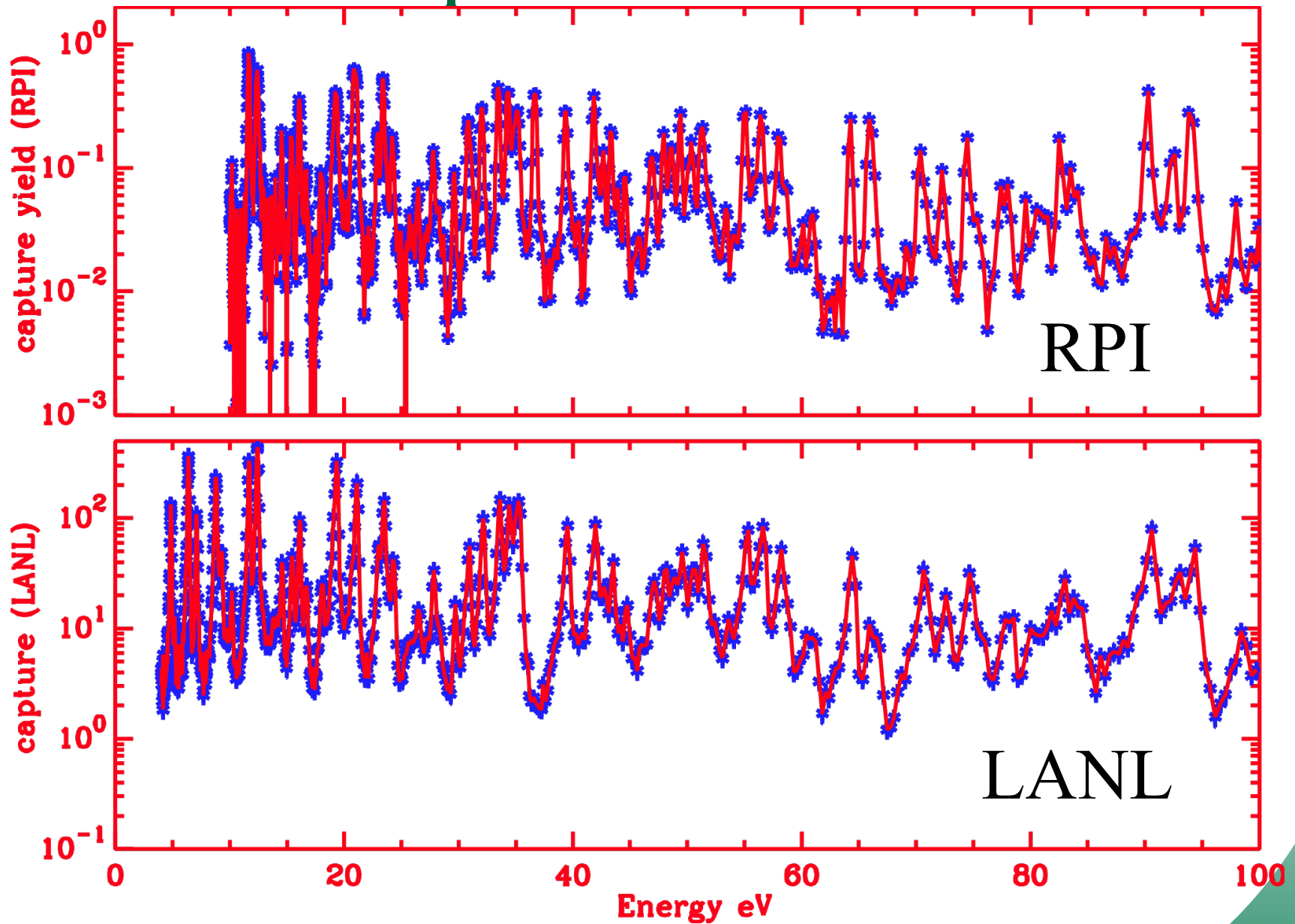
## **$^{235}\text{U}$ Evaluation:**

- ✓ **Intermediate energy benchmark problems;**
- ✓ **Fit new data measurements from RPI (capture and fission yields);**
- ✓ **Capture data from LANL;**
- ✓ **Test the new SAMMY  $^{235}\text{U}$  evaluation in benchmark calculations: ZEUS benchmarks;**
- ✓ **Use JENDL4 as the template;**
- ✓ **Benchmark Calculations done with everything else from ENDF;**

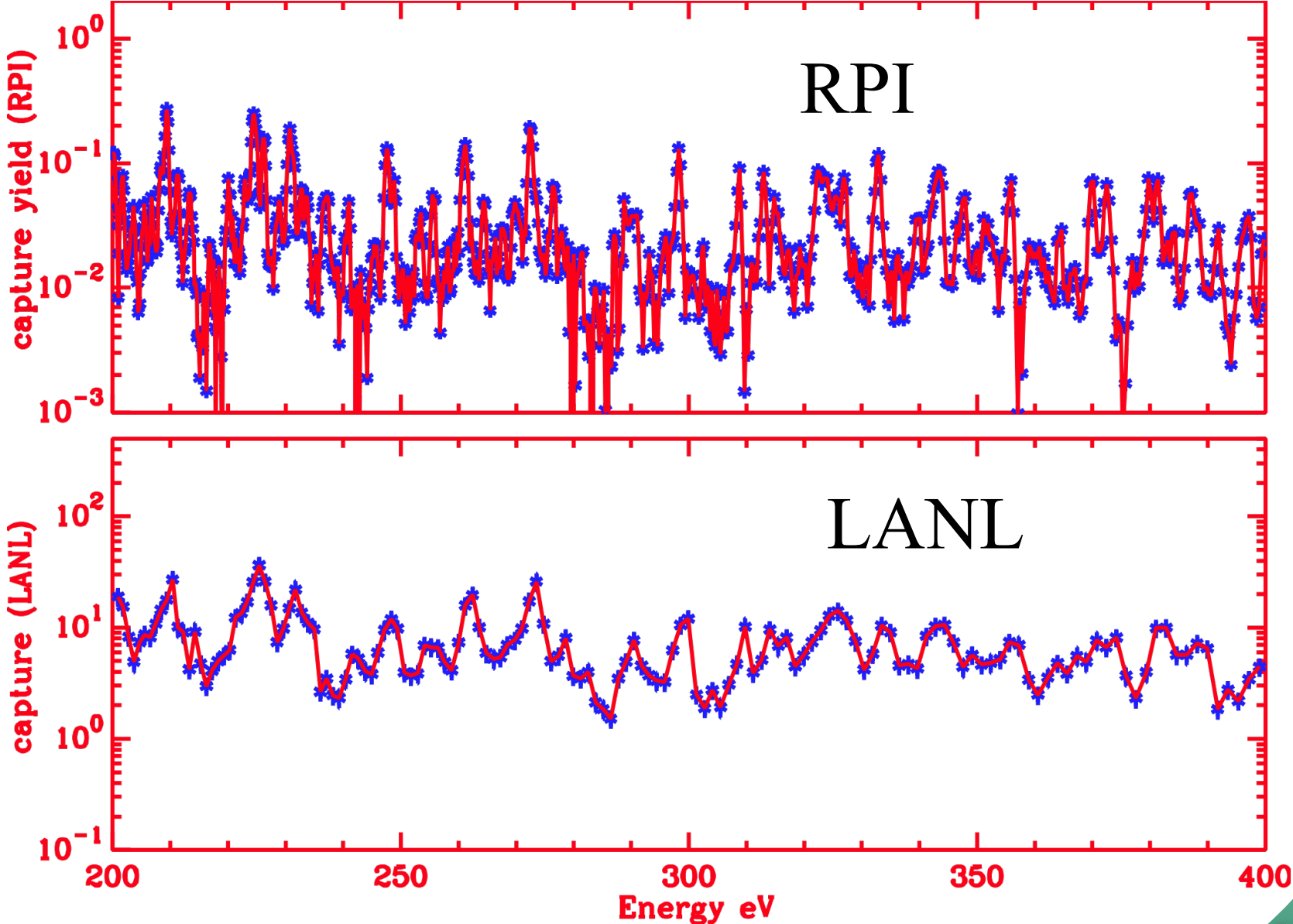
# RPI data and ENDF evaluation



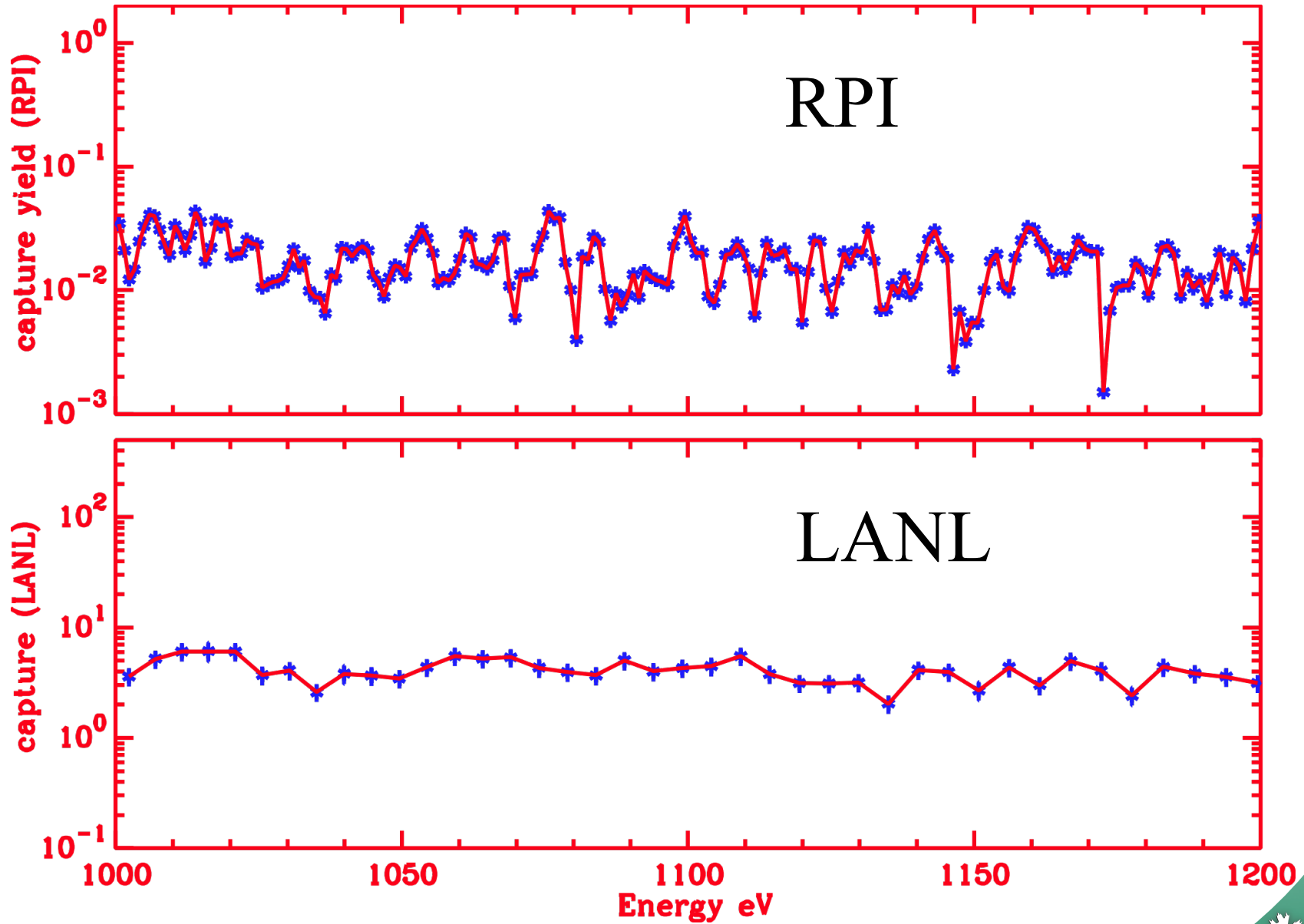
# RPI and LANL Capture Data



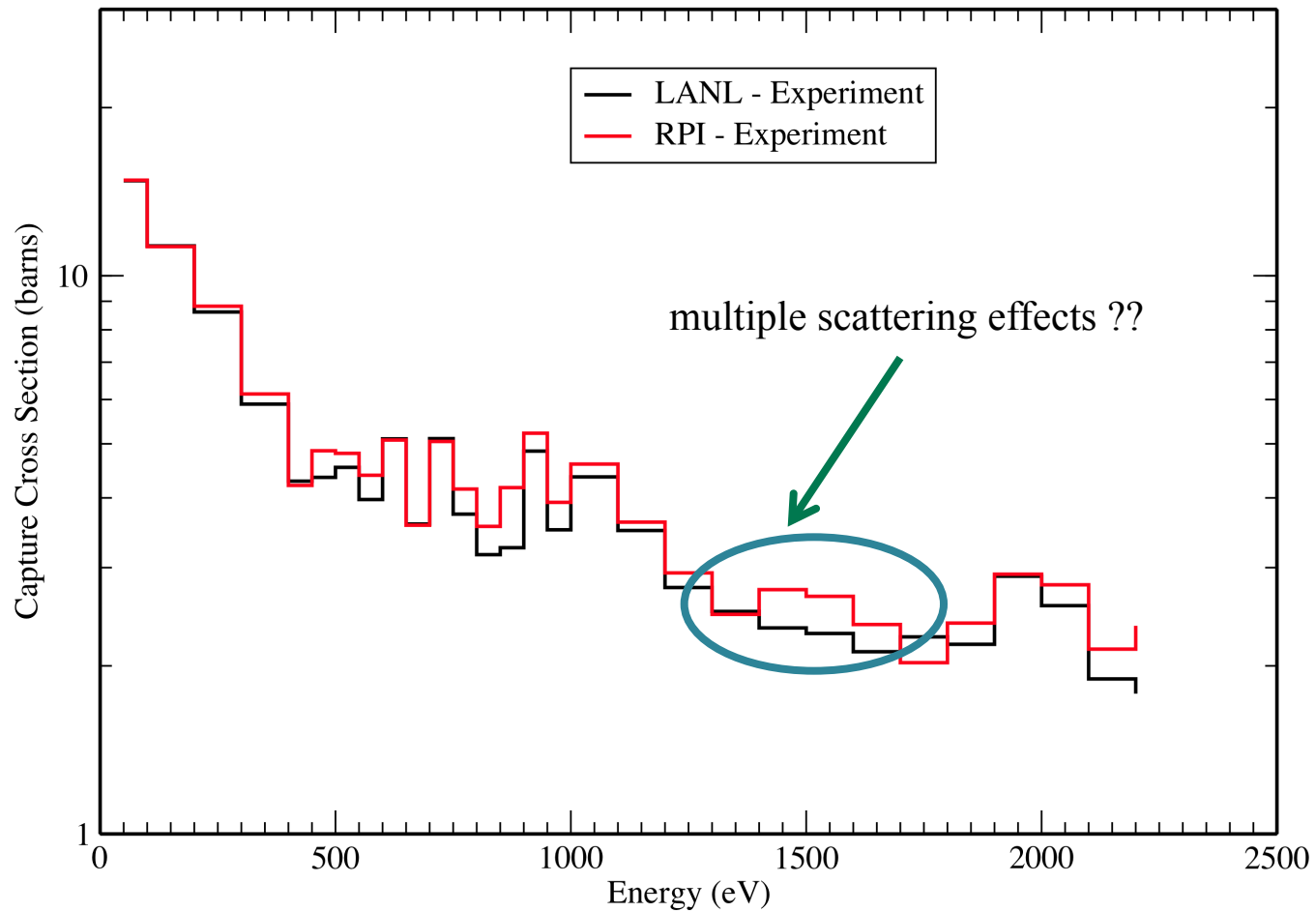
# RPI and LANL Capture Data



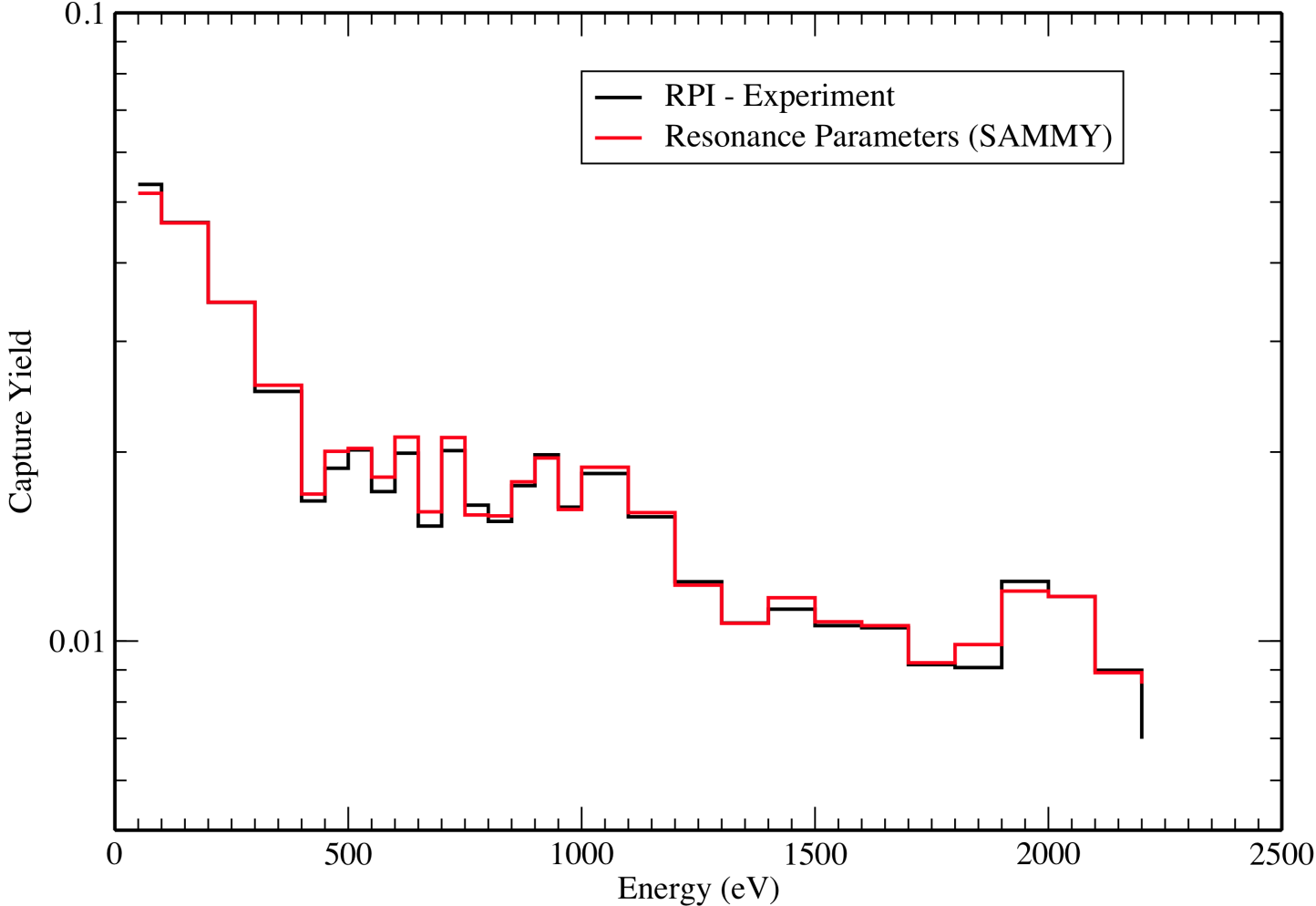
# RPI and LANL Capture Data



# RPI and LANL Capture Data (average)

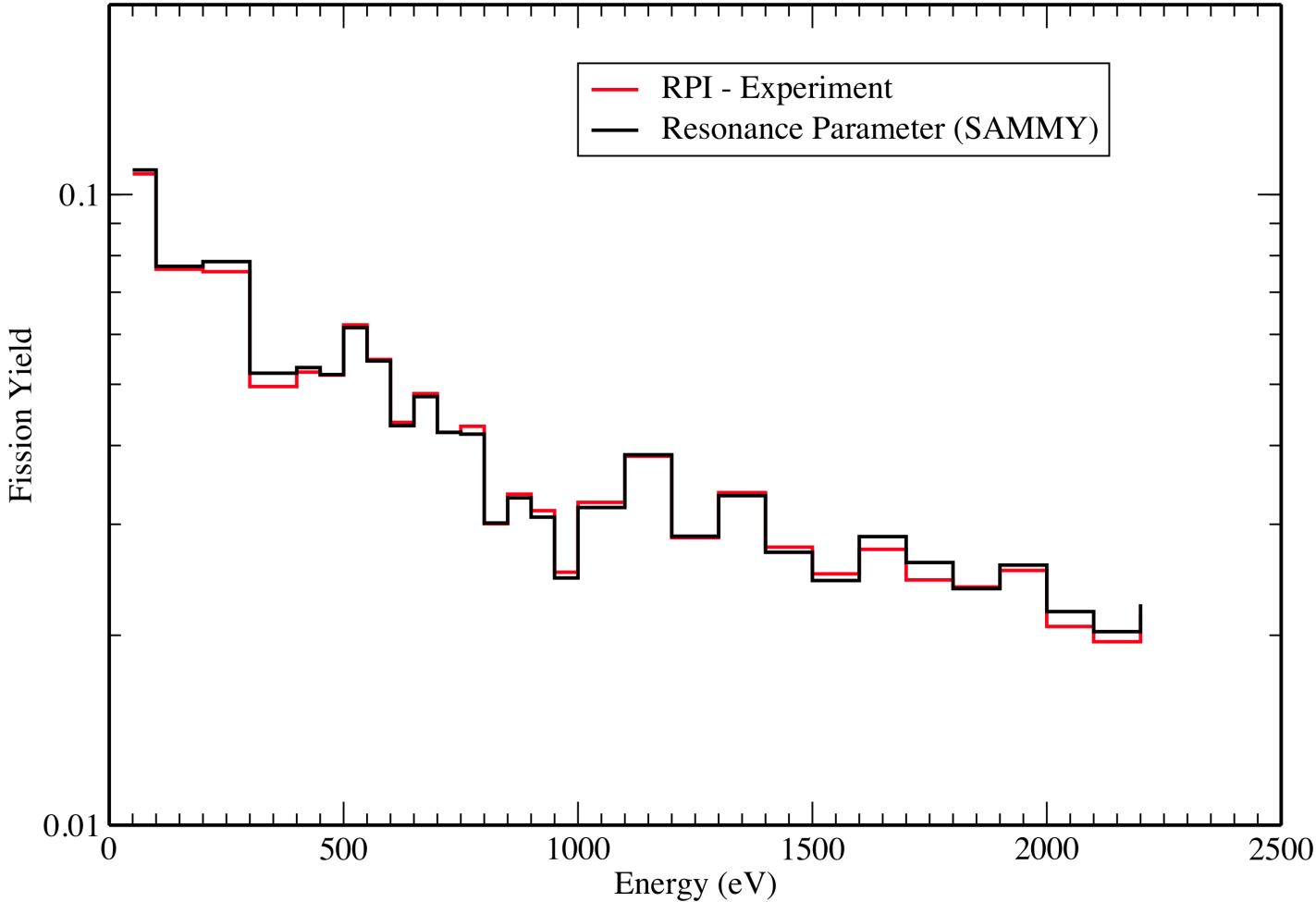


# Fit of the RPI data

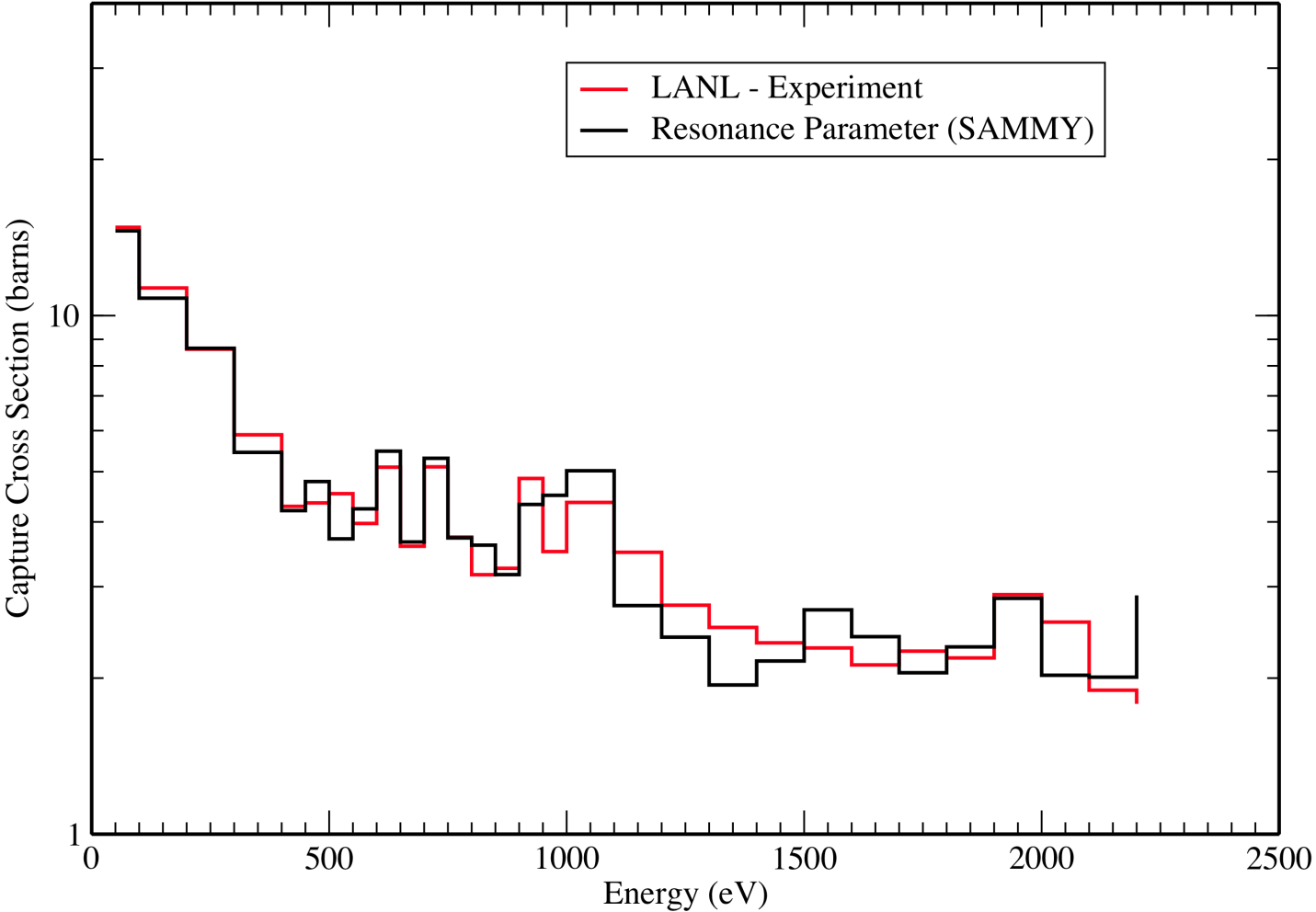




# Fit of the RPI data



# Fit of the LANL data



# The HEU-MET-INTER-006 cases (ZEUS)

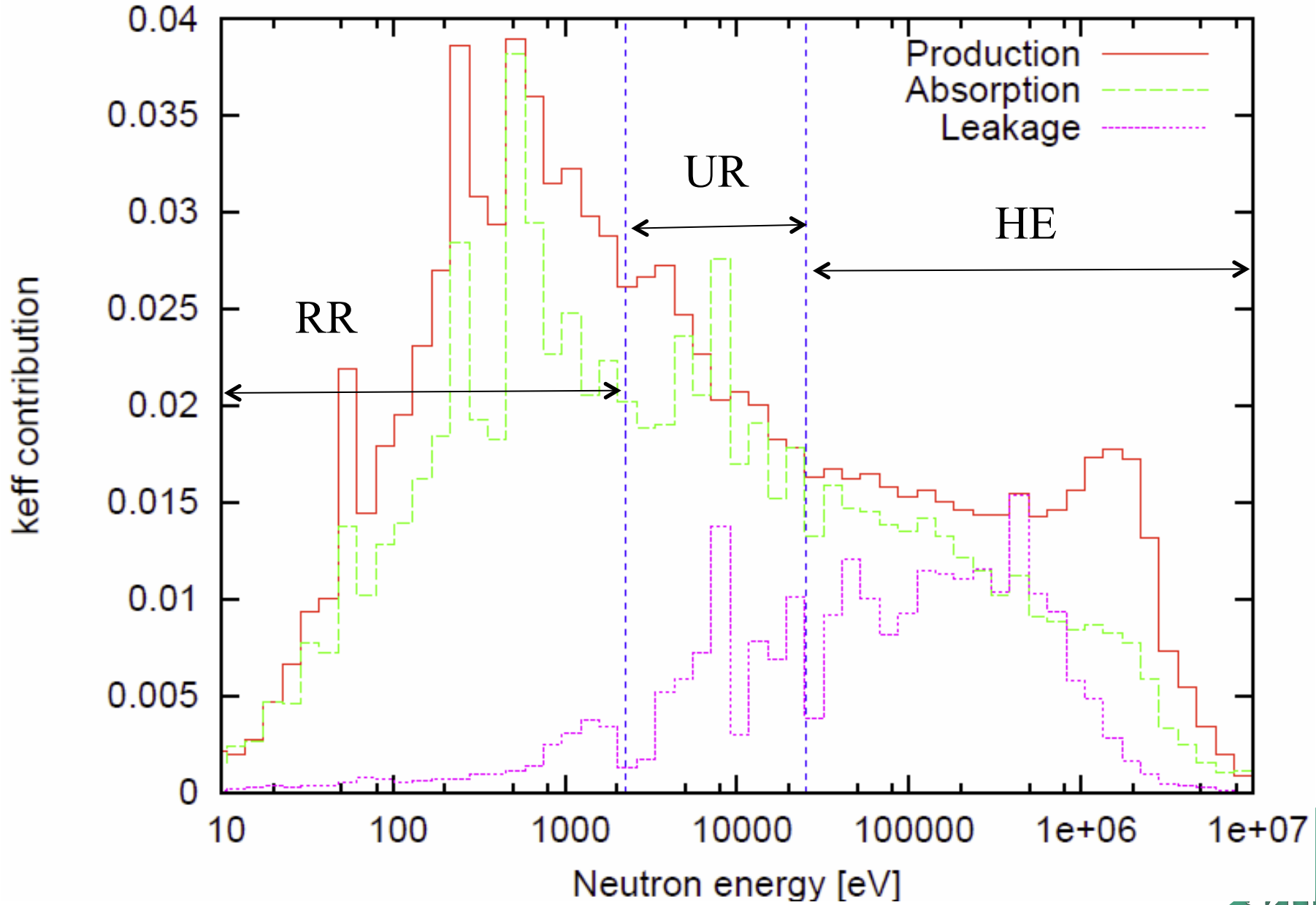
Case Number	$k_{\text{eff}}$	EALF (keV)	Intermediate-Energy Fission Fraction
1	0.9977 ± 0.0008	4.44	0.730
2	1.0001 ± 0.0008	9.45	0.698
3	1.0015 ± 0.0008	22.80	0.636
4	1.0016 ± 0.0008	80.80	0.503

EALF: Energy Average Lethargy Causing Fission

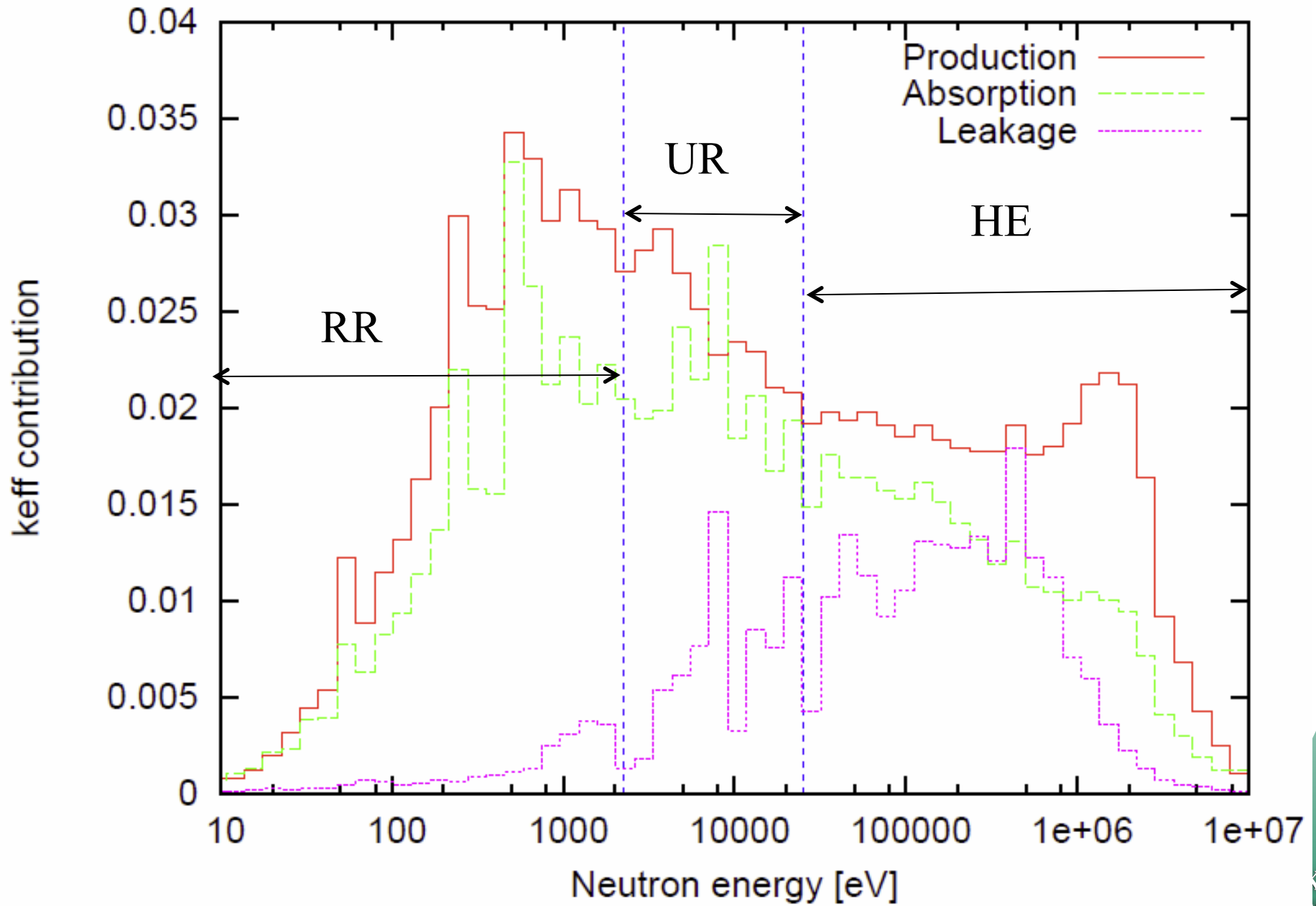
# Effective System Multiplication Factor

$$k_{eff} = \frac{\textit{Production}}{\textit{Absorption} + \textit{Leakage}}$$

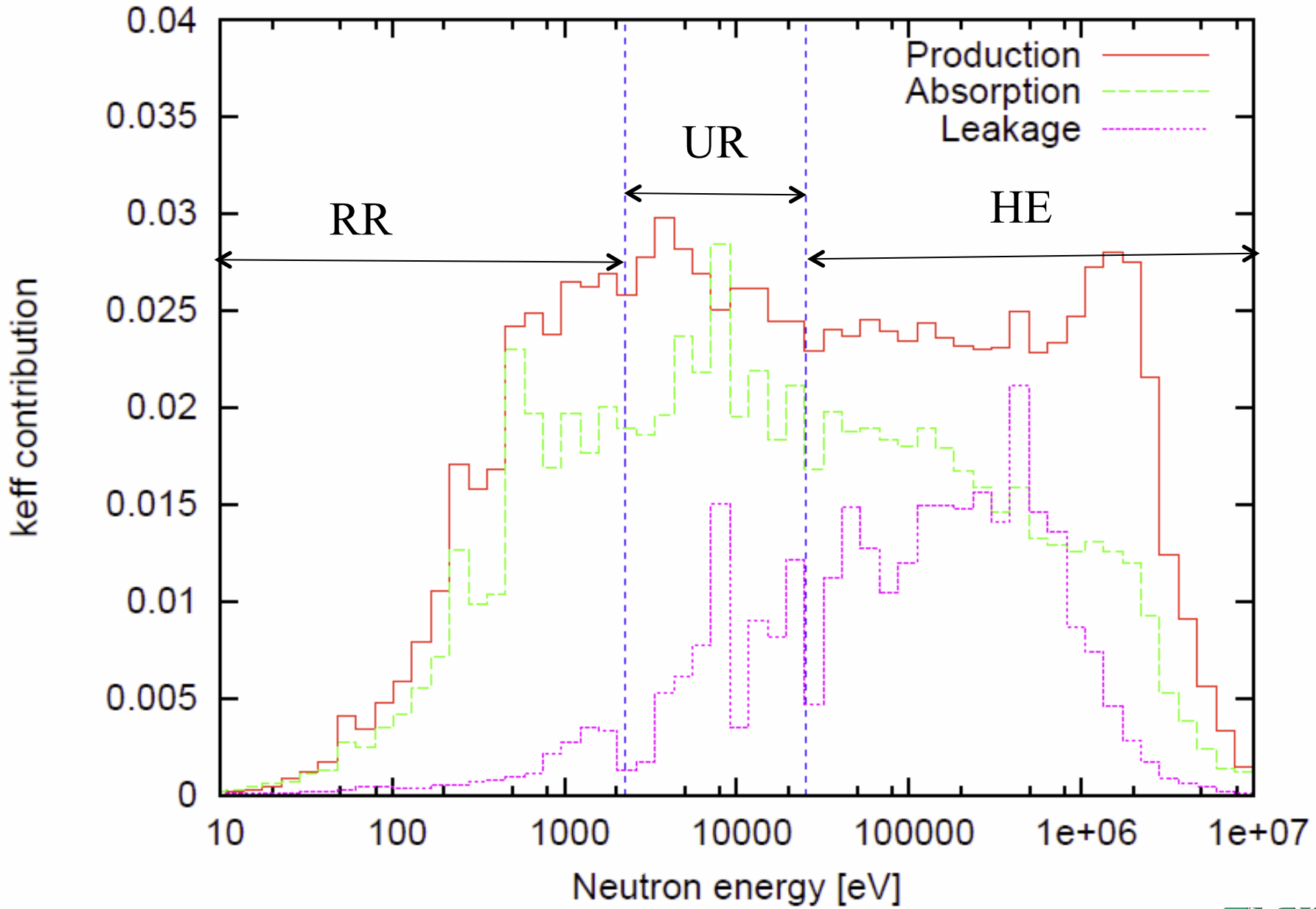
# ZEUS1



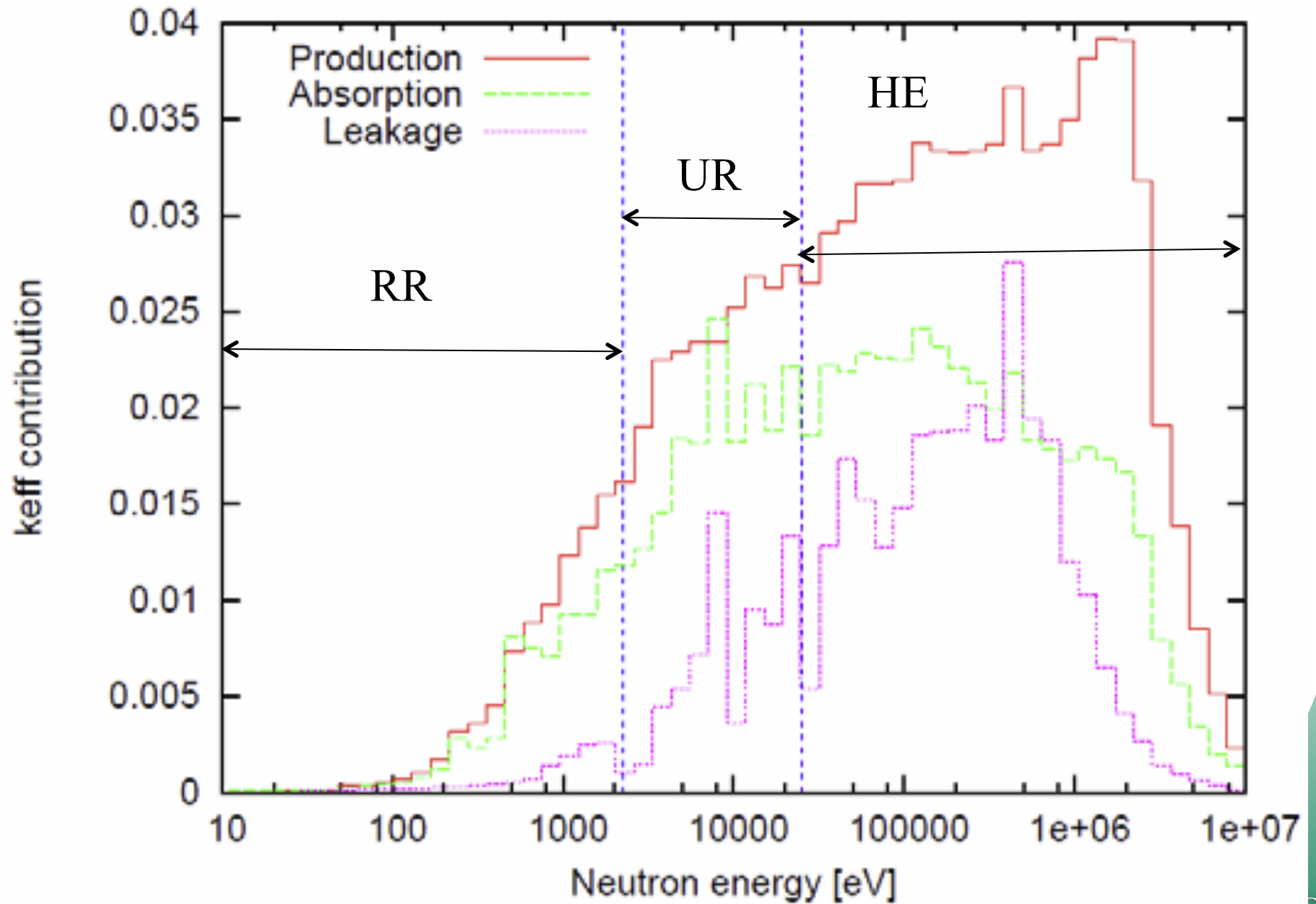
# ZEUS2



# ZEUS3



# ZEUS4

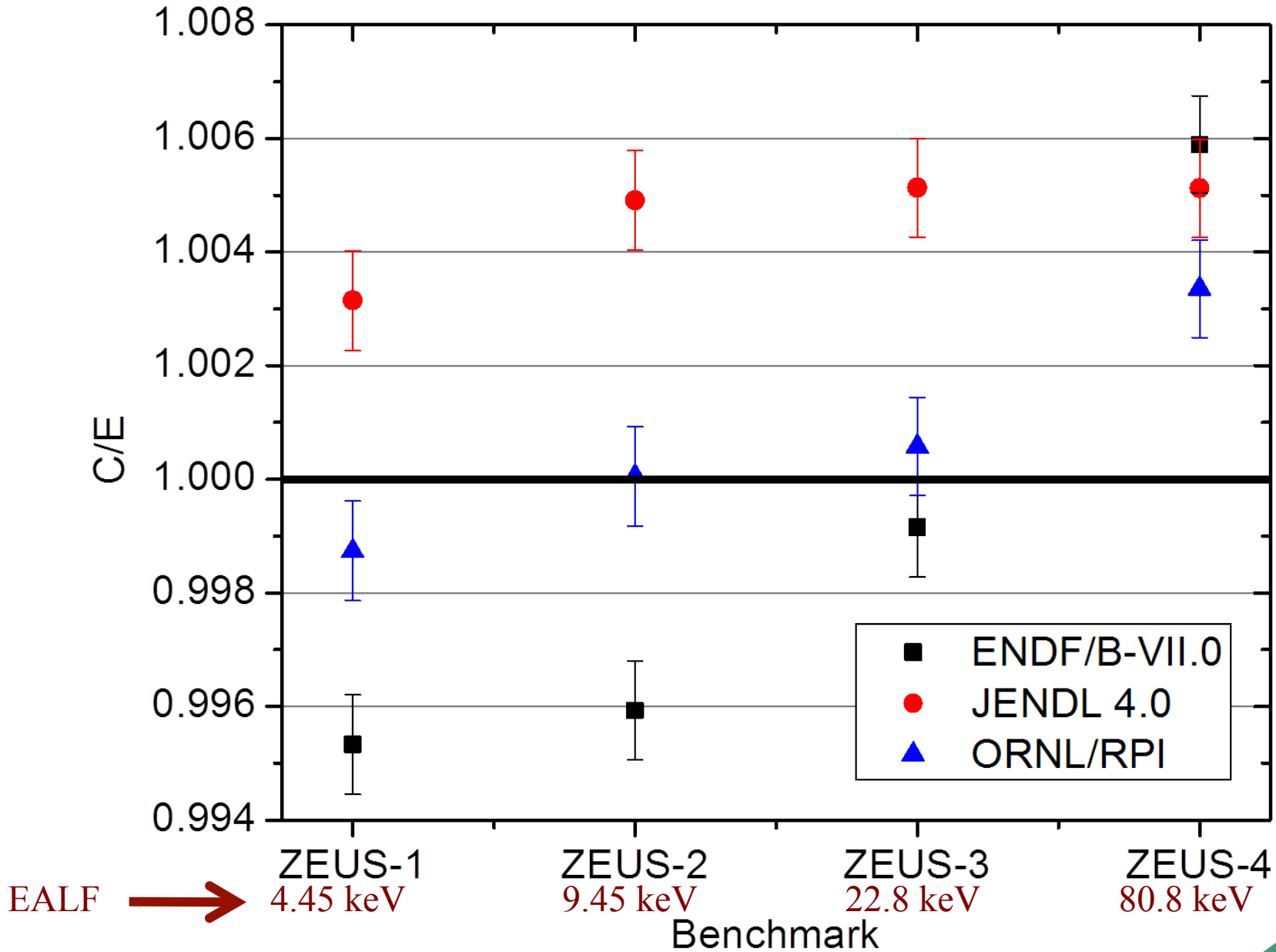




# The HEU-MET-INTER-006 cases (ZEUS)

Case Number	Benchmark $k_{\text{eff}}$	Calculated $k_{\text{eff}}$		
		ENDF/B-VII.0	JENDL4	ORNL
1 (ZEUS1)	0.9977 ± 0.0008	0.99304 ± 0.00035	1.00084 ± 0.00036	0.99644 ± 0.00035
2 (ZEUS2)	1.0001 ± 0.0008	0.99603 ± 0.00035	1.00501 ± 0.00036	1.00015 ± 0.00035
3 (ZEUS3)	1.0015 ± 0.0008	1.00065 ± 0.00035	1.00664 ± 0.00034	1.00208 ± 0.00033
4 (ZEUS4)	1.0016 ± 0.0008	1.00750 ± 0.00031	1.00673 ± 0.00034	1.00496 ± 0.00031

# The HEU-MET-INTER-006 cases (ZEUS)



Case Number	Benchmark Keff	Calculated keff			
		ENDF/B-VII.0	JENDL-4	JENDL4+ORNL	ENDF/B-VII.0+ORNL
HEU Benchmarks					
heu-met-fast-001 (godiva)	1.0000 ± 0.0010	0.99928 ± 0.00025	0.99751 ± 0.00026	0.99753 ± 0.00026	1.00004 ± 0.00027
heu-met-fast-028 (flattop)	1.0000 ± 0.0030	1.00320 ± 0.00030	0.99918 ± 0.00029	0.99886 ± 0.00029	1.00241 ± 0.00030
heu-met-inter-006-1 (ZEUS1)	0.9977 ± 0.0008	0.99304 ± 0.00035	1.00084 ± 0.00036	0.99644 ± 0.00035	1.00244 ± 0.00034
heu-met-inter-006-2 (ZEUS2)	1.0001 ± 0.0008	0.99603 ± 0.00035	1.00501 ± 0.00036	1.00015 ± 0.00035	1.00699 ± 0.00034
heu-met-inter-006-3 (ZEUS3)	1.0015 ± 0.0008	1.00065 ± 0.00035	1.00664 ± 0.00034	1.00208 ± 0.00033	1.00907 ± 0.00033
heu-met-inter-006-4 (ZEUS4)	1.0016 ± 0.0008	1.00750 ± 0.00031	1.00673 ± 0.00034	1.00496 ± 0.00031	1.01087 ± 0.00033
heu-sol-therm-013-case-1	1.0012 ± 0.0026	0.99848 ± 0.00026	0.99805 ± 0.00024	0.99771 ± 0.00024	0.99880 ± 0.00045
heu-sol-therm-013-case-2	1.0007 ± 0.0036	0.99745 ± 0.00026	0.99716 ± 0.00027	0.99690 ± 0.00028	0.99712 ± 0.00027
heu-sol-therm-013-case-3	1.0009 ± 0.0036	0.99417 ± 0.00028	0.99382 ± 0.00028	0.99327 ± 0.00028	0.99443 ± 0.00028
heu-sol-therm-013-case-4	1.0003 ± 0.0036	0.99571 ± 0.00030	0.99598 ± 0.00028	0.99501 ± 0.00029	0.99540 ± 0.00028
heu-sol-therm-032 (ORNL10-CSEWG)	1.0015 ± 0.0026	0.99906 ± 0.00017	0.99886 ± 0.00015	0.99894 ± 0.00017	0.99928 ± 0.00016

Case Number	Benchmark Keff	Calculated keff			
		ENDF/B-VII.0	JENDL-4	JENDL4+ORNL	ENDF/B- VII.0+ORNL
LEU Thermal Solution Benchmarks					
leu-sol-therm-002- case-1	1.0038 ± 0.0040	1.00002 ± 0.00025	0.99969 ± 0.00025	0.99905 ± 0.00025	1.00038 ± 0.00028
leu-sol-therm-002- case-2	1.0024 ± 0.0040	0.99594 ± 0.00028	0.99616 ± 0.00029	0.99618 ± 0.00028	0.99480 ± 0.00030
leu-sol-therm-007- case-14	0.9961 ± 0.0009	0.99495 ± 0.00030	0.99508 ± 0.00030	0.99487 ± 0.00031	0.99522 ± 0.00033
leu-sol-therm-007- case-30	0.9973 ± 0.0009	0.99771 ± 0.00031	0.99741 ± 0.00030	0.99744 ± 0.00031	0.99736 ± 0.00029
leu-sol-therm-007- case-32	0.9985 ± 0.0010	0.99579 ± 0.00029	0.99602 ± 0.00029	0.99589 ± 0.00031	0.99649 ± 0.00027
leu-sol-therm-007- case-36	0.9988 ± 0.0011	0.99860 ± 0.00027	0.99864 ± 0.00028	0.99830 ± 0.00028	0.99882 ± 0.00029
leu-sol-therm-007- case-49	0.9983 ± 0.0011	0.99752 ± 0.00028	0.99764 ± 0.00026	0.99716 ± 0.00025	0.99704 ± 0.00027

Case Number	Benchmark Keff	Calculated keff			
		ENDF/B-VII.0	JENDL-4	JENDL4+ORNL	ENDF/B- VII.0+ORNL
LEU Thermal Compound Benchmarks					
leu-com-therm-008- case-1	1.0007 ± 0.0016	1.00118 ± 0.00029	1.00136 ± 0.00029	0.99988 ± 0.00030	1.00134 ± 0.00031
leu-com-therm-008- case-2	1.0007 ± 0.0016	1.00131 ± 0.00030	1.00109 ± 0.00029	1.00036 ± 0.00030	1.00036 ± 0.00029
leu-com-therm-008- case-5	1.0007 ± 0.0016	1.00065 ± 0.00030	1.00064 ± 0.00029	0.99996 ± 0.00030	1.00000 ± 0.00031
leu-com-therm-008- case-7	1.0007 ± 0.0016	1.00029 ± 0.00030	1.00053 ± 0.00029	0.99971 ± 0.00030	1.00070 ± 0.00029
leu-com-therm-008- case-8	1.0007 ± 0.0016	1.00074 ± 0.00030	1.00014 ± 0.00029	0.99883 ± 0.00030	0.99991 ± 0.00030
leu-com-therm-008- case-11	1.0007 ± 0.0016	1.00203 ± 0.00030	1.00175 ± 0.00029	1.00044 ± 0.00030	0.99891 ± 0.00030

# Resonance Evaluation at ORNL



**L. Leal (ORNL)**

**CSEWG, Nov 5-9, 2012**

# $^{239}\text{Pu}$ Resonance Evaluation

## Presence of $^{239}\text{Pu}$ in a Nuclear System

- For a critical (or subcritical) nuclear system the fuel-temperature reactivity coefficient is negative. The presence of  $^{239}\text{Pu}$  can make it positive;
- The  $^{239}\text{Pu}$  resonance at  $\sim 0.3$  eV produces fissions and some capture and therefore increases reactivity;
- As the  $^{239}\text{Pu}$  builds up more fissions are produced leading to a change in the reactivity;
- Determination of the  $^{239}\text{Pu}$  content in the spent fuel and an accurate knowledge of the nuclear data is needed for a safe shipping and cask design;

# $^{239}\text{Pu}$ Resonance Evaluation

## Motivation:

- Existing resonance evaluation divided into three disjoint resonance parameter sets (computer limitations at the time  $\sim 1986$ ) :

$1.0 \times 10^{-5}$  eV - 1 keV, 1 keV - 2 keV, 2 keV - 2.5 keV;

## Issues are:

- Cross section mismatch at the energy boundaries;
- Not easy to generate uncertainty for the whole energy region (zero correlations between energy regions);
- **Solve long standing problem for thermal benchmark;**



## Early Evaluation (Leal/Derrien at ORNL - 2008)

- One single set of resonance parameters covering the energy range:

$1.0 \times 10^{-5}$  eV to 2.5 keV;

- Cross section mismatch at the energy boundaries gone!
- Uncertainty for the whole energy region generated with correlations properly determined!!
- **Does it solve the problem of thermal benchmark?**

## Issues with ORNL Evaluation

- Results of plutonium solution calculations indicate no improvement using the new ORNL evaluation. Longstanding problem persists!!
- In some case the good results from previous  $^{239}\text{Pu}$  evaluation deteriorated;
- Can the problem be solved?
- Efforts from ORNL, LANL and CEA (France)

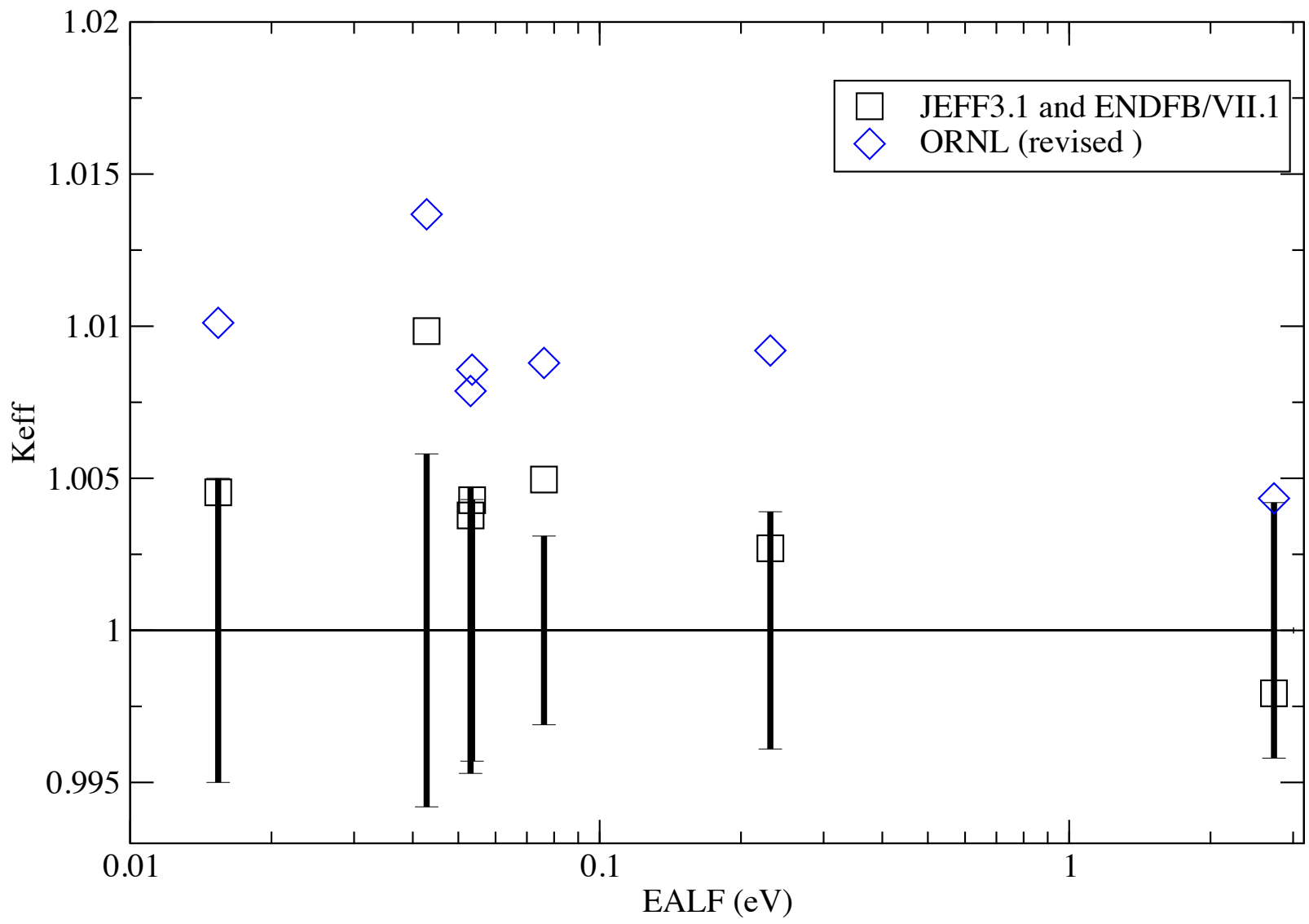
# Integral Benchmark Experiments

- Benchmark from the ICSBEP;
- Plutonium Solution Systems;
- A good choice would be those benchmark experiments spanning the energy region from 0.01 eV to 3 eV
- Choice based on the Energy of Average Lethargy Causing Fission (EALF)

# Benchmark problem from ICSBEP

Benchmark	Experimental <i>K<sub>eff</sub></i>	EALF(eV)	
PST1.4	1.0000 ± 0.0050	0.0154	5 % <sup>240</sup> Pu
PST4.1 (sphere)	1.0000 ± 0.0047	0.0531	5 % <sup>240</sup> Pu
PST12.10 (cubic tank)	1.0000 ± 0.0047	0.0535	25 % <sup>240</sup> Pu
PST12.13	1.0000 ± 0.0047	0.0428	19 % <sup>240</sup> Pu
PST18.1 (cylinder)	1.0000 ± 0.0047	0.0761	43 % <sup>240</sup> Pu
PST34.4 (cylinder)	1.0000 ± 0.0047	0.231	116g Pu/L, 1.42g Gd/L
PST34.15	1.0000 ± 0.0047	2.730	363 g Pu/L, 20.25g Gd/L

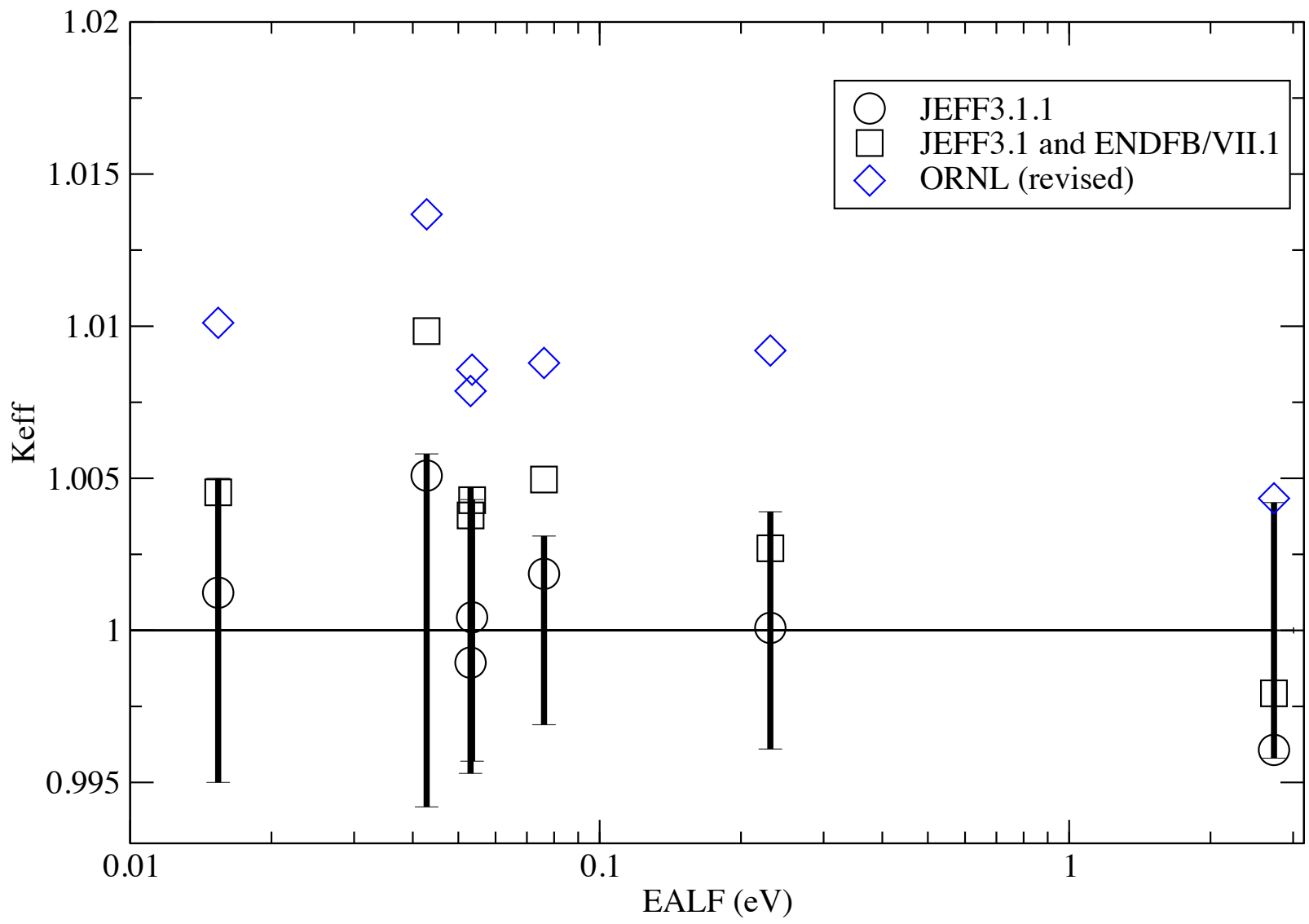
EALF: Energy Average Lethargy Causing Fission



## JEFF3.1.1 Evaluation

(work done at French Atomic Commission/Cadarache)

- Improves substantially prediction of thermal critical systems multiplication factor -  $k_{eff}$ ;
- Work started based on the JEFF3.1 (ENDF/VII.1), that is, the three disjoint sets of resonance parameters;
- Some adjustments to other quantities such as nu-bar;
- **Experimental cross section not well represented;**



# ORNL (USA) and Cadarache (France)

## Work Strategy

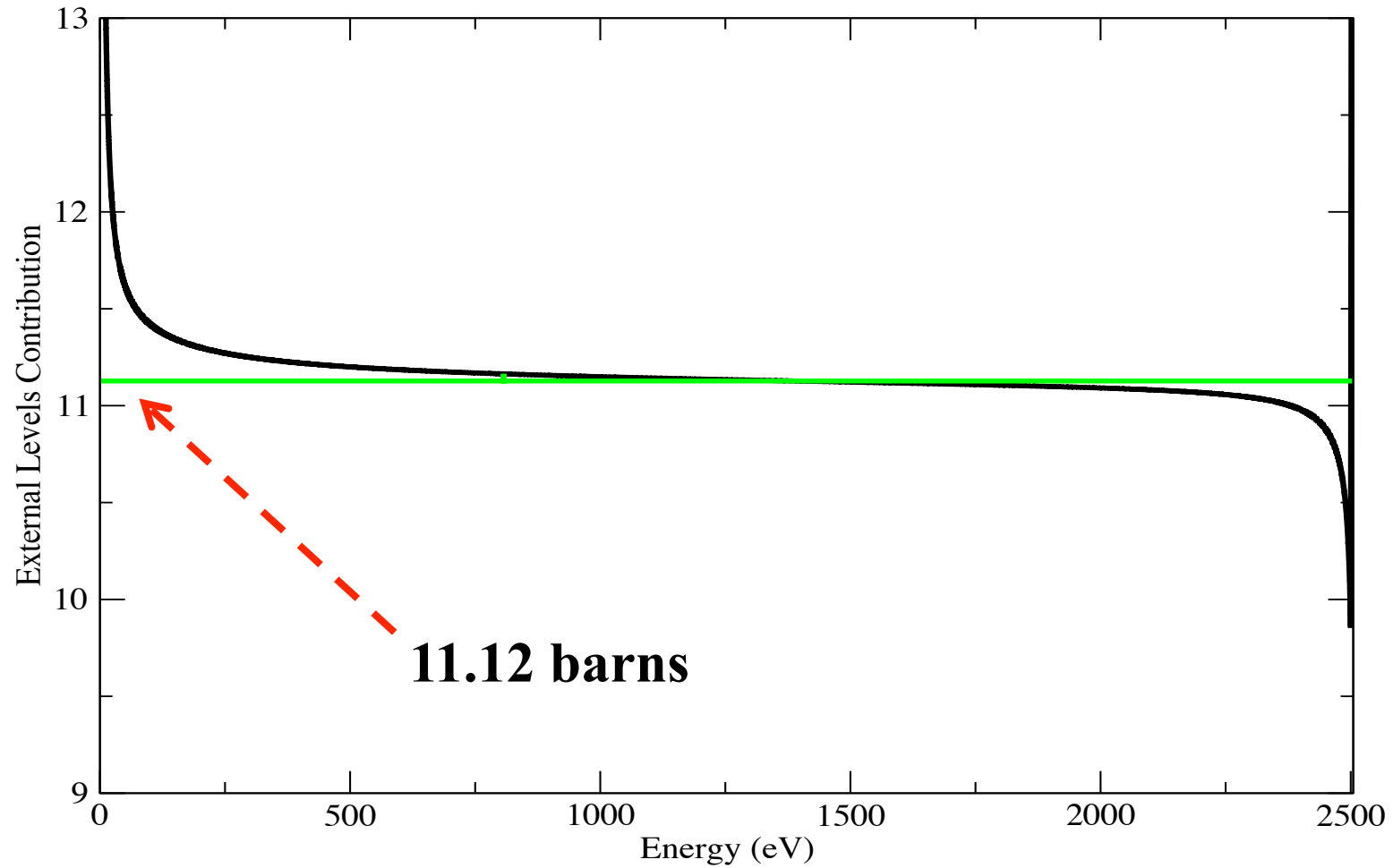
- **Use the SAMMY code to perform resonance analysis using the best selected set of experimental time-of-flight data;**
- **Generate cross-section library with the NJOY code for use in benchmark calculations with the MCNP code;**
- **Generate cross-section library with the GALLILE (NJOY +CALENDF) code for use in benchmark calculations with the MCNP (USA), TRIPOLI and APOLLO French codes;**
- **Use a selected set of experimental benchmarks with average of neutron lethargy causing fission spanning the energy range from 0.01 eV to 3 eV;**
- **Use other benchmarks in addition to the ICSBEP. Examples are the MISTRAL and FUBILA experiments (MOX fuel) performed at the EOLE facility to test the evaluation in France;**



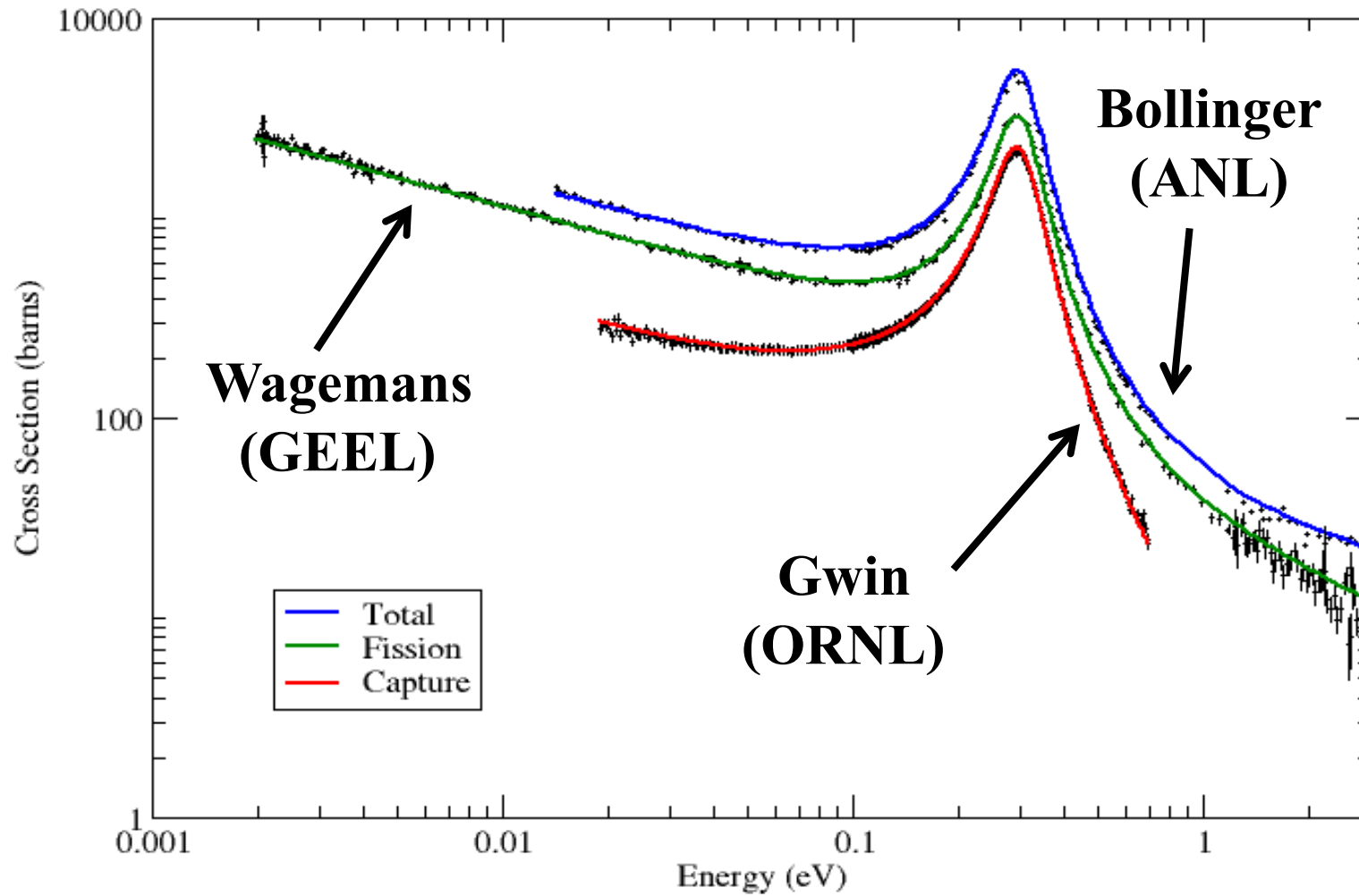
## EXPERIMENTAL DIFFERENTIAL DATA

Reference	Energy Range (eV)	Facility	Measurement
<b>Bollinger et al. (1956)</b>	<b>0.01 – 1.0</b>	<b>Chopper</b>	<b>Total Cross Section</b>
<b>Gwin et al. (1971)</b>	<b>0.01 – 0.5</b>	<b>ORELA</b>	<b>Fission and Absorption at 25.6 m</b>
<b>Gwin et al. (1976)</b>	<b>1.0 – 100.0</b>	<b>ORELA</b>	<b>Fission and Absorption at 40.0 m</b>
<b>Gwin et al. (1984)</b>	<b>0.01 – 20.0</b>	<b>ORELA</b>	<b>Fission at 8 m</b>
<b>Weston et al. (1984)</b>	<b>9.0 – 2500.0</b>	<b>ORELA</b>	<b>Fission at 18.9 m</b>
<b>Weston et al. (1988)</b>	<b>100.0 – 2500.0</b>	<b>ORELA</b>	<b>Fission at 86 m</b>
<b>Weston et al. (1993)</b>	<b>0.02 – 40.0</b>	<b>ORELA</b>	<b>Fission at 18.9 m</b>
<b>Wagemans et al. (1988)</b>	<b>0.002 – 20.0</b>	<b>GELINA</b>	<b>Fission at 8 m</b>
<b>Wagemans et al. (1993)</b>	<b>0.01 – 1000.0</b>	<b>GELINA</b>	<b>Fission at 8 m</b>
<b>Harvey et al. (1985)</b>	<b>0.7 – 30.0</b>	<b>ORELA</b>	<b>Transmission at 18 m</b>
<b>Harvey et al. (1985)</b>	<b>30.0 – 2500.0</b>	<b>ORELA</b>	<b>Transmission at 80 m</b>

# External Levels Determination



# Cross Section Fitting



## Integral Quantities:

- ✓ Benchmark experiments sensitive to the fission and capture cross sections, and also to  $\bar{\nu}$
- ✓ A right combination of capture, fission, and  $\bar{\nu}$  may lead to an improvement on the  $k_{eff}$ ;

Eta and K1 are two important quantities in reactor calculations:

- ✓ Eta( $\eta$ ): six factor form
- ✓ K1: from first-order perturbation theory

Multiplication Factor:  $k_{\infty}$

*Leakage*  $\longrightarrow 0$

*Production*  
*Absorption*

$k_{\infty} \propto \eta = \frac{\nu\sigma_f}{\sigma_a}$

# K1 Factor: first-order perturbation theory

*Reactivity change:  $\delta\rho$*

$$\delta\rho = \frac{\langle \phi^+, \Delta H \phi \rangle}{\langle \phi^+, P \phi \rangle}$$

$\Delta H = \text{Pr oduction} - \text{Absorption}$

*Equivalent K1*


$$K1 = \nu\sigma_f - \sigma_a$$

$$\eta = \frac{\nu\sigma_f}{\sigma_a}$$

and

$$K1 = \nu\sigma_f - \sigma_a$$

**Benchmarks sensitive to K1,  
i.e., the difference:**

**production - absorption**

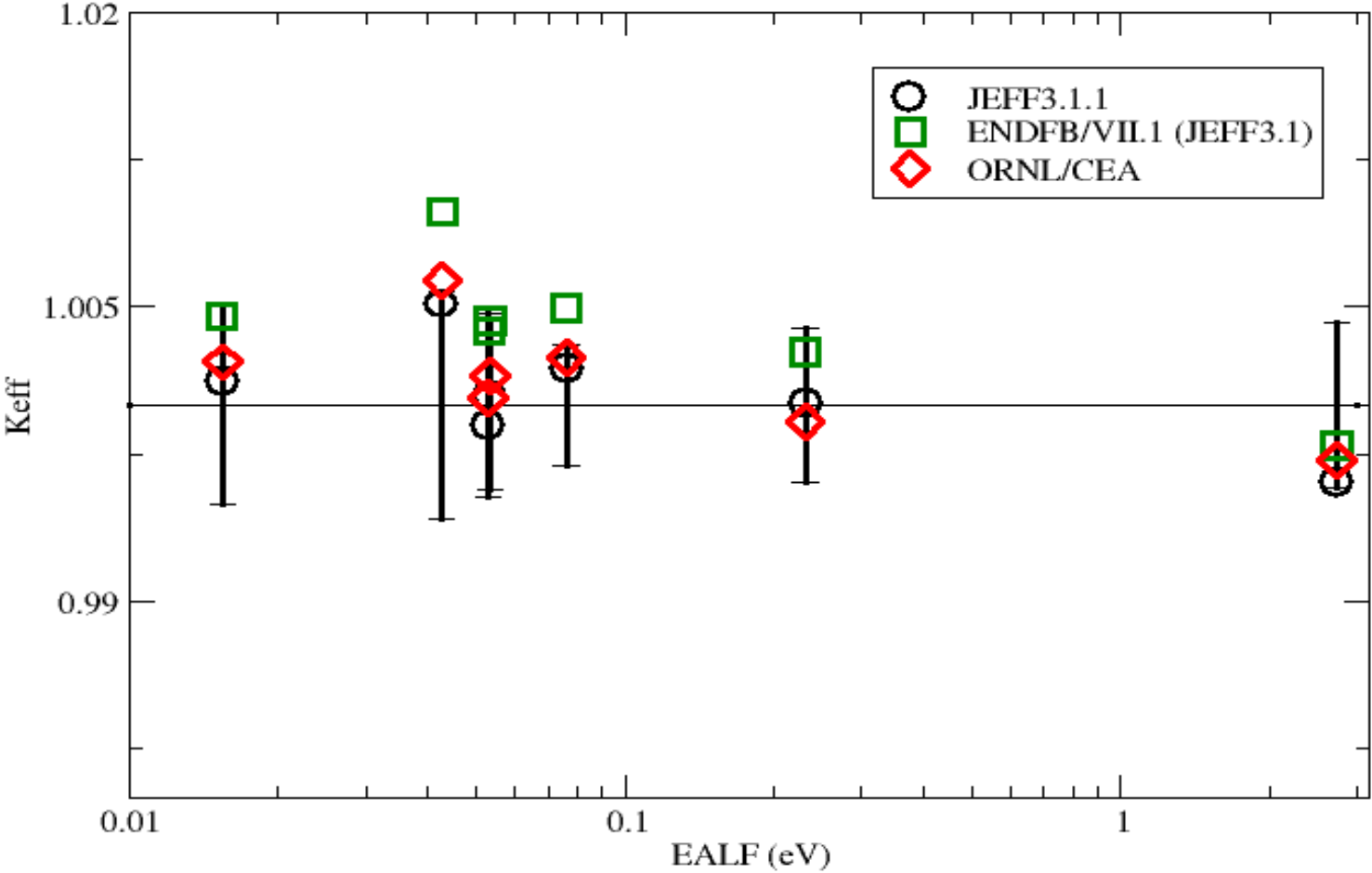
# Thermal values and integral quantities calculated with SAMMY

Quantity	ANR	ENDF/B-VII.1 (JEFF3.1)	JEFF3.1.1	NEW (ORNL/CEA)
$\sigma_\gamma$	$269.3 \pm 2.9$	270.64	272.72	270.06
$\sigma_f$	$748.1 \pm 2.0$	747.65	747.08	747.19
$g_f$	$1.0553 \pm 0.0013$	1.0544	1.0495	1.0516
$g_a$	$1.0770 \pm 0.0030$	1.0784	1.0750	1.0771
$\bar{\nu}$	$2.879 \pm 0.006$	2.873	2.873	2.873
$I_\gamma$	$180 \pm 20$	181.44	181.50	180.09
$I_f$	$303 \pm 10$	302.60	303.58	309.09
$K1$	1177.25	1166.62	1156.35	1161.30

## ANR: Atlas of Neutron Resonance



# ICSBEP Benchmark Results (everything else from BVII.1)



## ORNL Resonance Evaluations and deliverables

	Energy Range	Resonance Covariance Evaluation	Target date for delivery the evaluation
<b><math>^{63}\text{Cu}</math></b>	Thermal to 300 keV	Yes	July FY2014
<b><math>^{65}\text{Cu}</math></b>	Thermal to 300 keV	Yes	July FY2014
<b><math>^{182}\text{W}</math></b>	Thermal to 10 keV	Yes	FY2014
<b><math>^{183}\text{W}</math></b>	Thermal to 5 keV	Yes	FY2014
<b><math>^{184}\text{W}</math></b>	Thermal to 10 keV	Yes	FY2014
<b><math>^{186}\text{W}</math></b>	Thermal to 10 keV	Yes	FY2014
<b><math>^{56}\text{Fe}</math></b>	Thermal to 2 MeV	Yes	FY2014
<b><math>^{239}\text{Pu}</math></b>	Thermal to 2.5 keV	Use ENDF/B-VII.1 (FILE33)	FY2012
<b><math>^{235}\text{U}</math></b>	Thermal to 2.25 keV	Use ENDF/B-VII.1 (FILE33)	FY2013