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LAPH: A Multigroup Photon Production Matrix  
and Source Vector Code for ENDF/B

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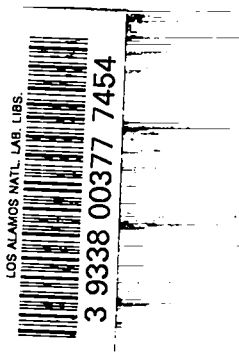
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Donald J. Dudziak  
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ABSTRACT

The LAPH code retrieves photon production cross sections or photon production multiplicities and corresponding neutron interaction cross sections from ENDF/B (Evaluated Nuclear Data File/B). It then applies suitable weighting functions over G specified photon groups and N specified neutron broad groups to construct a G x N photon production matrix. Pointwise cross sections are first integrated over each photon energy group with constant or direct energy weighting, and then over each neutron fine group with constant weighting. Within each neutron broad group, arbitrary fine-group weighting functions are read from input. Resonance fine-group interaction cross sections and weighting functions are also read as input; at the Los Alamos Scientific Laboratory (LASL), these cross sections and weights are produced directly by a modification of the MC<sup>2</sup> code. Macroscopic photon production and photon energy production matrices are then computed. As an option, spatially dependent photon source vectors for transport calculations can be generated by using input scalar neutron flux vectors. Multiple zones can be accommodated with separate weighting functions for each zone. Different materials and reaction types for which photon production matrices are desired can be specified for each zone. Input is in DTF-IV format, and output photon source vectors are also in this format. A sample problem is included along with an indexed listing of the code. The code is written in FORTRAN IV for a CDC-6600 computer with a 65k<sub>10</sub> memory.

I. INTRODUCTION AND SUMMARY

A national neutron data file now exists at the National Neutron Cross Section Center, Brookhaven National Laboratory, in a single format.<sup>1,2</sup> The file, called the Evaluated Nuclear Data File/B (ENDF/B), contains primarily neutron interaction cross sections, angular distributions, secondary energy distributions, thermal scattering laws, and other data of interest in reactor core neutronics analysis. Recently, however, with the expansion of the ENDF/B format to provide for photon production and photon interaction data,<sup>2</sup> the file is becoming increasingly important and useful in shield analysis and design. Included in the shielding interests are weapons and civil defense problems, as well as reactor shielding.

The ENDF/B data file is of real significance only when considered as part of what will be called the "ENDF/B system," which consists of not only the data file but also the data retrieval, checking, and processing codes. For neutron interaction data (ENDF/B Files 2 through 7), such codes are presently available in varying degrees of development, and the data are actually being extracted for use in neutronics calculations, such as transport, thermalization, and fast spectra problems. The photon files (14 through 16 and 23 through 27), however, are in their infancy with evaluated photon production data for only six materials<sup>3,4</sup> (sodium, magnesium, silicon, chlorine, potassium, and calcium) presently available in the ENDF/B format, and even these data have not been through a complete data testing procedure. Because of this, the publicly

released ENDF/B data file of 1969 contained no photon production data. One obvious requirement for checking the photon data in an integral manner, as well as a clear incentive for evaluators to place these data in the file, is to have a code to retrieve the data in a usable form for multigroup photon transport calculations. These are two motivations for the LAPH code.

Throughout this report, it is assumed that the reader is familiar with the ENDF/B system, since LAPH operates only within that system. Detailed descriptions of the data formats are given in the references cited above, and a review of the storage and retrieval of photon data in the ENDF/B system has been presented elsewhere.<sup>5</sup> Pertinent format information will be reviewed here as required, however.

Briefly, the LAPH code retrieves photon production cross sections or multiplicities and corresponding neutron interaction cross sections from the ENDF/B data file, applies suitable weighting functions over  $N$  specified neutron groups and  $G$  specified photon groups, and constructs a  $G \times N$  photon production matrix. As an option, it operates on this matrix with flux vectors from a neutronics code, as well as with scalar multipliers such as atom number densities and effective photon group energies, to directly provide spatially dependent photon source terms for transport calculations. Figure 1 presents a schematic description of the code, where the input data are left of the dotted line. This schematic diagram is not intended to present the detailed logic of the code, which is given in Appendices A and B.

## II. THEORY

### A. Photon Production Data Format in ENDF/B

To understand the process of computing photon production matrices and photon source functions from the ENDF/B data file (the process is loosely called "theory"), it is helpful to review the form in which the data are received into LAPH; i.e., the form in which they are stored in the ENDF/B data file. Photon multiplicities are entered into ENDF/B File 15 in one of two options,<sup>2</sup> either directly in a manner analogous to File 5 or as transition probability arrays.

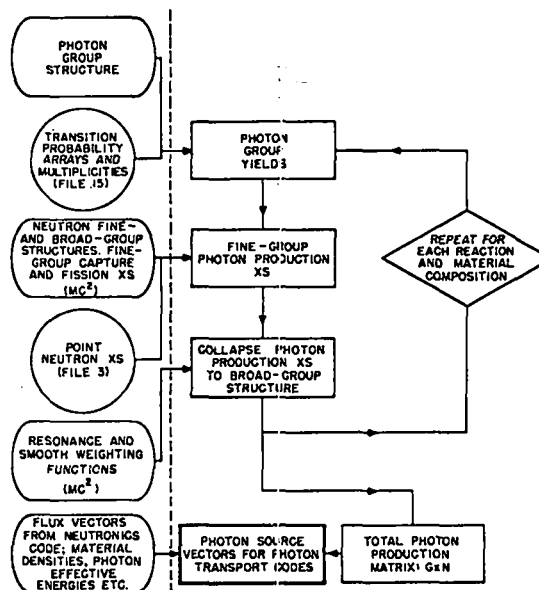


Fig. 1. LAPH code schematic.

Under Option 1 of File 15, the multiplicities are given by a normalized photon energy distribution and an associated total photon yield (units of photons) for an interaction. Normalized photon energy distributions are given according to allowable laws, of which two are presently instituted: viz., (Law 1) a tabulated probability density function vs photon energy, or (Law 2) a Dirac delta function in photon energy. In addition, the tabulated function (Law 1) is a function of incident neutron energy; hence, a two-dimensional table is used for tabulated probability functions. For either law, the yields are tabulated functions of incident neutron energy. New laws may be added later when deemed necessary; e.g., a normalized prompt fission-gamma spectrum may be useful.

For Option 2, a level is identified by a level sequence number and level energy. The only additional data (other than a few control parameters) needed to specify the photon energies and yields are (1) the nonzero transition probabilities to lower levels, (2) the gamma transition conditional probabilities if nonunity, and (3) the energies of the lower levels. These data are entered as doublets or triplets for each transition, depending

upon whether or not the conditional probabilities are unity. Thus, processes such as internal conversion can be accounted for very simply. Also, data listed for any level include only those for photons originating at the level. Further cascading is determined from the data for lower levels, so only the minimum required data are stored in the ENDF/B system. The LAPH code reconstructs the cascade.

An important limitation of the transition probability arrays is that they cannot be used to accurately predict photon production by neutrons at energies appreciably above that of the highest level for which the gamma decay scheme is well known. The reason for this is that, at higher energies, levels above the one for which the decay scheme is well known may be excited and cascade through lower levels. Thus, at these higher energies, the photon production must be accounted for under Option 1. In fact, LAPH will not use the transition probability arrays to calculate photon production at neutron (center of mass) energies above the highest level in the arrays; i.e., if  $ES_{\max}$  is the highest level energy for which a transition probability array is given, no photon production will be calculated from the arrays for incident-neutron energies above  $ES_{\max} \times \frac{AWR + 1}{AWR}$ , where AWR is the atomic weight ratio.

In ENDF/B data files<sup>4</sup> for sodium, magnesium, chlorine, potassium, and calcium (used for debugging purposes), the photon production at these higher energies was placed in a photon production reaction which was assigned MT = 110. A unit cross section was placed in File 3 for MT = 110, and the photon production cross sections (in barns) to produce a discrete photon of a given energy were placed in the yield table of File 15, Option 1, LF = 2.

The units for data stored in the ENDF/B file are:

Quantity	Units
energy	eV
angle	dimensionless cosine
cross section	barns
photon yields	photons

## B. Photon Yields and Photon Production Cross Sections

Photon yields are either given directly as a function of neutron energy in Option 1 of File 15 or must be constructed by processing codes (including LAPH) from the transition probability arrays of Option 2. The construction process for a microscopic photon production cross section in the latter case is discussed in Appendix B of Ref. 2 (the general equation on p. 51 of Ref. 2 should have the variable TP substituted for A in all of the summations). For completeness, the discussion will be reviewed. Define

- $\sigma_{j,i}(E)$  = cross section to produce the photon which arises from decay of level j to i, with incident-neutron energy E.
- $\sigma_k(E)$  = neutron cross section for inelastic scattering to level k, for incident-neutron energy E.
- $TP_{j,i}$  = probability of a direct transition from level j to level i,  $i < j$ .
- $GP_{j,i}$  = conditional probability of photon emission in a direct transition from level j to level i,  $i < j$ .
- $A_{j,i} = (TP_{j,i})(GP_{j,i})$ .
- $ES_i$  = energy of level i.

Note that the photon production cross section is given for transition between specific levels, which implicitly determines the photon energy, rather than for a given photon energy. This scheme avoids ambiguity when two different transitions produce photons of the same energy. The photon energy is simply  $E_\gamma = ES_j - ES_i$ .

For the general case, all possible transitions must be considered, as well as the possibility of transitions not involving gamma-ray emission. Accounting for all possibilities leads to the expression given in Ref. 2, p. 51, viz.,

$$\sigma_{j,i}(E) = A_{j,i} \sum_{m_0=j}^N \sigma_{m_0} \prod_{\ell=1}^{n+1} \prod_{m_\ell=j}^{m_{\ell-1}-1} TP_{m_{\ell-1},m_\ell} \quad (1)$$

where  $N$  = highest level such that  $ES_N \leq E \frac{AWR}{AWR + 1}$ . The requirement that  $m_n \leq j + 1$  determines the range of the index n, and  $(m_{\ell-1} - 1) > j$  is implicit.

This pointwise photon production cross section can then be written in the notation of Ref. 2 as  $\sigma(E_Y + E)$  for discrete photon energy  $E_Y = ES_j - ES_i$ . Recall that this construction scheme using Option 2 of File 15 does not apply at incident neutron energies  $E > ES_{\max} \times \frac{AWR + 1}{AWR}$ . The energy  $ES_{\max}$  is found by searching for the largest MT number in the set  $\{5 \leq MT \leq 14 \text{ or } 51 \leq MT \leq 80\}$ , and reading  $ES$  for that MT value.

Under Option 1 of File 15, the photon yield functions are first constructed from the tabulated yield at incident-neutron energy  $E$ , and a normalized photon energy distribution (which may be delta function in  $E_Y$ ). These two components can be given for different photon distribution laws as subsections of one reaction type (MT number). Specifically, if  $y_k(E)$  is the yield from subsection  $k$ , and  $f_k(E_Y + E)$  is the corresponding normalized photon energy distribution, the yield function is given by

$$y(E_Y + E) = \sum_{k=1}^{NK} y_k(E) f_k(E_Y + E) \quad (2)$$

(photons/eV).

The  $y_k(E)$  have units of photons, and the  $f_k(E_Y + E)$  have units of  $eV^{-1}$ . Having the yield function, the pointwise differential photon production cross section is determined as

$$\frac{d\sigma(E_Y + E)}{dE_Y} = \sigma(E) y(E_Y + E) \quad (3)$$

(b-photons/eV),

where  $\sigma(E)$  is the interaction cross section for the appropriate reaction type from Files 2 and 3.

Once the differential photon production cross sections are determined, they are integrated over arbitrary neutron and photon energy groups, with selected appropriate weighting functions, to determine a photon production cross-section matrix. In the discussion below, the subscripts and superscripts are defined as follows:

- $g$  = photon energy group,  $g = 1, 2, \dots, G$
- $\ell$  = neutron fine group,  $\ell = 1, 2, \dots, L$
- $n$  = neutron broad group,  $n = 1, 2, \dots, N$

- $k$  = partial yield index,  $k = 1, 2, \dots, NK$
- $p$  = reaction type (MT number)
- $i$  = material number
- $j$  = zone number,  $j = 1, 2, \dots, IZM$
- $m$  = spatial mesh interval,  $m = 1, 2, \dots, IM$
- $r$  = resolved resonance component
- $s$  = unresolved-resonance and smooth components.

The lower energy limit of a group is denoted by  $E_g$ ,  $E_{\ell}$ , or  $E_n$ . The indices  $i$  and  $j$  will be suppressed for a while to avoid too clumsy a notation, but they are implicit.

Two weighting options, called tracks, are available to compute the photon yield in a group,  $g$ , as follows:

Track 1 is a constant weighting, i.e.,

$$Y_g^P(E) = \int_{E_g}^{E_{g+1}} dE_Y Y^P(E_Y + E) \quad (4)$$

(photons),

where  $Y^P(E_Y + E)$  may be a Dirac delta function. On this track, the photon group energy yield,  $\bar{Y}_g^P(E)$ , is computed by using an arbitrary group effective energy,  $\bar{E}_g$ , which is an input quantity. However, the code still calculates the energy-weighted yield on Track 2 and provides the user with a listing of the average (yield-weighted) energy,  $\bar{E}_g^P$ , in each group. In effect, on Track 1, the photon energy yield is

$$\bar{Y}_g^P(E) = Y_g^P(E) \bar{E}_g \quad (5)$$

(eV).

If a value of  $\bar{E}_g$  is not in the interval  $[E_g, E_{g+1}]$ , the code will assume the median group energy,  $\bar{E}_g = \frac{1}{2}(E_g + E_{g+1})$ , and proceed with this calculated value vice the input value.

Track 2 is an energy-weighted yield, i.e.,

$$\bar{Y}_g^P(E) = \int_{E_g}^{E_{g+1}} dE_Y Y^P(E_Y + E) E_Y \quad (6)$$

(eV),

and

$$Y_g^P(E) = 2 \left[ \bar{Y}_g^P(E) \right] \left[ \frac{E_{g+1} + E_g}{2} \right]^{-1} \quad (7)$$

(photons).

The calculation in Eq. 6 is also performed on Track 1, where the average energy in each group is computed by

$$\bar{E}_g^P = \frac{\int_{E_g}^{E_{g+1}} dE_Y Y^P(E_Y + E) E_Y}{\int_{E_g}^{E_{g+1}} dE_Y Y^P(E_Y + E)} \quad (\text{eV}). \quad (8)$$

The photon energy group structure is arbitrary, and is specified by an input energy mesh, starting at the highest energy. Likewise, the neutron energy group structures are arbitrary, except that the fine-group energy mesh points must have the broad-group mesh points as a subset. In practice, the neutron group structures are usually the corresponding structures in a spectrum-averaging code such as MC<sup>2</sup>. In fact, a version of the MC<sup>2</sup> code<sup>6</sup> has been modified to output pertinent portions of the LAPH input. The photon energy mesh for the integrations on Tracks 1 and 2 is the overlay of the photon group energy mesh and the E<sub>Y</sub> mesh for the f<sub>k</sub>(E<sub>Y</sub> + E) in File 15. The simple trapezoidal rule is used for the integration. The Y<sub>g</sub><sup>P</sup>(E) are evaluated at every tabulated neutron energy in File 15.

There is one approximation inherent in using data for a continuous photon spectrum. For any incident-neutron energy E, between two neutron energies E<sub>1</sub> and E<sub>2</sub> at which photon energy distributions are tabulated, there may be a component of the photon distribution up to energy E<sub>2</sub> + Q. Here, Q has its usual meaning--the reaction energy. Thus, photons can be constructed at energies greater than E + Q (the theoretical maximum) from this interpolated energy distribution. This problem occurs for any interpolation scheme between incident-neutron energies, and minimizing the induced error depends upon the evaluator having entered the data in the ENDF/B file with a fine enough incident-neutron energy mesh. (The same problem occurs for secondary neutron distributions in ENDF/B File 5.)

Having averaged the yields over each photon group, the averaging over each neutron fine group proceeds along one of two tracks. The track used is determined by a combination of the reaction type (MT) number and by an input option. Briefly, for fission and capture (MT = 18 and = 102), respectively,

the cross-section averaging over a neutron fine group may be performed in the resonance region by a spectrum-averaging code, or the resonance parameters may be ignored (or be nonexistent) and all cross-section averaging will be done internally by LAPH.

Track A, which is always used except possibly for fission and capture, uses a constant weighting over a neutron fine group to calculate the photon production cross section,  $\bar{\tau}_{g,\ell}^P$ , as follows:

$$\bar{\tau}_{g,\ell}^P = (\Delta E_\ell)^{-1} \int_{E_\ell}^{E_{\ell+1}} dE \sigma^P(E) Y_g^P(E) \quad (9)$$

(b-photons),

where  $\Delta E_\ell = E_{\ell+1} - E_\ell$ , and  $\sigma^P(E)$  is the neutron interaction cross section for reaction type p (from ENDF/B File 3). The photon energy production cross section is, similarly,

$$\bar{\tau}_{g,\ell}^P = (\Delta E_\ell)^{-1} \int_{E_\ell}^{E_{\ell+1}} dE \sigma^P(E) \bar{Y}_g^P(E) \quad (10)$$

(b-eV).

Track B, which is used only for fission and capture and only then if this track is chosen by the input option, uses input values of the cross section averaged over the neutron fine group, as follows:

$$\rho_{g,\ell}^{P,r} = (\Delta E_\ell)^{-1} \bar{\sigma}_\ell^{P,r} \int_{E_\ell}^{E_{\ell+1}} dE Y_g^P(E) \quad (11)$$

$$\rho_{g,\ell}^{P,s} = (\Delta E_\ell)^{-1} \bar{\sigma}_\ell^{P,s} \int_{E_\ell}^{E_{\ell+1}} dE Y_g^P(E)$$

(b-photons),

where p = 18 or = 102. Here  $\bar{\sigma}_\ell^P$  is the cross section averaged over group  $\ell$  by a spectrum-averaging code, while  $\rho_{g,\ell}^P$  denotes the photon production cross section (resonance, or smooth plus unresolved resonance). Similarly,

$$\bar{\rho}_{g,\ell}^{P,r} = (\Delta E_\ell)^{-1} \bar{\sigma}_\ell^{P,r} \int_{E_\ell}^{E_{\ell+1}} dE \bar{Y}_g^P(E) \quad (12)$$

$$\bar{\rho}_{g,\ell}^{P,s} = (\Delta E_\ell)^{-1} \bar{\sigma}_\ell^{P,s} \int_{E_\ell}^{E_{\ell+1}} dE \bar{Y}_g^P(E)$$

(b-eV).



This track normally would not be used, for example, if resonance data were not given in ENDF/B File 2 for the materials considered. If it is used, it must be used over the entire neutron energy range, i.e., both tracks cannot be used for a given reaction. Also, the same track must be used for both fission and capture.

The above integrations on Tracks A and B are performed by the trapezoidal rule, using a mesh determined by the overlay of the fine-group energy mesh and the cross-section mesh in File 3.

Having computed the photon production cross-section elements for the neutron fine-group structure, it remains to find a weighted average over the broad groups. These broad groups would normally correspond to the groups used in a neutron transport calculation from which the fluxes are obtained for use in determining the photon source. Weighting of the fine-group photon production cross sections is done with arbitrary sets of input weights, one set for the smooth cross sections and one for the resonance cross sections. The latter set, of course, is used only if Track B is chosen. In practice, the smooth cross-section weights are usually the fine-group fluxes from an infinite medium (zero-dimensional), one-dimensional, or other appropriate spectrum. Also, the resonance weights are usually those from the same spectrum-averaging code. At LASL, both sets of weights are output by the modified MC<sup>2</sup> code referred to above. Denoting the smooth weights by  $w_{\ell}^s$  and the resonance weights by  $w_{\ell}^r$ , the elements of the G x N microscopic photon production matrix for reaction type p are

$$\sigma_{g,n}^p = \left[ \sum_{\ell \in n} \tau_{g,\ell}^p w_{\ell}^s \right] \left[ \sum_{\ell \in n} w_{\ell}^s \right]^{-1} + \left[ \sum_{\ell \in n} \rho_{g,\ell}^{p,r} w_{\ell}^r \right] \left[ \sum_{\ell \in n} w_{\ell}^r \right]^{-1} + \left[ \sum_{\ell \in n} \rho_{g,\ell}^{p,s} w_{\ell}^s \right] \left[ \sum_{\ell \in n} w_{\ell}^s \right]^{-1}, \quad (13)$$

and analogous elements  $\sigma_{g,n}^p$  for the energy production matrix. In the calculation of  $\sigma_{g,n}^p$ , the code

actually performs the calculation differently from the direct way shown in Eq. (13) by normalizing the weights ahead of time.

Though it is not explicitly indicated in the notation, these cross sections are determined by LAPH for materials in all the specified spatial zones of the problem. Options are available, however, to specify for each zone those materials for which photon production cross sections are desired and for each material to specify which reaction types are to be included in the calculation of the photon production cross sections. A problem arises for materials for which data are given for both total inelastic scattering (MT = 4) and for the individual levels and continuum (MT = 5 through 15, and 51 through 80). If the specific reaction types to be used by LAPH are explicitly given as input, there is no problem. However, under the flag MT = -1 (see discussion of input in Sec. III), which loosely means use all MT numbers for which photon production data are given in File 15, the code must make a decision concerning inelastic scattering. If photon production data are given in File 15 for MT = 4, it chooses to use these data only if data are not given for any MT in  $\{5 \leq MT \leq 15 \text{ or } 51 \leq MT \leq 80\}$ . Thus, when data are given for one or more of the individual levels and the user prefers to use the data in MT = 4, he must explicitly list the MT numbers desired. The flag MT = 0 means to ignore photon production from this material, and the material need not appear on the input ENDF/B data tape.

Given the set of reaction types, {MT}, for which photon production cross sections are desired, the total microscopic photon production cross-section matrix of material i is given by

$$[\sigma_{g,n}]_i = \left[ \sum_{p \in \{MT\}} \sigma_{g,n}^p \right]_i \equiv \sum_{p \in \{MT\}} [\sigma_{g,n}]_{i,p} \quad (\text{b-photons}), \quad (14)$$

where the subscript i, which has always been implicit in  $\sigma_{g,n}^p$ , is no longer suppressed. The energy production matrix  $[\tilde{\sigma}_{g,n}]_i$  has an analogous definition. When either matrix is used below, the subscripts g and n will be suppressed unless desired for clarity.

In photon source calculations, the quantity usually of more interest than the microscopic photon production matrix,  $[\sigma]_i$ , is the macroscopic matrix given by

$$[\Sigma]_{i,j} = A_{i,j}[\sigma]_i \quad (\text{photons/cm}), \quad (15)$$

where the scalar  $A_{i,j}$  is the number density of the  $i$ th material in the  $j$ th region (units of  $b^{-1}\text{-cm}^{-1}$ ). In all the following discussions, it is implicit that an exactly analogous development applies to the energy production matrix.

### C. Spatially Dependent Photon Sources

To determine a spatially dependent photon source from the macroscopic photon production matrix, an appropriate flux vector must be known. Denoting this  $N$ -dimensional (column) vector by  $[\phi(\vec{r})]_N$ , where  $\vec{r}$  symbolizes the spatial dependence, the photon source vector is given by

$$[\hat{S}(\vec{r})]_G = [\Sigma]_{G \times N} [\phi(\vec{r})]_N \quad (16)$$

(photons/cm<sup>3</sup>-sec).

In practice, the multigroup flux vectors  $[\phi(\vec{r})]$  are calculated at discrete mesh intervals,  $\Delta r_m$ , and usually in one dimension (e.g., by the DTF-IV code<sup>7</sup>). Also, the fluxes are usually calculated for an arbitrarily normalized neutron source term, so the eigenfunctions generally require a re-normalization factor,  $C$ , to account for the actual reactor power. The source is then given by

$$[S]_{i,m,p} = C[\Sigma]_{i,m,p}[\phi]_m, \quad (17)$$

where  $j$  is implicitly determined by  $m$ . For most applications, the source vector of interest for a photon transport calculation is

$$[S]_m = C \left[ \sum_i \sum_p \Sigma_{i,m,p} \right] [\phi]_m \quad (18)$$

(photons/cm<sup>3</sup>-sec),

and its energy production analog  $[\tilde{S}]_m$  (eV/cm<sup>3</sup>-sec). These source terms are listed under some output options by photon group at each mesh interval. Also, as an option, they may be output in formats suitable for the DTF-IV (photon transport) code.

## III. INPUT INSTRUCTIONS

### A. Background

Input to LAPH is generally in the DTF-IV format system, with the exception of the title and parameter cards at the beginning of the data. The DTF-IV system consists of a basic 12-column field, but the first three columns are reserved for a control flag, and the remaining nine columns are a data field. There are seven possible controls in the first column of the three-column subfield as follows:

0 or blank = normal input; the nine columns for data are read in normal FORTRAN E, F, or I format.

1 = repeat; the number in the data field is repeated the number of times specified by the integer NN in the second and third columns of the control field.

2 = interpolate; the number of interpolates, NN, specified in the second and third columns of the control field are placed between the number in the data field and the number in the succeeding data field.

3 = terminate; ends the data block--each data block must have this flag at the end.

4 = fill remainder of data block with the number in the data field.

5 = repeat the number in the data field 10\*NN times.

9 = skip to next card.

Whether the data in the data field is integer or real is indicated by the first letter of the block name in the usual FORTRAN tradition.

A problem regarding terminology arises for LAPH when using DTF-IV input along with ENDF/B input, because the term material has a different meaning in each case. No completely satisfactory resolution was found, but by sacrificing purity for consistency, the term material in DTF-IV has been replaced by the term nuclide, which is consistent with the usage in MC<sup>2</sup>, another code which is linked to LAPH. Also departing from DTF usage, "nuclide" does not include a mixture of nuclides. In LAPH, the term material is used strictly in the sense of a MAT in the ENDF/B system.

Units for input should be as follows:

Energy: eV  
 Number density: atoms/b-cm  
 Flux: n/cm<sup>2</sup>-sec  
 Length: cm

The code has many error triggers which will lead to a call to the subroutine ERROR. The type of error encountered will be identified on the output listing by an error number. A brief description of this error can then be found in the comment card in ERROR for the corresponding error number (cf. listing in Appendix B).

**B. Input Data Format**

Data blocks are given in Table I in order of input, preceded by the corresponding variable name in LAPH. For the parameter table, the location (order) of the parameter is given first.

**C. Array Size Restrictions**

To keep the code operable on computers with small-size memories, restrictions must be placed on array sizes. The restrictions are presently as follows:

- NFG ≤ 99
- NBG ≤ 99
- NGG ≤ 49
- IZM ≤ 10
- IM ≤ 100
- MS ≤ 50

**D. Computer Requirements and Running Times**

The LAPH code is presently operational on a CDC 6600 which has 65k<sub>10</sub> memory and uses the full core. It requires no special hardware or software but does use a disk and one magnetic tape, viz., Tape 20 which is the ENDF/B data tape in Mode 3 (BCD card-image format in standard arrangement). The central processor time required for a problem with three regions, six materials, 10 mesh points, 26 neutron groups, and 11 photon groups, including calculation of both photon production matrices and photon source vectors (cf. the sample problem, Sec. III.E) was 3.5 min. All coding is in FORTRAN IV and should be compatible with FORTRAN compilers on other computers.

**E. Sample Problem Input and Output**

A sample problem for an infinite-slab physically unreal shield configuration is included for illustrative purposes. (The problem choice is restricted by the available ENDF/B data.) The shield

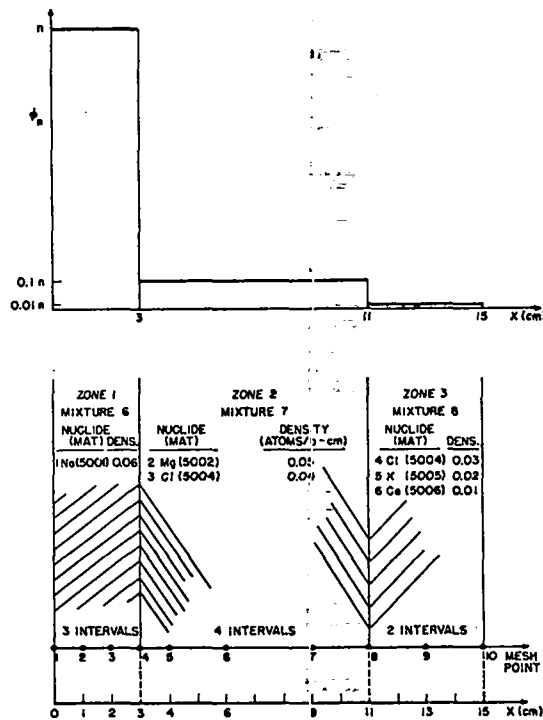


Fig. 2. Sample problem diagram.

configuration and composition are given in Fig. 2, and the corresponding input data are shown in Table II. Photon production from selected reactions was chosen as follows:

	Nuclide	MAT No.	MT Nos.
1	Na	5001	110
2	Mg	5002	102
3	Cl	5004	5+14 and 51+53
4	Cl	5004	0
			(no reactions)
5	K	5005	-1
			(all reactions)
6	Ca	5006	15

In the input for EG(10), there is a deliberate error giving the average gamma energy in the tenth group as 0.07 MeV instead of 0.7 MeV. In this case, the code will replace the value with the group median energy and proceed. This error is flagged in the sample output shown in Table III. Headings for the data blocks on the output listing are self-explanatory. A listing of the complete data deck for the sample problem is shown in Table II.

TABLE I  
INPUT DATA FORMAT

A. Title Card (I6,11A6): Any integer for problem identification, and any BCD information for identification of output.

B. Integer Parameters (I2I6):

<u>Location</u>	<u>Name</u>	<u>Definition</u>
1	NGG	Number of gamma groups.
2	NFG	Number of neutron fine groups.
3	NBG	Number of neutron broad groups.
4	IZM	Number of zones.
5	IM	Number of intervals.
6	MS	Number of mixture specifications (= length of mix tables).
7	MCR	Number of nuclides for which distinct fine-group cross sections and weighting functions are input.
8	MM	Number of reaction types, MT (= length of MT table).
9	NPM	Total number of nuclides plus mixtures.
10	IRES	Special resonance weighting option to be used? (0/1 = no/yes; 0 = Track A, 1 = Track B.)
11	IWØ	= 0, photon effective average energy for each group is input (Track 1). = 1, photon energy weighting function is yield function (Track 2).
12	IØØ	= 0, print $[\sigma_{g,n}]_{i,j}$ for each material i and zone j, and $\sum_i A_{i,j} [\sigma_{g,n}]_{i,j}$ , the macroscopic matrices for each zone j. = 1, print all of Option 0 plus the source vector, $C \sum_i A_{i,j} [\sigma_{g,n}]_{i,j} [\phi]_m$ , at each spatial point m. Note that m determines j. = 2, print all of Option 1 and punch the DTF-IV input source cards (cf. discussion of DTF-IV option). = 3, print only the matrix $\sum_i A_{i,j} [\sigma_{g,n}]_{i,j}$ for each zone j, along with the source vector $C \sum_i A_{i,j} [\sigma_{g,n}]_{i,j} [\phi]_m$ . = 4, print all of Option 3 and punch the DTF input source cards. = 10, same as IØØ = 0, substituting the energy production matrices $[\tilde{\sigma}_{g,n}]_{i,j}$ , etc. = 11, " " = 1, " " " " = 12, " " = 2, " " " " = 13, " " = 3, " " " " = 14, " " = 4, " " " " = 20, do both Options 0 and 10 (i.e., print both photon production and photon energy production matrices). = 21, do both Options 1 and 11. = 22, " " " 2 and 12. = 23, " " " 3 and 13. = 24, " " " 4 and 14.

[Note: The 2X series of output options requires an insignificant addition to the central processor time compared to the X or 1X series.]

TABLE I (continued)

C. Data Blocks (DTF-IV system): Dimension of variable is given if it is predetermined.

Name and Dimension	Definition
C(1)	Renormalization constant for $[\phi]$ .
NMAT(IZM)	Number of materials in each zone for which photon production cross sections are desired.
NNM(2*MCR)	Nuclide sequence numbers (for mix table) and corresponding material (MAT) numbers, in successive pairs.
MZT(MCR)	For each MAT number in the NNM block, MZT is the number of values of MT to be entered in the next (MTN) block.
MTN(MM)	MT numbers for each MAT number given in the NNM block. MT = -1 means use all MT numbers for which photon production data exist in File 15, except possibly MT = 4 (cf. Sec. II.B). MT = 0 means calculate no photon production for this material.

If, and only if,  $IW\emptyset = 0$ , the following data block appears:

EG(NGG) Effective average energy,  $\bar{E}_g$ , for each gamma group. [Same for all materials and reaction types. Code checks that  $E_{g-1} < \bar{E}_g < E_{g+1}$ ]

EMG(NGG+1) Gamma group energy mesh, in decreasing magnitude of energy.

The following eight data blocks will normally be punched by MC<sup>2</sup>.

EMNF(NFG+1) Neutron fine-group energy mesh, in decreasing magnitude of energy.

EMNB(NBG+1) Neutron broad-group energy mesh, in decreasing magnitude of energy.

One set of the following six data blocks for each zone. Each block is preceded by a title card in 12A6 format.

LOOP ON ZONES [IZM]	LOOP ON MAT'S [NMAT(IZM)]	RXSC(NFG) <sup>ab</sup>	Fine-group resonance capture cross sections, $\sigma_{\ell}^{-102,r}$ , starting at top group. First card is a title card in 12A6 format.
		RXSF(NFG) <sup>ab</sup>	Fine-group resonance fission cross sections, $\sigma_{\ell}^{-18,r}$ , starting at top group. First card is a title card in 12A6 format.
		SXSC(NFG) <sup>b</sup>	Fine-group smooth (including unresolved resonance) capture cross sections, $\sigma_{\ell}^{-102,s}$ , starting at top group. First card is a title card in 12A6 format.
		SXSF(NFG) <sup>b</sup>	Fine-group smooth (including unresolved resonance) fission cross sections, $\sigma_{\ell}^{-18,s}$ , starting at top group. First card is a title card in 12A6 format.
		RW(NFG) <sup>ab</sup>	Fine-group resonance weighting functions for the zone, starting at top group. First card is a title card in 12A6 format.
		SW(NFG)	Fine-group smooth (flux) weighting functions for the zone, starting at top group. First card is a title card in 12A6 format.

The following six data blocks are identical to their homologous blocks in DTF-IV. In fact, for many LAPH problems, they will be identical to those for the DTF-IV problem used to compute the neutron flux vectors.

R(IM+1) Radii of the spatial mesh points.

MA(IM) Zone numbers for each interval.

MZ(IZM) Mixture number in each zone.

MB(MS) Mixture numbers for mix table.

MC(MS) Mix command: Specification of nuclides in the mixtures.

XMD(MS) Mix density of the nuclide in the mixtures.

Lastly, the data block for the neutron flux vectors appears in a format exactly like that used for DTF-IV flux dumps, i.e.,

PHI(IM,NBG) Normalized neutron fluxes by columns (i.e., by mesh interval and then by neutron broad groups).

<sup>a</sup>These should be entered even for nonresonance materials. In such case, any numbers may be used to fill the fields, but MC<sup>2</sup> will automatically output zeros in this block.

<sup>b</sup>Delete this data block if IRES = 0.

TABLE II  
SAMPLE PROBLEM INPUT

71168 SAMPLE PROBL, 3 ZONE, 5 MAT, 9 INTERVAL, GAMMA SOURCE											ID TITLE
11	52	26	3	9	9	6	18	9	1	0	21 PARAMS.
1.0 F+123											C
1			2		33						NMAT
1		5001			2		5002			3	5004 1 NNM
4		5004			5		5005			6	5006 2 NNM
3											3 NNM
102	1		13103		13						1 MZT
	110		102		5		6			7	8 1 MTN
	9		10		11		12			13	14 2 MTN
	51		52		53		0			-1	15 3 MTN
3											4 MTN
8.5 F+06		6.0 F+06		4.5 E+06		3.5 E+06		2.8 E+06		2.4 E+06	1 EG
2.0 F+06		1.6 F+06		1.1 F+06		0.07 F+06		0.45 E+063			2 FG
10.0 F+06		7.0 F+06		5.0 E+06		4.0 F+06		3.0 E+06		2.6 F+06	1 FMG
2.2 F+06		1.8 F+06		1.35 F+06		0.9 F+06		0.5 F+06		0.4 F+06	2 FMG
3											3 FMG
1.5 F+07		1.17E+07		9.10E+06		7.09E+06		5.52E+06		4.30E+06	1EMNF
3.35F+06		2.61E+06		2.03E+06		1.58E+06		1.23E+06		9.59E+05	2EMNF
7.47E+05		5.82E+05		4.53E+05		3.53E+05		2.75E+05		2.14E+05	3EMNF
1.67E+05		1.30E+05		1.01E+05		7.87E+04		6.13E+04		4.77E+04	4EMNF
3.72E+04		2.90E+04		2.26E+04		1.76E+04		1.37E+04		1.07E+04	5EMNF
8.30E+03		6.46E+03		5.03E+03		3.92E+03		3.05E+03		2.38E+03	6EMNF
1.85E+03		1.44E+03		1.12E+03		8.74E+02		6.81E+02		5.30E+02	7EMNF
4.13E+02		3.22E+02		2.51E+02		1.95E+02		1.52E+02		1.18E+02	8EMNF
9.22F+01		7.18F+01		5.59E+01		4.35F+01		3.39E+013			9EMNF
1.50F+07		9.10E+06		5.52E+06		3.35E+06		2.61E+06		1.23F+06	1EMNB
7.47F+05		4.53F+05		2.75E+05		1.67E+05		1.01E+05		6.13E+04	2EMNB
3.72E+04		2.26E+04		1.37E+04		8.30E+03		5.03E+03		3.05E+03	3EMNB
1.85E+03		1.12E+03		6.81E+02		4.13E+02		2.51E+02		1.52F+02	4EMNB
9.22F+01		5.59F+01		3.39E+013							5EMNB
RESONANCE CAPTURE CROSS SECTION FOR NA IN ZONE 1											
0.		0.		0.		0.		0.		0.	RXSC 1
0.		0.		0.		0.		0.		0.	RXSC 2
0.		0.		0.		0.		0.		0.	RXSC 3
0.		0.		0.		0.		0.		0.	RXSC 4
0.		0.		0.		0.		0.		0.	RXSC 5
0.		0.		0.		0.		0.		0.	RXSC 6
0.		0.		0.		0.		0.		0.	RXSC 7
0.		0.		0.		0.		0.		0.	RXSC 8
0.		0.		0.		0.		0.		0.	RXSC 9
RESONANCE FISSION CROSS SECTION FOR NA IN ZONE 1											
0.		0.		0.		0.		0.		0.	RXSF 1
0.		0.		0.		0.		0.		0.	RXSF 2
0.		0.		0.		0.		0.		0.	RXSF 3
0.		0.		0.		0.		0.		0.	RXSF 4
0.		0.		0.		0.		0.		0.	RXSF 5
0.		0.		0.		0.		0.		0.	RXSF 6
0.		0.		0.		0.		0.		0.	RXSF 7
0.		0.		0.		0.		0.		0.	RXSF 8
0.		0.		0.		0.		0.		0.	RXSF 9
SMOOTH CAPTURE CROSS SECTION FOR NA IN ZONE 1											
0.		0.		0.		0.		0.		0.	UR+SC 1
0.		0.		0.		1.05E-04		1.54E-04		2.48E-04	UR+SC 2
3.42E-04		2.94E-04		2.88E-04		4.45E-04		6.09E-04		7.68E-04	UR+SC 3
8.81E-04		7.12E-04		2.29E-04		3.94E-04		1.83E-03		1.38E-03	UR+SC 4
2.17E-03		4.47E-04		4.94E-04		5.88E-04		7.45E-04		9.81E-04	UR+SC 5
1.34E-03		1.99E-03		4.94E-03		4.13E-02		1.82E-01		2.92E-02	UR+SC 6
1.19E-02		7.77E-03		6.38E-03		5.80E-03		5.56E-03		5.58E-03	UR+SC 7
5.86E-03		6.23E-03		6.83E-03		7.50E-03		8.23E-03		9.05E-03	UR+SC 8
1.02E-02		1.15E-02		1.30E-02		1.47E-023					UR+SC 9
SMOOTH FISSION CROSS SECTION FOR NA IN ZONE 1											

TABLE II (continued)

0.	0.	0.	0.	0.	0.	UR+SF	1
0.	0.	0.	0.	0.	0.	UR+SF	2
0.	0.	0.	0.	0.	0.	UR+SF	3
0.	0.	0.	0.	0.	0.	UR+SF	4
0.	0.	0.	0.	0.	0.	UR+SF	5
0.	0.	0.	0.	0.	0.	UR+SF	6
0.	0.	0.	0.	0.	0.	UR+SF	7
0.	0.	0.	0.	0.	0.	UR+SF	8
0.	0.	0.	0.	0.	0.	UR+SF	9
RESONANCE WEIGHTING FUNCTIONS FOR ZONE 1							
2.05E-02	1.06E-01	3.55E-01	8.53E-01	1.58E+00	2.42E+00RW		1
3.28E+00	3.93E+00	4.47E+00	4.59E+00	4.66E+00	5.18E+00RW		2
6.10E+00	7.07E+00	7.18E+00	7.16E+00	6.64E+00	6.13E+00RW		3
5.33E+00	4.50E+00	3.67E+00	3.14E+00	2.60E+00	2.30E+00RW		4
1.85E+00	1.61E+00	1.30E+00	8.79E-01	6.15E-01	4.38E-01RW		5
3.26E-01	5.81E+01	3.16E+01	1.83E+01	1.33E+01	1.01E+01RW		6
6.13E+00	2.89E+00	1.22E+00	5.17E-01	2.30E-01	9.48E-02RW		7
3.27E-02	1.24E-02	3.68E-03	1.46E-03	5.89E-04	1.87E-04RW		8
8.21E-05	2.23E-05	9.00E-06	3.51E-06		RW		9
UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 1							
1.34E-02	6.79E-02	2.26E-01	5.48E-01	1.02E+00	1.55E+00SW		1
2.26E+00	2.70E+00	3.01E+00	3.46E+00	4.24E+00	5.71E+00SW		2
6.82E+00	8.94E+00	8.74E+00	9.08E+00	7.81E+00	6.70E+00SW		3
5.77E+00	5.35E+00	4.20E+00	3.80E+00	2.54E+00	2.75E+00SW		4
1.55E+00	1.31E+00	1.52E+00	9.42E-01	6.01E-01	3.66E-01SW		5
2.23E-01	1.96E-01	1.08E-01	2.90E-02	1.12E-02	6.20E-02SW		6
7.25E-02	4.34E-02	2.29E-02	1.37E-02	6.67E-03	3.19E-03SW		7
1.63E-03	6.69E-04	2.67E-04	1.14E-04	6.73E-05	2.04E-05SW		8
1.31E-05	3.10E-06	2.35E-06	8.25E-07		SW		9
RESONANCE CAPTURE CROSS SECTION FOR MG IN ZONE2							
0.	0.	0.	0.	0.	0.	RXSC	1
0.	0.	0.	0.	0.	0.	RXSC	2
0.	0.	0.	0.	0.	0.	RXSC	3
0.	0.	0.	0.	0.	0.	RXSC	4
0.	0.	0.	0.	0.	0.	RXSC	5
0.	0.	0.	0.	0.	0.	RXSC	6
0.	0.	0.	0.	0.	0.	RXSC	7
0.	0.	0.	0.	0.	0.	RXSC	8
0.	0.	0.	0.	0.	0.	RXSC	9
RESONANCE FISSION CROSS SECTION FOR MG IN ZONE 2							
0.	0.	0.	0.	0.	0.	RXSF	1
0.	0.	0.	0.	0.	0.	RXSF	2
0.	0.	0.	0.	0.	0.	RXSF	3
0.	0.	0.	0.	0.	0.	RXSF	4
0.	0.	0.	0.	0.	0.	RXSF	5
0.	0.	0.	0.	0.	0.	RXSF	6
0.	0.	0.	0.	0.	0.	RXSF	7
0.	0.	0.	0.	0.	0.	RXSF	8
0.	0.	0.	0.	0.	0.	RXSF	9
SMOOTH CAPTURE CROSS SECTION FOR MG IN ZONE2							
2.48E-04	3.02E-04	3.68E-04	4.47E-04	5.45E-04	6.63E-04UR+SC		1
8.08E-04	9.83E-04	1.29E-03	1.87E-03	2.72E-03	3.63E-03UR+SC		2
4.34E-03	4.91E-03	5.28E-03	5.41E-03	5.42E-03	5.36E-03UR+SC		3
5.27E-03	5.39E-03	5.65E-03	6.06E-03	6.60E-03	7.72E-03UR+SC		4
2.02E-02	4.59E-02	1.88E-02	1.44E-02	2.02E-02	3.19E-02UR+SC		5
7.61E-02	4.63E-02	1.74E-02	1.44E-02	7.86E-03	7.65E-03UR+SC		6
1.99E-02	2.31E-01	3.88E-02	1.76E-02	1.58E-02	1.94E-02UR+SC		7
2.84E-02	2.72E-02	2.54E-02	2.96E-02	3.78E-02	3.81E-02UR+SC		8
4.53E-02	5.29E-02	6.57E-02	6.75E-02		UR+SC		9
SMOOTH FISSION CROSS SECTION FOR MG IN ZONE 2							
0.	0.	0.	0.	0.	0.	UR+SF	1
0.	0.	0.	0.	0.	0.	UR+SF	2

TABLE II (continued)

0.	0.	0.	0.	0.	0.	UR+SF	3
0.	0.	0.	0.	0.	0.	UR+SF	4
0.	0.	0.	0.	0.	0.	UR+SF	5
0.	0.	0.	0.	0.	0.	UR+SF	6
0.	0.	0.	0.	0.	0.	UR+SF	7
0.	0.	0.	0.	0.	0.	UR+SF	8
0.	0.	0.	0.	0.	0.	UR+SF	9
RESONANCE CAPTURE CROSS SECTION FOR CL IN ZONE 2							
0.	0.	0.	0.	0.	0.	RXSC	1
0.	0.	0.	0.	0.	0.	RXSC	2
0.	0.	0.	0.	0.	0.	RXSC	3
0.	0.	0.	0.	0.	0.	RXSC	4
0.	0.	0.	0.	0.	0.	RXSC	5
0.	0.	0.	0.	0.	0.	RXSC	6
0.	0.	0.	0.	0.	0.	RXSC	7
0.	0.	0.	0.	0.	0.	RXSC	8
0.	0.	0.	0.	0.	0.	RXSC	9
RESONANCE FISSION CROSS SECTION FOR CL IN ZONE 2							
0.	0.	0.	0.	0.	0.	RXSF	1
0.	0.	0.	0.	0.	0.	RXSF	2
0.	0.	0.	0.	0.	0.	RXSF	3
0.	0.	0.	0.	0.	0.	RXSF	4
0.	0.	0.	0.	0.	0.	RXSF	5
0.	0.	0.	0.	0.	0.	RXSF	6
0.	0.	0.	0.	0.	0.	RXSF	7
0.	0.	0.	0.	0.	0.	RXSF	8
0.	0.	0.	0.	0.	0.	RXSF	9
SMOOTH CAPTURE CROSS SECTION FOR CL IN ZONE 2							
0.	0.	0.	0.	0.	0.	UR+SC	1
0.	0.	0.	0.	0.	0.	UR+SC	2
0.	0.	0.	0.	0.	0.	UR+SC	3
0.	0.	0.	0.	0.	0.	UR+SC	4
0.	0.	0.	0.	0.	0.	UR+SC	5
0.	0.	0.	0.	0.	0.	UR+SC	6
0.	0.	0.	0.	0.	0.	UR+SC	7
0.	0.	0.	0.	0.	0.	UR+SC	8
0.	0.	0.	0.	0.	0.	UR+SC	9
SMOOTH FISSION CROSS SECTION FOR CL IN ZONE 2							
0.	0.	0.	0.	0.	0.	UR+SF	1
0.	0.	0.	0.	0.	0.	UR+SF	2
0.	0.	0.	0.	0.	0.	UR+SF	3
0.	0.	0.	0.	0.	0.	UR+SF	4
0.	0.	0.	0.	0.	0.	UR+SF	5
0.	0.	0.	0.	0.	0.	UR+SF	6
0.	0.	0.	0.	0.	0.	UR+SF	7
0.	0.	0.	0.	0.	0.	UR+SF	8
0.	0.	0.	0.	0.	0.	UR+SF	9
RESONANCE WEIGHTING FUNCTIONS FOR ZONE 2							
2.13E-02	1.10E-01	3.70E-01	8.88E-01	1.64E+00	2.52E+00RW		1
3.42E+00	4.10E+00	4.66E+00	4.80E+00	4.87E+00	5.42E+00RW		2
6.40E+00	7.43E+00	7.56E+00	7.54E+00	7.01E+00	6.48E+00RW		3
5.64E+00	4.76E+00	3.89E+00	3.33E+00	2.77E+00	2.44E+00RW		4
1.97E+00	1.71E+00	1.38E+00	9.41E-01	6.59E-01	4.70E-01RW		5
3.51E-01	6.02E+01	3.27E+01	1.90E+01	1.38E+01	1.04E+01RW		6
6.36E+00	3.06E+00	1.32E+00	5.63E-01	2.53E-01	1.04E-01RW		7
3.61E-02	1.38E-02	4.12E-03	1.64E-03	6.62E-04	2.06E-04RW		8
8.70E-05	2.17E-05	7.51E-06	2.68E-063		RW		9
UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 2							
1.36E-02	6.85E-02	2.28E-01	5.53E-01	1.03E+00	1.56E+00SW		1
2.28E+00	2.73E+00	3.05E+00	3.51E+00	4.30E+00	5.80E+00SW		2
6.93E+00	9.11E+00	8.91E+00	9.26E+00	7.97E+00	6.85E+00SW		3
5.90E+00	5.47E+00	4.29E+00	3.89E+00	2.61E+00	2.83E+00SW		4



TABLE II (continued)

1.59F+00	1.35F+00	1.57F+00	0.74F-01	6.23E-01	3.79F-01SW	5
2.31F-01	2.03F-01	1.12E-01	3.00F-02	1.15E-02	6.41F-02SW	6
7.66E-02	4.69E-02	2.49E-02	1.50E-02	7.33E-03	3.51E-03SW	7
1.81E-03	7.54E-04	2.99E-04	1.29E-04	7.74E-05	2.25E-05SW	8
1.42F-05	3.12F-06	1.96E-06	6.46F-073		SW	9
RESONANCE CAPTURE CROSS SECTION FOR CL IN ZONE3						
0.	0.	0.	0.	0.	0.	RXSC 1
0.	0.	0.	0.	0.	0.	RXSC 2
0.	0.	0.	0.	0.	0.	RXSC 3
0.	0.	0.	0.	0.	0.	RXSC 4
0.	0.	0.	0.	0.	0.	RXSC 5
0.	0.	5.58E-05	5.05F-01	5.44E-01	5.28E-01	RXSC 6
5.48E-01	7.42E-01	7.27E-01	8.59E-01	8.54E-01	7.32E-01	RXSC 7
8.44F-01	9.20F-01	1.05E+00	1.14F+00	4.24E-01	2.64F+00	RXSC 8
1.33F+00	2.63F+00	1.35E-01	6.25E+003			RXSC 9
RESONANCE FISSION CROSS SECTION FOR CL IN ZONE 3						
0.	0.	0.	0.	0.	0.	RXSF 1
0.	0.	0.	0.	0.	0.	RXSF 2
0.	0.	0.	0.	0.	0.	RXSF 3
0.	0.	0.	0.	0.	0.	RXSF 4
0.	0.	0.	0.	0.	0.	RXSF 5
0.	0.	0.	0.	0.	0.	RXSF 6
0.	0.	0.	0.	0.	0.	RXSF 7
0.	0.	0.	0.	0.	0.	RXSF 8
0.	0.	0.	0.	0.	0.	RXSF 9
SMOOTH CAPTURE CROSS SECTION FOR CL IN ZONE3						
3.57E-03	4.55E-03	6.08E-03	8.14E-03	1.14E-02	1.74E-02	UR+SC 1
2.74E-02	4.16E-02	6.51E-02	1.12E-01	1.47E-01	1.50E-01	UR+SC 2
1.41E-01	1.34E-01	1.33E-01	1.39E-01	1.49E-01	1.62E-01	UR+SC 3
1.78E-01	1.98E-01	2.29E-01	2.74E-01	3.25E-01	3.76E-01	UR+SC 4
4.31E-01	4.88E-01	5.45E-01	6.00E-01	6.52E-01	7.00E-01	UR+SC 5
7.43E-01	7.84E-01	8.21E-01	3.64E-01	3.32E-01	3.03F-01	UR+SC 6
2.72F-01	2.43E-01	2.17E-01	1.30F-01	0.	0.	UR+SC 7
0.	0.	0.	0.	0.	0.	UR+SC 8
0.	0.	0.	0.	0.	0.	UR+SC 9
SMOOTH FISSION CROSS SECTION FOR CL IN ZONE 3						
1.10F+00	1.01E+00	1.02E+00	7.50E-01	5.68E-01	5.63E-01	UR+SF 1
5.43E-01	5.72E-01	4.81E-01	1.77E-01	2.63E-02	7.85E-03	UR+SF 2
1.24F-03	4.04F-04	0.	0.	0.	0.	UR+SF 3
0.	0.	0.	0.	0.	0.	UR+SF 4
0.	0.	0.	0.	0.	0.	UR+SF 5
0.	0.	0.	0.	0.	0.	UR+SF 6
0.	0.	0.	0.	0.	0.	UR+SF 7
0.	0.	0.	0.	0.	0.	UR+SF 8
0.	0.	0.	0.	0.	0.	UR+SF 9
RESONANCE CAPTURE CROSS SECTION FOR K IN ZONE3						
0.	0.	0.	0.	0.	0.	RXSC 1
0.	0.	0.	0.	0.	0.	RXSC 2
0.	0.	0.	0.	0.	0.	RXSC 3
0.	0.	0.	0.	0.	0.	RXSC 4
0.	0.	0.	0.	0.	0.	RXSC 5
0.	0.	0.	0.	0.	0.	RXSC 6
0.	0.	0.	4.71E-06	1.22E-05	4.63E-05	RXSC 7
1.22E-03	4.08E+00	6.79E+00	4.75E+00	9.24E+00	4.35E+00	RXSC 8
6.07E+00	8.74E+00	2.04E+01	1.40E+013			RXSC 9
RESONANCE FISSION CROSS SECTION FOR K IN ZONE 3						
0.	0.	0.	0.	0.	0.	RXSF 1
0.	0.	0.	0.	0.	0.	RXSF 2
0.	0.	0.	0.	0.	0.	RXSF 3
0.	0.	0.	0.	0.	0.	RXSF 4
0.	0.	0.	0.	0.	0.	RXSF 5
0.	0.	0.	0.	0.	0.	RXSF 6

TABLE II (continued)

0.	0.	0.	7.68E-04	1.99E-03	7.02E-03	RXSF	7
3.95E-02	8.78E+00	9.89E+00	1.14E+01	1.46E+01	1.71E+01	RXSF	8
2.15E+01	5.01E+01	1.57E+01	3.25E+003			RXSF	9
SMOOTH CAPTURE CROSS SECTION FOR K IN ZONE 3							
0.	0.	0.	0.	0.	0.	UR+SC	1
0.	0.	0.	1.91E-02	4.18E-02	6.35E-02	UR+SC	2
8.73E-02	1.07E-01	1.33E-01	1.56E-01	1.80E-01	1.94E-01	UR+SC	3
2.09E-01	2.16E-01	2.18E-01	2.26E-01	2.76E-01	3.74E-01	UR+SC	4
4.88E-01	6.02E-01	7.13E-01	8.27E-01	9.43E-01	1.07E+00	UR+SC	5
1.18E+00	1.31E+00	1.47E+00	1.68E+00	1.94E+00	2.21E+00	UR+SC	6
2.52E+00	2.88E+00	3.66E+00	2.49E+00	4.61E+00	6.26E+00	UR+SC	7
3.70E+00	1.92E+00	3.66E-01	0.	0.	0.	UR+SC	8
0.	0.	0.	0.	0.	0.	UR+SC	9
SMOOTH FISSION CROSS SECTION FOR K IN ZONE 3							
2.61E+00	2.46E+00	2.34E+00	1.96E+00	1.88E+00	1.94E+00	UR+SF	1
2.00E+00	2.03E+00	1.94E+00	1.83E+00	1.77E+00	1.69E+00	UR+SF	2
1.64E+00	1.55E+00	1.50E+00	1.48E+00	1.48E+00	1.49E+00	UR+SF	3
1.52E+00	1.53E+00	1.53E+00	1.47E+00	1.46E+00	1.52E+00	UR+SF	4
1.61E+00	1.72E+00	1.82E+00	1.94E+00	2.07E+00	2.23E+00	UR+SF	5
2.38E+00	2.55E+00	2.72E+00	2.98E+00	3.33E+00	3.72E+00	UR+SF	6
4.15E+00	4.68E+00	5.89E+00	4.23E+00	7.38E+00	9.93E+00	UR+SF	7
6.51E+00	6.07E+00	2.84E+00	0.	0.	0.	UR+SF	8
0.	0.	0.	0.	0.	0.	UR+SF	9
RESONANCE CAPTURE CROSS SECTION FOR CA IN ZONE 3							
0.	0.	0.	0.	0.	0.	RXSC	1
0.	0.	0.	0.	0.	0.	RXSC	2
0.	0.	0.	0.	0.	0.	RXSC	3
0.	0.	0.	0.	0.	0.	RXSC	4
0.	0.	0.	0.	0.	0.	RXSC	5
0.	0.	0.	0.	0.	0.	RXSC	6
0.	0.	0.	0.	0.	0.	RXSC	7
0.	0.	0.	0.	0.	0.	RXSC	8
0.	0.	0.	0.	0.	0.	RXSC	9
RESONANCE FISSION CROSS SECTION FOR CA IN ZONE 3							
0.	0.	0.	0.	0.	0.	RXSF	1
0.	0.	0.	0.	0.	0.	RXSF	2
0.	0.	0.	0.	0.	0.	RXSF	3
0.	0.	0.	0.	0.	0.	RXSF	4
0.	0.	0.	0.	0.	0.	RXSF	5
0.	0.	0.	0.	0.	0.	RXSF	6
0.	0.	0.	0.	0.	0.	RXSF	7
0.	0.	0.	0.	0.	0.	RXSF	8
0.	0.	0.	0.	0.	0.	RXSF	9
SMOOTH CAPTURE CROSS SECTION FOR CA IN ZONE 3							
0.	0.	0.	0.	0.	0.	UR+SC	1
0.	0.	0.	1.05E-04	1.54E-04	2.48E-04	UR+SC	2
3.42E-04	2.94E-04	2.88E-04	4.45E-04	6.09E-04	7.68E-04	UR+SC	3
8.81E-04	7.12E-04	2.29E-04	3.94E-04	1.83E-03	1.38E-03	UR+SC	4
2.17E-03	4.47E-04	4.94E-04	5.88E-04	7.45E-04	9.81E-04	UR+SC	5
1.34E-03	1.99E-03	4.94E-03	4.13E-02	1.82E-01	2.92E-02	UR+SC	6
1.19E-02	7.77E-03	6.38E-03	5.80E-03	5.56E-03	5.58E-03	UR+SC	7
5.86E-03	6.23E-03	6.83E-03	7.50E-03	8.23E-03	9.05E-03	UR+SC	8
1.02E-02	1.15E-02	1.30E-02	1.47E-023			UR+SC	9
SMOOTH FISSION CROSS SECTION FOR CA IN ZONE 3							
0.	0.	0.	0.	0.	0.	UR+SF	1
0.	0.	0.	0.	0.	0.	UR+SF	2
0.	0.	0.	0.	0.	0.	UR+SF	3
0.	0.	0.	0.	0.	0.	UR+SF	4
0.	0.	0.	0.	0.	0.	UR+SF	5
0.	0.	0.	0.	0.	0.	UR+SF	6
0.	0.	0.	0.	0.	0.	UR+SF	7
0.	0.	0.	0.	0.	0.	UR+SF	8

TABLE II (continued)

RESONANCE WEIGHTING FUNCTIONS FOR ZONE 3						UR+SF	9
n.	n.	0.	n.	3			
2.05E-02	1.06E-01	3.55E-01	8.53E-01	1.58E+00	2.42E+00RW		1
3.28E+00	2.93E+00	4.47E+00	4.59E+00	4.66E+00	5.18E+00RW		2
6.10E+00	7.07E+00	7.18E+00	7.16E+00	6.64E+00	6.13E+00RW		3
5.33E+00	4.50E+00	3.67E+00	3.14E+00	2.60E+00	2.30E+00RW		4
1.85E+00	1.61E+00	1.30E+00	8.79E-01	6.15E-01	4.38E-01RW		5
3.26E-01	5.81E+01	3.16E+01	1.83E+01	1.33E+01	1.01E+01RW		6
6.13E+00	2.89E+00	1.22E+00	5.17E-01	2.30E-01	9.48E-02RW		7
3.27E-02	1.24E-02	3.68E-03	1.46E-03	5.89E-04	1.87E-04RW		8
8.21E-05	2.23E-05	9.00E-06	2.51E-06		RW		9
UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 3							
n.	n.	0.	n.	3			
1.34E-02	6.79E-02	2.26E-01	5.48E-01	1.02E+00	1.55E+00SW		1
2.26E+00	2.70E+00	3.01E+00	3.46E+00	4.24E+00	5.71E+00SW		2
6.82E+00	8.94E+00	8.74E+00	9.08E+00	7.81E+00	6.70E+00SW		3
5.77E+00	5.35E+00	4.20E+00	3.80E+00	2.54E+00	2.75E+00SW		4
1.55E+00	1.31E+00	1.52E+00	9.42E-01	6.01E-01	3.66E-01SW		5
2.23E-01	1.96E-01	1.08E-01	2.90E-02	1.12E-02	6.20E-02SW		6
7.25E-02	4.34E-02	2.29E-02	1.37E-02	6.67E-03	3.19E-03SW		7
1.63E-03	6.69E-04	2.67E-04	1.14E-04	6.73E-05	2.04E-05SW		8
1.31E-05	2.19E-06	2.35E-06	8.25E-07		SW		9
203 0.0	4.0	6.0	202 9.0	15.0			R
103	1104	2102	33				MA
	7	8	93				MZ
102	7102	8104	93				MB
	0	1	0	2	3	0	1 MC
	4	5	62				2 MC
0.0	0.06	0.0	0.05	0.04	0.0		1 XMD
0.02	0.02	0.01	3				2 XMD
103 1.0	104 0.1	102 0.01	103 2.0	104 0.2	102 0.02		1 PHI
103 3.0	104 0.3	102 0.03	103 4.0	104 0.4	102 0.04		2 PHI
103 5.0	104 0.5	102 0.05	103 6.0	104 0.6	102 0.06		3 PHI
103 7.0	104 0.7	102 0.07	103 8.0	104 0.8	102 0.08		4 PHI
103 9.0	104 0.9	102 0.09	103 10.0	104 1.0	102 0.10		5 PHI
103 11.0	104 1.1	102 0.11	103 12.0	104 1.2	102 0.12		6 PHI
103 13.0	104 1.3	102 0.13	103 14.0	104 1.4	102 0.14		7 PHI
103 15.0	104 1.5	102 0.15	103 16.0	104 1.6	102 0.16		8 PHI
103 17.0	104 1.7	102 0.17	103 18.0	104 1.8	102 0.18		9 PHI
103 19.0	104 1.9	102 0.19	103 20.0	104 2.0	102 0.20		10 PHI
103 21.0	104 2.1	102 0.21	103 22.0	104 2.2	102 0.22		11 PHI
103 23.0	104 2.3	102 0.23	103 24.0	104 2.4	102 0.24		12 PHI
103 25.0	104 2.5	102 0.25	103 26.0	104 2.6	102 0.26		13 PHI
2							14 PHI

TABLE III  
SAMPLE PROBLEM OUTPUT

ENDF/B TAPE I. D. = 1304 LIBRARY TAPE PREPARED FOR LAPH SAMPLE PROBLEM ON 13 JANUARY 1970.

LAPH PROBLEM ID= 71168 SAMPLE PROBL. 3 ZONE, 5 MAT, 9 INTERVAL, GAMMA SOURCE  
 INTEGER PARAMETERS NGG NFG NBG IZM IM MS MCR MM NPM IRES IWO IOO  
 11 52 26 3 9 9 6 18 9 1 0 21

RENORM CONST 1  
 1.0000E+12

NO MATS/ZONE 3  
 1 2 3  
 NUMBER OF NUCLIDES IN EACH ZONE  
 ZONE NUMBER OF NUCLIDES  
 1 1  
 2 2  
 3 3

NNM ARRAY 12  
 1 5001 2 5002 3 5004 4 5004 5 5005  
 6 5006

NUCLIDE SEQUENCE NUMBER NUCLIDE  
 1----- 5001  
 2----- 5002  
 3----- 5004  
 4----- 5004  
 5----- 5005  
 6----- 5006

MZT ARRAY 6  
 1 13 1 1 1

MTN NUMBERS 18  
 110 102 5 6 7 8 9 10 11 12 13 14 15 11 12  
 13 14 51 52 53 0 -1

NUCLIDE SEQUENCE NUMBER MT NUMBERS  
 1 110  
 2 102  
 3 5 6 7 8 9 10 11 12 13 14 51 52 53  
 4 0  
 5 -1  
 6 15

EGAMMA BAR 11  
 8.5000E+06 6.0000E+06 4.5000E+06 3.5000E+06 2.8000E+06 2.4000E+06 2.0000E+06 1.6000E+06 1.1000E+06 7.0000E+04  
 4.5000E+05

GAMMA BOUNDS 12  
 1.0000E+07 7.0000E+06 5.0000E+06 4.0000E+06 3.0000E+06 2.6000E+06 2.2000E+06 1.8000E+06 1.3500E+06 9.0000E+05  
 5.0000E+05 4.0000E+05

NEUTRON FINE 53  
 1.5000E+07 1.1700E+07 9.1000E+06 7.0900E+06 5.5200E+06 4.3000E+06 3.3500E+06 2.6100E+06 2.0300E+06 1.5800E+06  
 1.2300E+06 9.5900E+05 7.4700E+05 5.8200E+05 4.5300E+05 3.5300E+05 2.7500E+05 2.1400E+05 1.6700E+05 1.3000E+05  
 1.0100E+05 7.8700E+04 6.1300E+04 4.7700E+04 3.7200E+04 2.9000E+04 2.2600E+04 1.7600E+04 1.3700E+04 1.0700E+04  
 8.3000E+03 6.4600E+03 5.0300E+03 3.9200E+03 3.0500E+03 2.3800E+03 1.8500E+03 1.4400E+03 1.1200E+03 8.7400E+02  
 6.8100E+02 5.3000E+02 4.1300E+02 3.2200E+02 2.5100E+02 1.9500E+02 1.5200E+02 1.1800E+02 9.2200E+01 7.1800E+01  
 5.5900E+01 4.3500E+01 3.3900E+01

NEUTRON BRD 27  
 1.5000E+07 9.1000E+06 5.5200E+06 3.3500E+06 2.6100E+06 1.2300E+06 7.4700E+05 4.5300E+05 2.7500E+05 1.6700E+05  
 1.0100E+05 6.1300E+04 3.7200E+04 2.2600E+04 1.3700E+04 8.3000E+03 5.0300E+03 3.0500E+03 1.8500E+03 1.1200E+03  
 6.8100E+02 4.1300E+02 2.5100E+02 1.5200E+02 9.2200E+01 5.5900E+01 3.3900E+01

ERROR IN THE EFFECTIVE AVERAGE ENERGY INPUT FOR GROUP 10  
 THE VALUE EG(I) = 7.000000E+04 SHOULD LIE BETWEEN THE BOUNDARIES EMG(I) = 9.000000E+05 AND EMG(I+1) = 5.000000E+05  
 THE MIDPOINT OF THE ENERGY INTERVAL HAS BEEN USED. EG(I) HAS BEEN REPLACED BY 7.000000E+05

RESONANCE CAPTURE CROSS SECTION FOR NA IN ZONE 1

RXSC 52  
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  
 0. 0.

RESONANCE FISSION CROSS SECTION FOR NA IN ZONE 1

TABLE III (continued)

RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

SMOOTH CAPTURE CROSS SECTION FOR NA IN ZONE 1

SXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0500E-04
1.5400E-04	2.4800E-04	3.4200E-04	2.9400E-04	2.8800E-04	4.4500E-04	6.0900E-04	7.6800E-04	8.8100E-04	7.1200E-04	7.1200E-04
2.2900E-04	3.9400E-04	1.8300E-03	1.3800E-03	2.1700E-03	4.4700E-04	4.9400E-04	5.8800E-04	7.4500E-04	9.8100E-04	9.8100E-04
1.3400E-03	1.9900E-03	4.9400E-03	4.1300E-02	1.8200E-01	2.9200E-02	1.1900E-02	7.7700E-03	6.3800E-03	5.8000E-03	5.8000E-03
5.5600E-03	5.5800E-03	5.8600E-03	6.2300E-03	6.8300E-03	7.5000E-03	8.2300E-03	9.0500E-03	1.0200E-02	1.1500E-02	1.1500E-02
1.3000E-02	1.4700E-02									

SMOOTH FISSION CROSS SECTION FOR NA IN ZONE 1

SXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

RESONANCE WEIGHTING FUNCTIONS FOR ZONE 1

RW	52									
2.0500E-02	1.0600E-01	3.5500E-01	8.5300E-01	1.5800E+00	2.4200E+00	3.2800E+00	3.9300E+00	4.4700E+00	4.5900E+00	4.5900E+00
4.6600E+00	5.1800E+00	6.1000E+00	7.0700E+00	7.1800E+00	7.1600E+00	6.6400E+00	6.1300E+00	5.3300E+00	4.5000E+00	4.5000E+00
3.6700E+00	3.1400E+00	2.6000E+00	2.3000E+00	1.8500E+00	1.6100E+00	1.3000E+00	8.7900E-01	6.1500E-01	4.3800E-01	4.3800E-01
3.2600E-01	5.8100E+01	3.1600E+01	1.8300E+01	1.3300E+01	1.0100E+01	6.1300E+00	2.8900E+00	1.2200E+00	5.1700E-01	5.1700E-01
2.3000E-01	9.4800E-02	3.2700E-02	1.2400E-02	3.6800E-03	1.4600E-03	5.8900E-04	1.8700E-04	8.2100E-05	2.2300E-05	2.2300E-05
9.0000E-06	3.5100E-06									

UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 1

SW	52									
1.3400E-02	6.7900E-02	2.2600E-01	5.4800E-01	1.0200E+00	1.5500E+00	2.2600E+00	2.7000E+00	3.0100E+00	3.4600E+00	3.4600E+00
4.2400E+00	5.7100E+00	6.8200E+00	8.9400E+00	8.7400E+00	9.0800E+00	7.8100E+00	6.7000E+00	5.7700E+00	5.3500E+00	5.3500E+00
4.2000E+00	3.8000E+00	2.5400E+00	2.7500E+00	1.5500E+00	1.3100E+00	1.5200E+00	9.4200E-01	6.0100E-01	3.6600E-01	3.6600E-01
2.2300E-01	1.9600E-01	1.0800E-01	2.9000E-02	1.1200E-02	6.2000E-02	7.2500E-02	4.3400E-02	2.2900E-02	1.3700E-02	1.3700E-02
6.6700E-03	3.1900E-03	1.6300E-03	6.6900E-04	2.6700E-04	1.1400E-04	6.7300E-05	2.0400E-05	1.3100E-05	3.1900E-06	3.1900E-06
2.3500E-06	8.2500E-07									

RESONANCE CAPTURE CROSS SECTION FOR MG IN ZONE 2

RXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

RESONANCE FISSION CROSS SECTION FOR MG IN ZONE 2

RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

SMOOTH CAPTURE CROSS SECTION FOR MG IN ZONE 2

SXSC	52									
2.4800E-04	3.0200E-04	3.6800E-04	4.4700E-04	5.4500E-04	6.6300E-04	8.0800E-04	9.8300E-04	1.2900E-03	1.8700E-03	1.8700E-03
2.7200E-03	3.6300E-03	4.3400E-03	4.9100E-03	5.2800E-03	5.4100E-03	5.4200E-03	5.3600E-03	5.2700E-03	5.3900E-03	5.3900E-03
5.6500E-03	6.0600E-03	6.6000E-03	7.7200E-03	2.0200E-02	4.5900E-02	1.8800E-02	1.4400E-02	2.0200E-02	3.1900E-02	3.1900E-02
7.6100E-02	4.6300E-02	1.7400E-02	1.4400E-02	7.8600E-03	7.6500E-03	1.9900E-02	2.3100E-01	3.8800E-02	1.7600E-02	1.7600E-02
1.5800E-02	1.9400E-02	2.8400E-02	2.7200E-02	2.5400E-02	2.9600E-02	3.7800E-02	3.8100E-02	4.5300E-02	5.2900E-02	5.2900E-02
6.5700E-02	6.7500E-02									

SMOOTH FISSION CROSS SECTION FOR MG IN ZONE 2

SXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

RESONANCE CAPTURE CROSS SECTION FOR CL IN ZONE 2

RXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

RESONANCE FISSION CROSS SECTION FOR CL IN ZONE 2

RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

SMOOTH CAPTURE CROSS SECTION FOR CL IN ZONE 2

SXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

SMOOTH FISSION CROSS SECTION FOR CL IN ZONE 2

SXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

RESONANCE WEIGHTING FUNCTIONS FOR ZONE 2

RW	52									
2.1300E-02	1.1000E-01	3.7000E-01	8.8800E-01	1.6400E+00	2.5200E+00	3.4200E+00	4.1000E+00	4.6600E+00	4.8000E+00	
4.8700E+00	5.4200E+00	6.4000E+00	7.4300E+00	7.5600E+00	7.5400E+00	7.0100E+00	6.4800E+00	5.6400E+00	4.7600E+00	
3.8900E+00	3.3300E+00	2.7700E+00	2.4400E+00	1.9700E+00	1.7100E+00	1.3800E+00	9.4100E-01	6.5900E-01	4.7000E-01	
3.5100E-01	6.0200E-01	3.2700E-01	1.9000E-01	1.3800E-01	1.0400E-01	6.3600E-01	3.0600E-01	1.3200E-01	5.6300E-01	
2.5300E-01	1.0400E-01	3.6100E-02	1.3800E-02	4.1200E-03	1.6400E-03	6.6200E-04	2.0600E-04	8.7000E-05	2.1700E-05	
7.5100E-06	2.6800E-06									

UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 2

SW	52									
1.3600E-02	6.8500E-02	2.2800E-01	5.5300E-01	1.0300E+00	1.5600E+00	2.2800E+00	2.7300E+00	3.0500E+00	3.5100E+00	
4.3000E+00	5.8000E+00	6.9300E+00	9.1100E+00	8.9100E+00	9.2600E+00	7.9700E+00	6.8500E+00	5.9000E+00	5.4700E+00	
4.2900E+00	3.8900E+00	2.6100E+00	2.8300E+00	1.5900E+00	1.3500E+00	1.5700E+00	9.7400E-01	6.2300E-01	3.7900E-01	
2.3100E-01	2.0300E-01	1.1200E-01	3.0000E-02	1.1500E-02	6.4100E-02	7.6600E-02	4.6900E-02	2.4900E-02	1.5000E-02	
7.3300E-03	3.5100E-03	1.8100E-03	7.5400E-04	2.9900E-04	1.2900E-04	7.7400E-05	2.2500E-05	1.4200E-05	3.1200E-06	
1.9600E-06	6.4600E-07									

RESONANCE CAPTURE CROSS SECTION FOR CL IN ZONE 3

RXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	5.5800E-05	5.0500E-01	5.4400E-01	5.2800E-01	5.4800E-01	7.4200E-01	7.2700E-01	8.5900E-01	
8.5400E-01	7.3200E-01	8.4400E-01	9.2000E-01	1.0500E+00	1.1400E+00	4.2400E-01	2.6400E+00	1.3300E+00	2.6300E+00	
1.3500E-01	6.2500E+00									

RESONANCE FISSION CROSS SECTION FOR CL IN ZONE 3

RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

SMOOTH CAPTURE CROSS SECTION FOR CL IN ZONE 3

SXSC	52									
3.5700E-03	4.5500E-03	6.0800E-03	8.1400E-03	1.1400E-02	1.7400E-02	2.7400E-02	4.1600E-02	6.5100E-02	1.1200E-01	
1.4700E-01	1.5000E-01	1.4100E-01	1.3400E-01	1.3300E-01	1.3900E-01	1.4900E-01	1.6200E-01	1.7800E-01	1.9800E-01	
2.2900E-01	2.7400E-01	3.2500E-01	3.7600E-01	4.3100E-01	4.8800E-01	5.4500E-01	6.0000E-01	6.5200E-01	7.0000E-01	
7.4300E-01	7.8400E-01	8.2100E-01	3.6400E-01	3.3200E-01	3.0300E-01	2.7200E-01	2.4300E-01	2.1700E-01	1.3000E-01	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	

SMOOTH FISSION CROSS SECTION FOR CL IN ZONE 3

SXSF	52									
1.1000E+00	1.0100E+00	1.0200E+00	7.5000E-01	5.6800E-01	5.6300E-01	5.4300E-01	5.7200E-01	4.8100E-01	1.7700E-01	
2.6300E-02	7.8500E-03	1.2400E-03	4.0400E-04	0.	0.	0.	0.	0.	0.	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	

TABLE III (continued)

0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.									
RESONANCE CAPTURE CROSS SECTION FOR K IN ZONE 3										
RXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.2200E-05	4.6300E-05	1.2200E-03	4.0800E+00	6.7900E+00	4.7500E+00	9.2400E+00	4.3500E+00	6.0700E+00	8.7400E+00	4.7100E-06
2.0400E+01	1.4000E+01									
RESONANCE FISSION CROSS SECTION FOR K IN ZONE 3										
RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
1.9900E-03	7.0200E-03	3.9500E-02	8.7800E+00	9.8900E+00	1.1400E+01	1.4600E+01	1.7100E+01	2.1500E+01	5.0100E+01	7.6800E-04
1.5700E+01	3.2500E+00									
SMOOTH CAPTURE CROSS SECTION FOR K IN ZONE 3										
SXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.9100E-02
4.1800E-02	6.3500E-02	8.7300E-02	1.0700E-01	1.3300E-01	1.5600E-01	1.8000E-01	1.9400E-01	2.0900E-01	2.1600E-01	2.1600E-01
2.1800E-01	2.2600E-01	2.7600E-01	3.7400E-01	4.8000E-01	6.0200E-01	7.1300E-01	8.2700E-01	9.4300E-01	1.0700E+00	1.0700E+00
1.1800E+00	1.3100E+00	1.4700E+00	1.6800E+00	1.9400E+00	2.2100E+00	2.5200E+00	2.8800E+00	3.6600E+00	2.4900E+00	2.4900E+00
4.6100E+00	6.2600E+00	3.7000E+00	1.9200E+00	3.6600E-01	0.	0.	0.	0.	0.	0.
0.	0.									
SMOOTH FISSION CROSS SECTION FOR K IN ZONE 3										
SXSF	52									
2.6100E+00	2.4600E+00	2.3400E+00	1.9600E+00	1.8800E+00	1.9400E+00	2.0000E+00	2.0300E+00	1.9400E+00	1.8300E+00	1.8300E+00
1.7700E+00	1.6900E+00	1.6400E+00	1.5500E+00	1.5000E+00	1.4800E+00	1.4800E+00	1.4900E+00	1.5200E+00	1.5300E+00	1.5300E+00
1.5300E+00	1.4700E+00	1.4600E+00	1.5200E+00	1.6100E+00	1.7200E+00	1.8200E+00	1.9400E+00	2.0700E+00	2.2300E+00	2.2300E+00
2.3800E+00	2.5500E+00	2.7200E+00	2.9800E+00	3.3300E+00	3.7200E+00	4.1500E+00	4.6800E+00	5.8900E+00	4.2300E+00	4.2300E+00
7.3800E+00	9.9300E+00	6.5100E+00	6.0700E+00	2.8400E+00	0.	0.	0.	0.	0.	0.
0.	0.									
RESONANCE CAPTURE CROSS SECTION FOR CA IN ZONE 3										
RXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.									
RESONANCE FISSION CROSS SECTION FOR CA IN ZONE 3										
RXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.									
SMOOTH CAPTURE CROSS SECTION FOR CA IN ZONE 3										
SXSC	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	1.0500E-04
1.5400E-04	2.4800E-04	3.4200E-04	2.9400E-04	2.8800E-04	4.4500E-04	6.0900E-04	7.6800E-04	8.8100E-04	7.1200E-04	7.1200E-04
2.2900E-04	3.9400E-04	1.8300E-03	1.3800E-03	2.1700E-03	4.4700E-04	4.9400E-04	5.8800E-04	7.4500E-04	9.8100E-04	9.8100E-04
1.3400E-03	1.9900E-03	4.9400E-03	4.1300E-02	1.8200E-01	2.9200E-02	1.1900E-02	7.7700E-03	6.3800E-03	5.8000E-03	5.8000E-03
5.5600E-03	5.5800E-03	5.8600E-03	6.2300E-03	6.8300E-03	7.5000E-03	8.2300E-03	9.0500E-03	1.0200E-02	1.1500E-02	1.1500E-02
1.3000E-02	1.4700E-02									
SMOOTH FISSION CROSS SECTION FOR CA IN ZONE 3										
SXSF	52									
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
0.	0.									
RESONANCE WEIGHTING FUNCTIONS FOR ZONE 3										
RW	52									
2.0500E-02	1.0600E-01	3.5500E-01	8.5300E-01	1.5600E+00	2.4200E+00	3.2800E+00	3.9300E+00	4.4700E+00	4.5900E+00	4.5900E+00
4.6600E+00	5.1800E+00	6.1000E+00	7.0700E+00	7.1800E+00	7.1600E+00	6.6400E+00	6.1300E+00	5.3300E+00	4.5000E+00	4.5000E+00
3.6700E+00	3.1400E+00	2.6000E+00	2.3000E+00	1.8500E+00	1.6100E+00	1.3000E+00	8.1900E-01	6.1500E-01	4.3800E-01	4.3800E-01
3.2600E-01	5.8100E+01	3.1600E+01	1.8300E+01	1.3300E+01	1.0100E+01	6.1300E+00	2.8900E+00	1.2200E+00	5.1700E-01	5.1700E-01
2.3000E-01	9.4800E-02	3.2700E-02	1.2400E-02	3.6800E-03	1.4600E-03	5.8900E-04	1.0700E-04	8.2100E-05	2.2300E-05	2.2300E-05
9.0000E-06	3.5100E-06									

TABLE III (continued)

UNRESOLVED PLUS SMOOTH WEIGHTING FUNCTIONS FOR ZONE 3

SM	52	2.2600E-01	5.4800E-01	1.0200E+00	1.5500E+00	2.2600E+00	2.7000E+00	3.0100E+00	3.4600E+00												
1.3400E-02	6.7900E-02	2.2600E-01	5.4800E-01	1.0200E+00	1.5500E+00	2.2600E+00	2.7000E+00	3.0100E+00	3.4600E+00												
4.2400E+00	5.7100E+00	6.8200E+00	8.9400E+00	8.7400E+00	9.0800E+00	7.8100E+00	6.7000E+00	5.7700E+00	5.3500E+00												
4.2000E+00	3.8000E+00	2.5400E+00	2.7500E+00	1.5500E+00	1.3100E+00	1.5200E+00	9.4200E-01	6.0100E-01	3.6600E-01												
2.2300E-01	1.9600E-01	1.0800E-01	2.9000E-02	1.1200E-02	6.2000E-02	7.2500E-02	4.3400E-02	2.2900E-02	1.3700E-02												
6.6700E-03	3.1900E-03	1.6300E-03	6.6900E-04	2.6700E-04	1.1400E-04	6.7300E-05	2.0400E-05	1.3100E-05	3.1900E-06												
2.3500E-06	8.2500E-07																				
RADII	10																				
0.	1.0000E+00	2.0000E+00	3.0000E+00	4.0000E+00	6.0000E+00	9.0000E+00	1.1000E+01	1.3000E+01	1.5000E+01												
ZONE NUMBERS	9																				
1	1	1	2	2	2	2	2	3	3												
MIXTURE NOS	3																				
7	8	9																			
MIX TABLE	9																				
7	7	8	8	8	9	9	9	9	9												
MIX COMMAND	9																				
0	1	0	2	3	0	4	5	6													
MIX DENSITY	9																				
0.	6.0000E-02	0.	5.0000E-02	4.0000E-02	0.	3.0000E-02	2.0000E-02	1.0000E-02													
NEUTRON FLUX	234																				
1.0000E+00	1.0000E+00	1.0000E+00	1.0000E-01	1.0000E-01	1.0000E-01	1.0000E-01	1.0000E-02	1.0000E-02	2.0000E+00												
2.0000E+00	2.0000E+00	2.0000E+00	2.0000E-01	2.0000E-01	2.0000E-01	2.0000E-02	2.0000E-02	3.0000E+00	3.0000E+00												
3.0000E+00	3.0000E+01	3.0000E-01	3.0000E-01	3.0000E-01	3.0000E-02	3.0000E-02	4.0000E+00	4.0000E+00	4.0000E+00												
4.0000E-01	4.0000E-01	4.0000E-01	4.0000E-01	4.0000E-02	4.0000E-02	5.0000E+00	5.0000E+00	5.0000E+00	5.0000E-01												
5.0000E-01	5.0000E-01	5.0000E-01	5.0000E-02	5.0000E-02	6.0000E+00	6.0000E+00	6.0000E+00	6.0000E-01	6.0000E-01												
6.0000E-01	6.0000E-01	6.0000E-02	6.0000E-02	7.0000E+00	7.0000E+00	7.0000E+00	7.0000E-01	7.0000E-01	7.0000E-01												
7.0000E-01	7.0000E-02	7.0000E-02	8.0000E+00	8.0000E+00	8.0000E+00	8.0000E-01	8.0000E-01	8.0000E-01	8.0000E-01												
8.0000E-02	8.0000E-02	9.0000E+00	9.0000E+00	9.0000E+00	9.0000E-01	9.0000E-01	9.0000E-01	9.0000E-01	9.0000E-02												
9.0000E-02	1.0000E+01	1.0000E+01	1.0000E+01	1.0000E+01	1.0000E+00	1.0000E+00	1.0000E+00	1.0000E-01	1.0000E-01												
1.1000E+01	1.1000E+01	1.1000E+01	1.1000E+00	1.1000E+00	1.1000E+00	1.1000E+00	1.1000E-01	1.1000E-01	1.2000E+01												
1.2000E+01	1.2000E+01	1.2000E+00	1.2000E+00	1.2000E+00	1.2000E+00	1.2000E-01	1.2000E-01	1.3000E+01	1.3000E+01												
1.3000E+01	1.3000E+00	1.3000E+00	1.3000E+00	1.3000E+00	1.3000E+00	1.3000E-01	1.4000E+01	1.4000E+01	1.4000E+01												
1.4000E+00	1.4000E+00	1.4000E+00	1.4000E+00	1.4000E-01	1.4000E-01	1.5000E+01	1.5000E+01	1.5000E+01	1.5000E+00												
1.5000E+00	1.5000E+00	1.5000E+00	1.5000E-01	1.5000E-01	1.6000E+01	1.6000E+01	1.6000E+01	1.6000E+00	1.6000E+00												
1.6000E+00	1.6000E+00	1.6000E-01	1.6000E-01	1.7000E+01	1.7000E+01	1.7000E+01	1.7000E+00	1.7000E+00	1.7000E+00												
1.7000E+00	1.7000E-01	1.7000E-01	1.8000E+01	1.8000E+01	1.8000E+01	1.8000E+00	1.8000E+00	1.8000E+00	1.8000E+00												
1.8000E-01	1.8000E-01	1.9000E+01	1.9000E+01	1.9000E+01	1.9000E+00	1.9000E+00	1.9000E+00	1.9000E+00	1.9000E-01												
1.9000E-01	2.0000E+01	2.0000E+01	2.0000E+01	2.0000E+00	2.0000E+00	2.0000E+00	2.0000E+00	2.0000E-01	2.0000E-01												
2.1000E+01	2.1000E+01	2.1000E+01	2.1000E+00	2.1000E+00	2.1000E+00	2.1000E+00	2.1000E-01	2.1000E-01	2.2000E+01												
2.2000E+01	2.2000E+01	2.2000E+00	2.2000E+00	2.2000E+00	2.2000E+00	2.2000E-01	2.2000E-01	2.3000E+01	2.3000E+01												
2.3000E+01	2.3000E+00	2.3000E+00	2.3000E+00	2.3000E+00	2.3000E+00	2.3000E-01	2.4000E+01	2.4000E+01	2.4000E+01												
2.4000E+00	2.4000E+00	2.4000E+00	2.4000E+00	2.4000E+01	2.4000E+01	2.5000E+01	2.5000E+01	2.5000E+01	2.5000E+00												
2.5000E+00	2.5000E+00	2.5000E+00	2.5000E-01	2.5000E-01	2.6000E+01	2.6000E+01	2.6000E+01	2.6000E+00	2.6000E+00												
2.6000E+00	2.6000E+00	2.6000E-01	2.6000E-01																		
-----ZONE	1	-----MATERIAL	1	-----																	
-----ZONE	2	-----MATERIAL	1	-----																	
-----ZONE	2	-----MATERIAL	2	-----																	
-----ZONE	3	-----MATERIAL	1	-----																	
-----ZONE	3	-----MATERIAL	2	-----																	
UNDER THE OPTION PROVIDED WHEN INPUT MT=-1 IS USED, THERE WILL BE 22 REACTION TYPES USED AS FOLLOWS -																					
MTNO(I)=	5	6	7	8	9	10	11	12	13	14	15	51	52	53	54	55	56	57	102	103	
MTNO(I)=	107	110																			
INDEX	101	MT	NUMBER	GAMMA ENERGY RANGE		NUMERATOR		DENOMINATOR		EHAT											
1	15			.40000000E+06	.50000000E+06	.71956500E+04	.15642250E-01	.46001374E+06													
23	15			.50000000E+06	.90000000E+06	.57921700E+05	.80912250E-01	.71585823E+06													
45	15			.90000000E+06	.13500000E+07	.13033064E+06	.11495719E+00	.11337320E+07													
67	15			.13500000E+07	.18000000E+07	.20214041E+06	.12810231E+00	.15779607E+07													
89	15			.18000000E+07	.22000000E+07	.23460980E+06	.11727700E+00	.20004758E+07													
111	15			.22000000E+07	.26000000E+07	.28072260E+06	.11701300E+00	.23990719E+07													
133	15			.26000000E+07	.30000000E+07	.31364940E+06	.11215300E+00	.27966207E+07													
155	15			.30000000E+07	.40000000E+07	.65685000E+06	.19283500E+00	.34062800E+07													
177	15			.40000000E+07	.50000000E+07	.33776000E+06	.77684750E-01	.43478289E+07													
199	15			.50000000E+07	.70000000E+07	.77647500E+05	.15529500E-01	.50000000E+07													
243	15			.40000000E+06	.50000000E+06	.68521500E+04	.14895000E-01	.46003021E+06													
255	15			.50000000E+06	.90000000E+06	.55177250E+05	.77077000E-01	.71587179E+06													
267	15			.90000000E+06	.13500000E+07	.12413607E+06	.10949206E+00	.11337450E+07													
279	15			.13500000E+07	.18000000E+07	.19255472E+06	.12202794E+00	.15779561E+07													
291	15			.18000000E+07	.22000000E+07	.22395700E+06	.11195300E+00	.20004555E+07													
303	15			.22000000E+07	.26000000E+07	.26736360E+06	.11144400E+00	.23990847E+07													
315	15			.26000000E+07	.30000000E+07	.29870680E+06	.10681000E+00	.27966183E+07													
327	15			.30000000E+07	.40000000E+07	.64049500E+06	.18751500E+00	.34167667E+07													
339	15			.40000000E+07	.50000000E+07	.41782600E+06	.94886750E-01	.44034178E+07													
351	15			.50000000E+07	.70000000E+07	.19452250E+06	.37352500E-01	.52077505E+07													
375	15			.40000000E+06	.50000000E+06	.66207000E+04	.14391250E-01	.46005038E+06													
381	15			.50000000E+06	.90000000E+06	.53313150E+05	.74475000E-01	.71585297E+06													
387	15			.90000000E+06	.13500000E+07	.11995469E+06	.10580350E+00	.11337497E+07													
393	15			.13500000E+07	.18000000E+07	.18606746E+06	.11791525E+00	.15779762E+07													
399	15			.18000000E+07	.22000000E+07	.21591240E+06	.10793200E+00	.20004484E+07													
405	15			.22000000E+07	.26000000E+07	.25833840E+06	.10768200E+00	.23990862E+07													
411	15			.26000000E+07	.30000000E+07	.28861980E+06	.10320300E+00	.27966222E+07													
417	15			.30000000E+07	.40000000E+07	.62642250E+06	.18310750E+00	.34210641E+07													
423	15			.40000000E+07	.50000000E+07	.43409400E+06	.98260750E-01	.44177762E+07													



TABLE III (continued)

429	15	.5000000E+07	.7000000E+07	.33518650E+06	.61566500E-01	.54443001E+07
435	15	.7000000E+07	.1000000E+08	.74115383E-09	.10587912E-15	.70000000E+07
441	15	.4000000E+06	.5000000E+06	.62988000E+04	.13691000E-01	.46006866E+06
446	15	.5000000E+06	.9000000E+06	.50726650E+05	.70862750E-01	.71584366E+06
451	15	.9000000E+06	.1350000E+07	.11410785E+06	.10064669E+00	.11337467E+07
456	15	.1350000E+07	.1800000E+07	.17700490E+06	.11217256E+00	.15779697E+07
461	15	.1800000E+07	.2200000E+07	.20540460E+06	.10267900E+00	.20004538E+07
466	15	.2200000E+07	.2600000E+07	.24575120E+06	.10243600E+00	.23990706E+07
471	15	.2600000E+07	.3000000E+07	.27453400E+06	.98166000E-01	.27966302E+07
476	15	.3000000E+07	.4000000E+07	.60261500E+06	.17593750E+00	.34251652E+07
481	15	.4000000E+07	.5000000E+07	.46293375E+06	.10435225E+00	.44362604E+07
486	15	.5000000E+07	.7000000E+07	.49334300E+06	.87542000E-01	.56355007E+07
491	15	.7000000E+07	.1000000E+08	.49703500E+05	.71005000E-02	.70000000E+07
496	15	.4000000E+06	.5000000E+06	.60465000E+04	.13143500E-01	.46003728E+06
499	15	.5000000E+06	.9000000E+06	.48697150E+05	.68024500E-01	.71587663E+06
502	15	.9000000E+06	.1350000E+07	.10955477E+06	.96630312E-01	.11337516E+07
505	15	.1350000E+07	.1800000E+07	.14995017E+06	.10770269E+00	.15779567E+07
508	15	.1800000E+07	.2200000E+07	.19692640E+06	.98452000E-01	.20002275E+07
511	15	.2200000E+07	.2600000E+07	.23513980E+06	.98003000E-01	.23993123E+07
514	15	.2600000E+07	.3000000E+07	.26361000E+06	.94260000E-01	.27966264E+07
517	15	.3000000E+07	.4000000E+07	.58627500E+06	.17091500E+00	.34302138E+07
520	15	.4000000E+07	.5000000E+07	.47496250E+06	.10687250E+00	.44441975E+07
523	15	.5000000E+07	.7000000E+07	.60786200E+06	.10613600E+00	.57271991E+07
526	15	.7000000E+07	.1000000E+08	.11832340E+06	.16421800E-01	.72052637E+07

-----ZONE 3 -----MATERIAL 3 -----

INDEX	ILOI	MT	NUMBER	GAMMA ENERGY RANGE		OUTPUT FROM PRI5		EHAT
						NUMERATOR	DENOMINATOR	
1	15		.4000000E+06	.5000000E+06	.46782700E+04	.10464300E-01	.46618216E+06	
5	15		.5000000E+06	.9000000E+06	.45350940E+05	.62620600E-01	.72421759E+06	
9	15		.9000000E+06	.1350000E+07	.11353927E+06	.99762937E-01	.11380907E+07	
13	15		.1350000E+07	.1800000E+07	.18616027E+06	.11782256E+00	.15800053E+07	
17	15		.1800000E+07	.2200000E+07	.22288160E+06	.11138000E+00	.20010918E+07	
21	15		.2200000E+07	.2600000E+07	.26158880E+06	.10913200E+00	.23969945E+07	
25	15		.2600000E+07	.3000000E+07	.27935840E+06	.99998000E-01	.27936399E+07	
29	15		.3000000E+07	.4000000E+07	.63512000E+07	.18461250E+00	.34402871E+07	
33	15		.4000000E+07	.5000000E+07	.46916750E+06	.10819150E+00	.43364543E+07	
37	15		.5000000E+07	.7000000E+07	.40756215E+06	.73310450E-01	.55594005E+07	
41	15		.7000000E+07	.1000000E+08	.28706650E+05	.41009500E-02	.70000000E+07	
45	15		.4000000E+06	.5000000E+06	.46803600E+04	.10040275E-01	.46615855E+06	
51	15		.5000000E+06	.9000000E+06	.43514070E+05	.60082175E-01	.72424259E+06	
57	15		.9000000E+06	.1350000E+07	.10895967E+06	.95738375E-01	.11380982E+07	
63	15		.1350000E+07	.1800000E+07	.17866477E+06	.11307887E+00	.15800013E+07	
69	15		.1800000E+07	.2200000E+07	.21393700E+06	.10690900E+00	.20011131E+07	
75	15		.2200000E+07	.2600000E+07	.25105600E+06	.10473800E+00	.23969906E+07	
81	15		.2600000E+07	.3000000E+07	.26811040E+06	.95972000E-01	.27936315E+07	
87	15		.3000000E+07	.4000000E+07	.60939500E+06	.17713750E+00	.34402371E+07	
93	15		.4000000E+07	.5000000E+07	.47472750E+06	.10872050E+00	.43664948E+07	
99	15		.5000000E+07	.7000000E+07	.54658250E+06	.95935500E-01	.56973956E+07	
105	15		.7000000E+07	.1000000E+08	.99525000E+05	.13792500E-01	.72158782E+07	
111	15		.4000000E+06	.5000000E+06	.44811600E+04	.96125250E-02	.46617928E+06	
116	15		.5000000E+06	.9000000E+06	.41661570E+05	.57525425E-01	.72422881E+06	
121	15		.9000000E+06	.1350000E+07	.1043312E+06	.91673562E-01	.11380939E+07	
126	15		.1350000E+07	.1800000E+07	.17103862E+06	.10825319E+00	.15799870E+07	
131	15		.1800000E+07	.2200000E+07	.20479000E+06	.10233800E+00	.20011140E+07	
136	15		.2200000E+07	.2600000E+07	.24032240E+06	.10026000E+00	.23969918E+07	
141	15		.2600000E+07	.3000000E+07	.25669680E+06	.91886000E-01	.27936443E+07	
146	15		.3000000E+07	.4000000E+07	.58348750E+06	.16960750E+00	.34402233E+07	
151	15		.4000000E+07	.5000000E+07	.47092000E+06	.10737200E+00	.43858734E+07	
156	15		.5000000E+07	.7000000E+07	.62029800E+06	.10785500E+00	.57512215E+07	
161	15		.7000000E+07	.1000000E+08	.28721750E+06	.36521500E-01	.78643402E+07	
166	15		.4000000E+06	.5000000E+06	.43689000E+04	.93717500E-02	.46617761E+06	
169	15		.5000000E+06	.9000000E+06	.40624500E+05	.56092500E-01	.72424121E+06	
172	15		.9000000E+06	.1350000E+07	.10171830E+06	.89376562E-01	.11380870E+07	
175	15		.1350000E+07	.1800000E+07	.16676310E+06	.10554619E+00	.15800012E+07	
178	15		.1800000E+07	.2200000E+07	.19967220E+06	.99781000E-01	.20011044E+07	
181	15		.2200000E+07	.2600000E+07	.23456920E+06	.97852000E-01	.23971835E+07	
184	15		.2600000E+07	.3000000E+07	.25022320E+06	.89582000E-01	.27932308E+07	
187	15		.3000000E+07	.4000000E+07	.56828000E+06	.16515500E+00	.34408889E+07	
190	15		.4000000E+07	.5000000E+07	.46858250E+06	.10657950E+00	.43965537E+07	
193	15		.5000000E+07	.7000000E+07	.66979750E+06	.11576750E+00	.57857127E+07	
196	15		.7000000E+07	.1000000E+08	.37118805E+06	.47317295E-01	.78446591E+07	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 1

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	2.49268E-03	0.	0.	0.	0.	0.	0.
2	0.	8.71466E-04	0.	0.	0.	0.	0.	0.
3	0.	1.96759E-02	0.	0.	0.	0.	0.	0.
4	0.	5.03455E-02	0.	0.	0.	0.	0.	0.
5	0.	3.14871E-02	0.	0.	0.	0.	0.	0.
6	0.	4.01304E-02	0.	0.	0.	0.	0.	0.
7	0.	1.05218E-02	0.	0.	0.	0.	0.	0.
8	0.	7.10706E-02	0.	0.	0.	0.	0.	0.
9	0.	3.58987E-03	0.	0.	0.	0.	0.	0.
10	0.	1.01278E-02	0.	0.	0.	0.	0.	0.
11	5.40831E-01	1.66637E-01	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	0.	0.						
2	0.	0.						
3	0.	0.						
4	0.	0.						
5	0.	0.						
6	0.	0.						
7	0.	0.						
8	0.	0.						
9	0.	0.						
10	0.	0.						
11	0.	0.						

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 2

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	2.25275E-04	4.64928E-04	5.32968E-04
2	0.	0.	0.	0.	0.	1.68578E-04	3.47915E-04	3.98830E-04
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	2.36876E-03	4.88871E-03	5.60416E-03
5	0.	0.	0.	0.	0.	1.15462E-03	2.38294E-03	2.73167E-03
6	0.	0.	0.	0.	0.	2.22744E-04	4.59704E-04	5.26980E-04
7	0.	0.	0.	0.	0.	2.13072E-04	4.39744E-04	5.04098E-04
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	5.03021E-04	1.03815E-03	1.19008E-03
10	0.	0.	0.	0.	0.	1.41912E-03	2.92883E-03	3.35745E-03
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	5.37555E-04	5.31121E-04	5.82686E-04	7.16038E-04	3.19018E-03	1.70624E-03	2.45491E-03	6.19686E-03
2	4.02263E-04	3.97449E-04	4.36035E-04	5.35825E-04	2.38728E-03	1.27681E-03	1.83706E-03	4.63723E-03
3	0.	0.	0.	0.	0.	0.	0.	0.
4	5.65239E-03	5.58474E-03	6.12694E-03	7.52914E-03	3.35447E-02	1.79411E-02	2.58134E-02	6.51600E-02
5	2.75518E-03	2.72220E-03	2.98649E-03	3.66997E-03	1.63509E-02	8.74512E-03	1.25824E-02	3.17613E-02
6	5.31516E-04	5.25154E-04	5.76139E-04	7.07994E-04	3.15434E-03	1.68707E-03	2.42733E-03	6.12724E-03
7	5.08437E-04	5.02352E-04	5.51123E-04	6.77252E-04	3.01738E-03	1.61381E-03	2.32193E-03	5.86119E-03
8	0.	0.	0.	0.	0.	0.	0.	0.
9	1.20032E-03	1.18595E-03	1.30109E-03	1.59886E-03	7.12343E-03	3.80989E-03	5.48162E-03	1.38371E-02
10	3.38634E-03	3.34581E-03	3.67064E-03	4.51070E-03	2.00966E-02	1.07485E-02	1.54648E-02	3.90373E-02
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	1.67142E-03	7.65813E-04	9.97565E-03	3.07345E-03	1.69131E-03	2.79602E-03	2.65832E-03	3.77502E-03
2	1.25076E-03	5.73073E-04	7.46498E-03	2.29992E-03	1.26564E-03	2.09231E-03	1.98928E-03	2.82492E-03
3	0.	0.	0.	0.	0.	0.	0.	0.
4	1.75750E-02	8.05252E-03	1.04894E-01	3.23173E-02	1.77841E-02	2.94001E-02	2.79523E-02	3.96943E-02
5	8.56669E-03	3.92509E-03	5.11291E-02	1.57526E-02	8.66862E-03	1.43307E-02	1.36249E-02	1.93484E-02
6	1.65264E-03	7.57209E-04	9.86358E-03	3.03892E-03	1.67231E-03	2.76460E-03	2.62846E-03	3.73261E-03
7	1.58088E-03	7.24331E-04	9.43529E-03	2.90697E-03	1.59969E-03	2.64456E-03	2.51433E-03	3.57053E-03
8	0.	0.	0.	0.	0.	0.	0.	0.
9	3.73216E-03	1.71000E-03	2.22749E-02	6.86277E-03	3.77656E-03	6.24329E-03	5.93583E-03	8.42932E-03
10	1.05292E-02	4.82426E-03	6.28419E-02	1.93613E-02	1.06544E-02	1.76136E-02	1.67462E-02	2.37808E-02
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 25	GROUP 26	GROUP
1	4.65244E-03	6.59411E-03	
2	3.48151E-03	4.93451E-03	
3	0.	0.	
4	4.89204E-02	6.93371E-02	
5	2.38456E-02	3.37974E-02	
6	4.60017E-03	6.52003E-03	
7	4.40043E-03	6.23693E-03	
8	0.	0.	
9	1.03885E-02	1.47241E-02	
10	2.93002E-02	4.15398E-02	
11	0.	0.	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 3

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	8.37424E-15	0.	0.	0.	0.	0.
3	0.	0.	5.96705E-03	0.	0.	0.	0.	0.
4	0.	0.	8.57543E-02	1.13475E-02	0.	0.	0.	0.
5	0.	0.	1.35131E-01	7.30168E-02	0.	0.	0.	0.
6	0.	0.	1.84105E-03	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	2.25918E-01	2.82302E-01	8.90859E-02	0.	0.	0.
9	0.	0.	1.57589E-01	1.52537E-01	9.98537E-02	0.	0.	0.
10	0.	0.	1.50302E-03	6.19263E-11	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 4

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	0.	0.						
2	0.	0.						
3	0.	0.						
4	0.	0.						
5	0.	0.						
6	0.	0.						
7	0.	0.						
8	0.	0.						
9	0.	0.						
10	0.	0.						
11	0.	0.						

## PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 5

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	4.79425E-03	0.	0.	0.	5.26094E-04	3.96047E-03	7.18867E-03	1.05645E-02
2	8.61033E-02	3.63571E-02	0.	0.	2.33499E-03	1.75780E-02	3.19059E-02	4.68891E-02
3	1.20051E-01	1.09488E-01	0.	0.	1.67197E-03	1.25867E-02	2.28462E-02	3.35749E-02
4	2.14624E-01	4.05126E-01	1.83639E-01	5.77015E-03	2.32058E-03	1.74695E-02	3.17089E-02	4.65997E-02
5	1.20451E-01	2.39808E-01	1.43481E-01	2.47068E-02	7.56710E-04	5.69656E-03	1.03399E-02	1.51955E-02
6	1.25647E-01	1.71660E-01	7.77110E-02	4.84230E-02	1.00895E-03	7.59542E-03	1.37865E-02	2.02607E-02
7	1.25982E-01	1.42053E-01	0.	0.	1.58549E-03	1.19357E-02	2.16645E-02	3.18383E-02
8	1.37627E-01	1.61149E-01	9.41182E-03	3.53499E-03	2.40035E-03	1.57334E-02	2.85577E-02	4.19686E-02
9	1.23488E-01	1.51896E-01	3.08341E-02	1.17747E-02	1.93846E-03	4.88277E-03	8.86275E-03	1.30247E-02
10	8.69303E-02	1.25011E-01	2.17163E-02	3.30837E-04	2.45030E-03	1.84460E-02	3.34815E-02	4.92046E-02
11	1.67972E-02	1.89212E-02	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	1.36119E-02	1.55028E-02	1.61914E-02	2.38670E-02	3.94358E-02	5.52331E-02	7.23480E-02	9.05792E-02
2	6.04145E-02	6.88072E-02	7.18632E-02	1.05930E-01	1.75030E-01	2.45144E-01	3.21106E-01	4.02023E-01
3	4.32598E-02	4.92693E-02	5.14576E-02	7.58513E-02	1.25330E-01	1.75535E-01	2.29928E-01	2.87868E-01
4	6.00416E-02	6.83824E-02	7.14196E-02	1.05276E-01	1.73950E-01	2.43631E-01	3.19124E-01	3.99541E-01
5	1.95788E-02	2.22986E-02	2.32890E-02	3.43292E-02	5.67228E-02	7.94449E-02	1.04062E-01	1.30285E-01
6	2.61050E-02	2.97315E-02	3.10520E-02	4.57723E-02	7.56303E-02	1.05927E-01	1.38750E-01	1.73714E-01
7	4.10222E-02	4.67209E-02	4.87960E-02	7.19279E-02	1.18848E-01	1.66456E-01	2.18035E-01	2.72799E-01
8	5.40747E-02	6.15867E-02	6.43220E-02	9.48141E-02	1.56663E-01	2.19419E-01	2.87410E-01	3.59835E-01
9	1.67818E-02	1.91131E-02	1.99620E-02	2.94251E-02	4.86195E-02	6.80956E-02	8.91961E-02	1.11673E-01
10	6.33979E-02	7.22051E-02	7.54120E-02	1.11161E-01	1.83674E-01	2.57250E-01	3.36963E-01	4.21876E-01
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	1.10555E-01	1.58314E-01	1.93801E-01	2.35210E-01	3.75501E-01	3.14242E-01	4.72093E-01	5.88498E-01
2	4.90683E-01	7.02655E-01	8.60157E-01	1.04394E+00	1.66661E+00	1.39472E+00	2.09532E+00	2.61196E+00
3	3.51353E-01	5.03136E-01	6.15915E-01	7.47516E-01	1.19337E+00	9.98687E-01	1.50035E+00	1.87029E+00
4	4.87654E-01	6.98318E-01	8.54847E-01	1.03750E+00	1.65632E+00	1.38611E+00	2.08238E+00	2.59584E+00
5	1.59018E-01	2.27712E-01	2.78755E-01	3.38315E-01	5.40104E-01	4.51992E-01	6.79038E-01	8.46469E-01
6	2.12023E-01	3.03616E-01	3.71673E-01	4.51087E-01	7.20138E-01	6.02656E-01	9.05385E-01	1.12863E+00
7	3.33180E-01	4.77111E-01	5.84057E-01	7.08851E-01	1.13165E+00	9.47031E-01	1.42275E+00	1.77355E+00
8	4.39191E-01	6.28920E-01	7.69894E-01	9.34395E-01	1.49172E+00	1.24836E+00	1.87544E+00	2.33787E+00
9	1.36301E-01	1.95182E-01	2.38933E-01	2.89985E-01	4.62946E-01	3.87422E-01	5.82033E-01	7.25545E-01
10	5.14914E-01	7.37354E-01	9.02634E-01	1.09550E+00	1.74891E+00	1.46359E+00	2.19879E+00	2.74095E+00
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 25	GROUP 26	GROUP
1	4.84743E-01	1.35812E+00	
2	2.15146E+00	6.02780E+00	
3	1.54055E+00	4.31620E+00	
4	2.13818E+00	5.99059E+00	
5	6.97233E-01	1.95345E+00	
6	9.29644E-01	2.60460E+00	
7	1.46087E+00	4.09295E+00	
8	1.92569E+00	5.39525E+00	
9	5.97628E-01	1.67439E+00	
10	2.25771E+00	6.32547E+00	
11	0.	0.	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 6

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	2.59923E-02	7.33992E-05	0.	0.	0.	0.	0.	0.
2	1.11998E-01	1.19142E-03	0.	0.	0.	0.	0.	0.
3	1.22693E-01	1.73197E-03	0.	0.	0.	0.	0.	0.
4	1.98330E-01	2.94863E-03	0.	0.	0.	0.	0.	0.
5	1.07457E-01	1.59718E-03	0.	0.	0.	0.	0.	0.
6	1.17272E-01	1.74307E-03	0.	0.	0.	0.	0.	0.
7	1.19691E-01	1.77899E-03	0.	0.	0.	0.	0.	0.
8	1.26607E-01	1.88188E-03	0.	0.	0.	0.	0.	0.
9	1.07202E-01	1.59342E-03	0.	0.	0.	0.	0.	0.
10	6.72763E-02	1.00017E-03	0.	0.	0.	0.	0.	0.
11	1.12421E-02	1.67135E-04	0.	0.	0.	0.	0.	0.

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 7

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	1.49561E-04	0.	0.	0.	0.	0.	0.
2	0.	5.22879E-05	0.	0.	0.	0.	0.	0.
3	0.	1.18055E-03	0.	0.	0.	0.	0.	0.
4	0.	3.02073E-03	0.	0.	0.	0.	0.	0.
5	0.	1.88923E-03	0.	0.	0.	0.	0.	0.
6	0.	2.40782E-03	0.	0.	0.	0.	0.	0.
7	0.	6.31307E-04	0.	0.	0.	0.	0.	0.
8	0.	4.26424E-03	0.	0.	0.	0.	0.	0.
9	0.	2.15392E-04	0.	0.	0.	0.	0.	0.
10	0.	6.07667E-04	0.	0.	0.	0.	0.	0.
11	3.24499E-02	9.99820E-03	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 25	GROUP 26	GROUP
1	2.32622E-04	3.29706E-04	
2	1.74076E-04	2.46725E-04	
3	0.	0.	
4	2.44602E-03	3.46685E-03	
5	1.19228E-03	1.68987E-03	
6	2.30008E-04	3.26002E-04	
7	2.20021E-04	3.11846E-04	
8	0.	0.	
9	5.19427E-04	7.36207E-04	
10	1.46541E-03	2.07699E-03	
11	0.	0.	

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 9

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	3.55808E-04	7.33992E-07	0.	0.	1.05219E-05	7.92093E-05	1.43773E-04	2.11290E-04
2	2.84204E-03	7.39057E-04	0.	0.	4.66998E-05	3.51559E-04	6.38118E-04	9.37782E-04
3	3.62795E-03	2.20708E-03	0.	0.	3.34394E-05	2.51734E-04	4.56924E-04	6.71498E-04
4	6.27579E-03	8.13201E-03	3.67278E-03	1.15403E-04	4.64115E-05	3.49389E-04	6.34179E-04	9.31993E-04
5	3.48360E-03	4.81213E-03	2.86963E-03	4.94137E-04	1.51342E-05	1.13931E-04	2.06797E-04	3.03911E-04
6	3.68566E-03	3.45062E-03	1.55422E-03	9.68460E-04	2.01789E-05	1.51908E-04	2.75730E-04	4.05214E-04
7	3.71654E-03	2.85885E-03	0.	0.	3.17097E-05	2.38713E-04	4.33290E-04	6.36765E-04
8	4.01860E-03	3.24181E-03	1.88236E-04	7.06997E-05	4.80071E-05	3.14667E-04	5.71155E-04	8.39373E-04
9	3.54177E-03	3.05385E-03	6.16682E-04	2.35494E-04	3.87692E-05	9.76553E-05	1.77255E-04	2.60495E-04
10	2.41137E-03	2.51023E-03	4.34325E-04	6.61675E-06	4.90060E-05	3.68920E-04	6.69630E-04	9.84092E-04
11	4.48365E-04	3.80096E-04	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	2.72238E-04	3.10057E-04	3.23828E-04	4.77340E-04	7.88717E-04	1.10466E-03	1.44696E-03	1.81158E-03
2	1.20829E-03	1.37614E-03	1.43726E-03	2.11860E-03	3.50060E-03	4.90289E-03	6.42212E-03	8.04046E-03
3	8.65195E-04	9.85387E-04	1.02915E-03	1.51703E-03	2.50661E-03	3.51071E-03	4.59856E-03	5.75737E-03
4	1.20083E-03	1.36765E-03	1.42839E-03	2.10553E-03	3.47900E-03	4.87262E-03	6.38248E-03	7.99083E-03
5	3.91575E-04	4.45972E-04	4.65780E-04	6.86585E-04	1.13446E-03	1.58890E-03	2.08124E-03	2.60570E-03
6	5.22101E-04	5.94630E-04	6.21040E-04	9.15447E-04	1.51261E-03	2.11853E-03	2.77499E-03	3.47427E-03
7	8.20444E-04	9.34418E-04	9.75920E-04	1.43856E-03	2.37695E-03	3.32912E-03	4.36070E-03	5.45957E-03
8	1.08149E-03	1.23173E-03	1.28644E-03	1.89628E-03	3.13326E-03	4.38839E-03	5.74820E-03	7.19671E-03
9	3.35636E-04	3.82262E-04	3.99240E-04	5.88501E-04	9.72390E-04	1.36191E-03	1.78392E-03	2.23346E-03
10	1.26796E-03	1.44410E-03	1.50824E-03	2.22323E-03	3.67347E-03	5.14500E-03	6.73926E-03	8.43752E-03
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	2.21110E-03	3.16629E-03	3.87602E-03	4.70419E-03	7.51001E-03	6.28484E-03	9.44167E-03	1.17700E-02
2	9.81365E-03	1.40531E-02	1.72031E-02	2.08789E-02	3.33321E-02	2.78944E-02	4.19064E-02	5.22392E-02
3	7.02706E-03	1.00627E-02	1.23183E-02	1.49503E-02	2.38674E-02	1.99737E-02	3.00070E-02	3.74059E-02
4	9.75307E-03	1.39664E-02	1.70969E-02	2.07500E-02	3.31264E-02	2.77222E-02	4.16477E-02	5.19168E-02
5	3.18035E-03	4.55425E-03	5.57509E-03	6.76631E-03	1.08021E-02	9.03984E-03	1.35808E-02	1.69294E-02
6	4.24047E-03	6.07233E-03	7.43346E-03	9.02174E-03	1.44028E-02	1.20531E-02	1.81077E-02	2.25725E-02
7	6.66359E-03	9.54223E-03	1.16811E-02	1.41770E-02	2.26329E-02	1.89406E-02	2.84549E-02	3.54711E-02
8	8.78382E-03	1.25784E-02	1.53979E-02	1.86879E-02	2.98343E-02	2.49672E-02	3.75088E-02	4.67573E-02
9	2.72601E-03	3.90364E-03	4.77865E-03	5.79969E-03	9.25892E-03	7.74843E-03	1.16407E-02	1.45109E-02
10	1.02983E-02	1.47471E-02	1.80527E-02	2.19099E-02	3.49782E-02	2.92719E-02	4.39758E-02	5.48190E-02
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	9.69486E-03	2.71623E-02						
2	4.30292E-02	1.20556E-01						
3	3.08111E-02	8.63240E-02						
4	4.27636E-02	1.19812E-01						
5	1.39447E-02	3.90691E-02						
6	1.85929E-02	5.20921E-02						
7	2.92174E-02	8.18590E-02						
8	3.85138E-02	1.07905E-01						
9	1.19526E-02	3.34878E-02						
10	4.51541E-02	1.26509E-01						
11	0.	0.						

TABLE III (continued)

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	0.	0.						
2	0.	0.						
3	0.	0.						
4	0.	0.						
5	0.	0.						
6	0.	0.						
7	0.	0.						
8	0.	0.						
9	0.	0.						
10	0.	0.						
11	0.	0.						

PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 8

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	1.12637E-05	2.32464E-05	2.66484E-05
2	0.	0.	3.34970E-16	0.	0.	8.42888E-06	1.73957E-05	1.99415E-05
3	0.	0.	2.38682E-04	0.	0.	0.	0.	0.
4	0.	0.	3.43017E-03	4.53899E-04	0.	1.18438E-04	2.44436E-04	2.80208E-04
5	0.	0.	5.40523E-03	2.92067E-03	0.	5.77310E-05	1.19147E-04	1.36583E-04
6	0.	0.	7.36422E-05	0.	0.	1.11372E-05	2.29852E-05	2.63490E-05
7	0.	0.	0.	0.	0.	1.06536E-05	2.19877E-05	2.52049E-05
8	0.	0.	9.03674E-03	1.12921E-02	3.56344E-03	0.	0.	0.
9	0.	0.	6.30354E-03	6.10149E-03	3.99415E-03	2.51511E-05	5.19074E-05	5.95038E-05
10	0.	0.	6.01208E-05	2.47705E-12	0.	7.09562E-05	1.46441E-04	1.67872E-04
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	2.68778E-05	2.65561E-05	2.91343E-05	3.58019E-05	1.59509E-04	8.53118E-05	1.22746E-04	3.09843E-04
2	2.01132E-05	1.98724E-05	2.18018E-05	2.67913E-05	1.19364E-04	6.38405E-05	9.18529E-05	2.31862E-04
3	0.	0.	0.	0.	0.	0.	0.	0.
4	2.82620E-04	2.79237E-04	3.06347E-04	3.76457E-04	1.67724E-03	8.97053E-04	1.29067E-03	3.25800E-03
5	1.37759E-04	1.36110E-04	1.49325E-04	1.83499E-04	8.17546E-04	4.37256E-04	6.29119E-04	1.58807E-03
6	2.65758E-05	2.62577E-05	2.88070E-05	3.53997E-05	1.57717E-04	8.43533E-05	1.21367E-04	3.06362E-04
7	2.54218E-05	2.51176E-05	2.75561E-05	3.38626E-05	1.50869E-04	8.06906E-05	1.16097E-04	2.93059E-04
8	0.	0.	0.	0.	0.	0.	0.	0.
9	6.00159E-05	5.92976E-05	6.50546E-05	7.99429E-05	3.56171E-04	1.90494E-04	2.74081E-04	6.91855E-04
10	1.69317E-04	1.67291E-04	1.83532E-04	2.25535E-04	1.00483E-03	5.37424E-04	7.73239E-04	1.95186E-03
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	8.35711E-05	3.82907E-05	4.98783E-04	1.53673E-04	8.45654E-05	1.39801E-04	1.32914E-04	1.88751E-04
2	6.25379E-05	2.86537E-05	3.73249E-04	1.14996E-04	6.32820E-05	1.04616E-04	9.94638E-05	1.41246E-04
3	0.	0.	0.	0.	0.	0.	0.	0.
4	8.78750E-04	4.02626E-04	5.24470E-03	1.61587E-03	8.89205E-04	1.47001E-03	1.39761E-03	1.98471E-03
5	4.28334E-04	1.96254E-04	2.55645E-03	7.87631E-04	4.33431E-04	7.16534E-04	6.81247E-04	9.67422E-04
6	8.26322E-05	3.78605E-05	4.93179E-04	1.51946E-04	8.36154E-05	1.38230E-04	1.31423E-04	1.86630E-04
7	7.90442E-05	3.62165E-05	4.71765E-04	1.45348E-04	7.99847E-05	1.32228E-04	1.25716E-04	1.78527E-04
8	0.	0.	0.	0.	0.	0.	0.	0.
9	1.86608E-04	8.55000E-05	1.11374E-03	3.43139E-04	1.88828E-04	3.12164E-04	2.96791E-04	4.21466E-04
10	5.26459E-04	2.41213E-04	3.14210E-03	9.68064E-04	5.32722E-04	8.80079E-04	8.37309E-04	1.18904E-03
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

PHOTON PRODUCTION SOURCE VECTORS AT INDICATED MESH INTERVALS

FOR MESH INTERVAL 1 BOUNDED BY RADII R= 0. AND R= 1.0000E+00 THE VECTOR IS									
2.99121185E+08	1.04575880E+08	2.36110834E+09	6.04145688E+09	3.77845681E+09	4.81564585E+09	1.26261364E+09	8.52847253E+09		
4.30784467E+08	1.21533336E+09	5.24462832E+10							
FOR MESH INTERVAL 2 BOUNDED BY RADII R= 1.0000E+00 AND R= 2.0000E+00 THE VECTOR IS									
2.99121185E+08	1.04575880E+08	2.36110834E+09	6.04145688E+09	3.77845681E+09	4.81564585E+09	1.26261364E+09	8.52847253E+09		
4.30784467E+08	1.21533336E+09	5.24462832E+10							
FOR MESH INTERVAL 3 BOUNDED BY RADII R= 2.0000E+00 AND R= 3.0000E+00 THE VECTOR IS									
2.99121185E+08	1.04575880E+08	2.36110834E+09	6.04145688E+09	3.77845681E+09	4.81564585E+09	1.26261364E+09	8.52847253E+09		
4.30784467E+08	1.21533336E+09	5.24462832E+10							
FOR MESH INTERVAL 4 BOUNDED BY RADII R= 3.0000E+00 AND R= 4.0000E+00 THE VECTOR IS									
5.32544491E+09	3.98513582E+09	7.16046338E+07	5.72076453E+10	3.00848123E+10	5.28770710E+09	5.03697663E+09	9.00957538E+09		
1.82200358E+10	3.35658284E+10	0.							
FOR MESH INTERVAL 5 BOUNDED BY RADII R= 4.0000E+00 AND R= 6.0000E+00 THE VECTOR IS									
5.32544491E+09	3.98513582E+09	7.16046338E+07	5.72076453E+10	3.00848123E+10	5.28770710E+09	5.03697663E+09	9.00957538E+09		
1.82200358E+10	3.35658284E+10	0.							
FOR MESH INTERVAL 6 BOUNDED BY RADII R= 6.0000E+00 AND R= 9.0000E+00 THE VECTOR IS									
5.32544491E+09	3.98513582E+09	7.16046338E+07	5.72076453E+10	3.00848123E+10	5.28770710E+09	5.03697663E+09	9.00957538E+09		
1.82200358E+10	3.35658284E+10	0.							
FOR MESH INTERVAL 7 BOUNDED BY RADII R= 9.0000E+00 AND R= 1.1000E+01 THE VECTOR IS									
5.32544491E+09	3.98513582E+09	7.16046338E+07	5.72076453E+10	3.00848123E+10	5.28770710E+09	5.03697663E+09	9.00957538E+09		
1.82200358E+10	3.35658284E+10	0.							
FOR MESH INTERVAL 8 BOUNDED BY RADII R= 1.1000E+01 AND R= 1.3000E+01 THE VECTOR IS									
2.10135116E+10	9.32927934E+10	6.68517337E+10	9.30141747E+10	3.04567080E+10	4.04842675E+10	6.34119664E+10	8.35779484E+10		
2.60283692E+10	9.79421226E+10	1.20855669E+07							
FOR MESH INTERVAL 9 BOUNDED BY RADII R= 1.3000E+01 AND R= 1.5000E+01 THE VECTOR IS									
2.10135116E+10	9.32927934E+10	6.68517337E+10	9.30141747E+10	3.04567080E+10	4.04842675E+10	6.34119664E+10	8.35779484E+10		
2.60283692E+10	9.79421226E+10	1.20855669E+07							

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 1

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	1.77229E+04	0.	0.	0.	0.	0.	0.
2	0.	5.81337E+03	0.	0.	0.	0.	0.	0.
3	0.	8.64877E+04	0.	0.	0.	0.	0.	0.
4	0.	1.85553E+05	0.	0.	0.	0.	0.	0.
5	0.	8.77429E+04	0.	0.	0.	0.	0.	0.
6	0.	9.45773E+04	0.	0.	0.	0.	0.	0.
7	0.	2.12524E+04	0.	0.	0.	0.	0.	0.
8	0.	1.18202E+05	0.	0.	0.	0.	0.	0.
9	0.	3.78220E+03	0.	0.	0.	0.	0.	0.
10	0.	6.32986E+03	0.	0.	0.	0.	0.	0.
11	2.37533E+05	7.31868E+04	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	0.	0.						
2	0.	0.						
3	0.	0.						
4	0.	0.						
5	0.	0.						
6	0.	0.						
7	0.	0.						
8	0.	0.						
9	0.	0.						
10	0.	0.						
11	0.	0.						



TABLE III (continued)

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 2

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	1.87575E+03	3.87122E+03	4.43775E+03
2	0.	0.	0.	0.	0.	1.06513E+03	2.19825E+03	2.51995E+03
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	8.70612E+03	1.79679E+04	2.05974E+04
5	0.	0.	0.	0.	0.	3.26626E+03	6.74100E+03	7.72751E+03
6	0.	0.	0.	0.	0.	5.63987E+02	1.16397E+03	1.33431E+03
7	0.	0.	0.	0.	0.	3.87844E+02	8.00443E+02	9.17584E+02
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	5.15557E+02	1.06402E+03	1.21973E+03
10	0.	0.	0.	0.	0.	8.28769E+02	1.71043E+03	1.96075E+03
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	4.47595E+03	4.42238E+03	4.85173E+03	5.96208E+03	2.65630E+04	1.42069E+04	2.04408E+04	5.15981E+04
2	2.54164E+03	2.51122E+03	2.75503E+03	3.38554E+03	1.50837E+04	8.06734E+03	1.16072E+04	2.92997E+04
3	0.	0.	0.	0.	0.	0.	0.	0.
4	2.07747E+04	2.05261E+04	2.25189E+04	2.76725E+04	1.23290E+05	6.59403E+04	9.48747E+04	2.39488E+05
5	7.79402E+03	7.70074E+03	8.44837E+03	1.03819E+04	4.62545E+04	2.47387E+04	3.55938E+04	8.98484E+04
6	1.34580E+03	1.32969E+03	1.45878E+03	1.79264E+03	7.98679E+03	4.27165E+03	6.14600E+03	1.55142E+04
7	9.25482E+02	9.14405E+02	1.00318E+03	1.23277E+03	5.49238E+03	2.93754E+03	4.22650E+03	1.06688E+04
8	0.	0.	0.	0.	0.	0.	0.	0.
9	1.23023E+03	1.21551E+03	1.33352E+03	1.63870E+03	7.30095E+03	3.90484E+03	5.61823E+03	1.41819E+04
10	1.97762E+03	1.95396E+03	2.14366E+03	2.63425E+03	1.17364E+04	6.27711E+03	9.03143E+03	2.27978E+04
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	1.39171E+04	6.37653E+03	8.30622E+04	2.55910E+04	1.40827E+04	2.32810E+04	2.21345E+04	3.14326E+04
2	7.90274E+03	3.62088E+03	4.71664E+04	1.45317E+04	7.99676E+03	1.32200E+04	1.25689E+04	1.78489E+04
3	0.	0.	0.	0.	0.	0.	0.	0.
4	6.45949E+04	2.95961E+04	3.85526E+05	1.18779E+05	6.53635E+04	1.08057E+05	1.02735E+05	1.45892E+05
5	2.42340E+04	1.11035E+04	1.44637E+05	4.45620E+04	2.45223E+04	4.05395E+04	3.85431E+04	5.47341E+04
6	4.18449E+03	1.91725E+03	2.49746E+04	7.69455E+03	4.23428E+03	6.99998E+03	6.65525E+03	9.45096E+03
7	2.87760E+03	1.31846E+03	1.71746E+04	5.29141E+03	2.91184E+03	4.81376E+03	4.57670E+03	6.49926E+03
8	0.	0.	0.	0.	0.	0.	0.	0.
9	3.82516E+03	1.75262E+03	2.28300E+04	7.03380E+03	3.87068E+03	6.39887E+03	6.08375E+03	8.63939E+03
10	6.14904E+03	2.81737E+03	3.66997E+04	1.13070E+04	6.22220E+03	1.02863E+04	9.77977E+03	1.38880E+04
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	3.87385E+04	5.49058E+04						
2	2.19974E+04	3.11780E+04						
3	0.	0.						
4	1.79801E+05	2.54841E+05						
5	6.74558E+04	9.56082E+04						
6	1.16476E+04	1.65087E+04						
7	8.00987E+03	1.13528E+04						
8	0.	0.						
9	1.06474E+04	1.50911E+04						
10	1.71160E+04	2.42593E+04						
11	0.	0.						

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 3

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	4.29599E-08	0.	0.	0.	0.	0.
3	0.	0.	2.46929E+04	0.	0.	0.	0.	0.
4	0.	0.	2.59016E+05	3.41105E+04	0.	0.	0.	0.
5	0.	0.	3.64004E+05	1.94275E+05	0.	0.	0.	0.
6	0.	0.	4.22706E+03	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	3.81556E+05	4.87552E+05	1.56969E+05	0.	0.	0.
9	0.	0.	1.92258E+05	1.86095E+05	1.21822E+05	0.	0.	0.
10	0.	0.	7.78564E+02	3.20778E+05	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 4

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

TABLE III (continued)

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 5

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	4.07511E+04	0.	0.	0.	4.17587E+03	3.14362E+04	5.70602E+04	8.38559E+04
2	5.16620E+05	2.18143E+05	0.	0.	1.30065E+04	9.79135E+04	1.77724E+05	2.61184E+05
3	5.40230E+05	4.92696E+05	0.	0.	7.23340E+03	5.44535E+04	9.88390E+04	1.45254E+05
4	7.51186E+05	1.43178E+06	6.26886E+05	1.74316E+04	7.99213E+03	6.01652E+04	1.09206E+05	1.60490E+05
5	3.37264E+05	6.73233E+05	4.04187E+05	6.95991E+04	2.18559E+03	1.64533E+04	2.98645E+04	4.38891E+04
6	3.01553E+05	4.15776E+05	1.96298E+05	1.22316E+05	2.50406E+03	1.88507E+04	3.42161E+04	5.02842E+04
7	2.51963E+05	2.84106E+05	0.	0.	3.19490E+03	2.40514E+04	4.36559E+04	6.41570E+04
8	2.20203E+05	2.57346E+05	1.43060E+04	5.37318E+03	3.88737E+03	2.57127E+04	4.66712E+04	6.85883E+04
9	1.35836E+05	1.69265E+05	3.91593E+04	1.49539E+04	2.32333E+03	5.15837E+03	9.36300E+03	1.37599E+04
10	6.08512E+04	8.98942E+04	1.71124E+04	2.60700E+02	1.89163E+03	1.42403E+04	2.58477E+04	3.79860E+04
11	7.55875E+03	8.51455E+03	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	1.08045E+05	1.23054E+05	1.28519E+05	1.89444E+05	3.13022E+05	4.38413E+05	5.74263E+05	7.18973E+05
2	3.36523E+05	3.83272E+05	4.00295E+05	5.90057E+05	9.74961E+05	1.36551E+06	1.78864E+06	2.23936E+06
3	1.87154E+05	2.13153E+05	2.22620E+05	3.28154E+05	5.42213E+05	7.59415E+05	9.94731E+05	1.24540E+06
4	2.06785E+05	2.35511E+05	2.45971E+05	3.62574E+05	5.99087E+05	8.39071E+05	1.09907E+06	1.37603E+06
5	5.65491E+04	6.44048E+04	6.72653E+04	9.91527E+04	1.63832E+05	2.29460E+05	3.00561E+05	3.76301E+05
6	6.47890E+04	7.37893E+04	7.70666E+04	1.13600E+05	1.87704E+05	2.62895E+05	3.44357E+05	4.31132E+05
7	8.26634E+04	9.41469E+04	9.83284E+04	1.44941E+05	2.39489E+05	3.35424E+05	4.39360E+05	5.50077E+05
8	8.83730E+04	1.00650E+05	1.05120E+05	1.54952E+05	2.56030E+05	3.58592E+05	4.69707E+05	5.88070E+05
9	1.77290E+04	2.01919E+04	2.10887E+04	3.10859E+04	5.13638E+04	7.19393E+04	9.42304E+04	1.17976E+05
10	4.89432E+04	5.57423E+04	5.82181E+04	8.58166E+04	1.41796E+05	1.98597E+05	2.60136E+05	3.25688E+05
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	8.77531E+05	1.25662E+06	1.53830E+06	1.86698E+06	2.98054E+06	2.49430E+06	3.74724E+06	4.67120E+06
2	2.73322E+06	3.91396E+06	4.79128E+06	5.81502E+06	9.28340E+06	7.76892E+06	1.16714E+07	1.45493E+07
3	1.52005E+06	2.17670E+06	2.66462E+06	3.23396E+06	5.16286E+06	4.32060E+06	6.49094E+06	8.09141E+06
4	1.67949E+06	2.40502E+06	2.94412E+06	3.57318E+06	5.70440E+06	4.77379E+06	7.17178E+06	8.94013E+06
5	4.59288E+05	6.57698E+05	8.05123E+05	9.77151E+05	1.55997E+06	1.30548E+06	1.96126E+06	2.44484E+06
6	5.26212E+05	7.53533E+05	9.22439E+05	1.11953E+06	1.78728E+06	1.49571E+06	2.24704E+06	2.80109E+06
7	6.71387E+05	9.61423E+05	1.17693E+06	1.42840E+06	2.28037E+06	1.90835E+06	2.86697E+06	3.57387E+06
8	7.17760E+05	1.02783E+06	1.25822E+06	1.52706E+06	2.43787E+06	2.04016E+06	3.06499E+06	3.82072E+06
9	1.43994E+05	2.06199E+05	2.52419E+05	3.06353E+05	4.89077E+05	4.09289E+05	6.14885E+05	7.66498E+05
10	3.97514E+05	5.69237E+05	6.96833E+05	8.45724E+05	1.35016E+06	1.12989E+06	1.69747E+06	2.11601E+06
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP	GROUP	GROUP	GROUP	GROUP	GROUP
1	3.84765E+06	1.07800E+07						
2	1.19842E+07	3.35763E+07						
3	6.66486E+06	1.86731E+07						
4	7.36395E+06	2.06317E+07						
5	2.01381E+06	5.64213E+06						
6	2.30724E+06	6.46426E+06						
7	2.94378E+06	8.24767E+06						
8	3.14711E+06	8.81733E+06						
9	6.31361E+05	1.76890E+06						
10	1.74295E+06	4.88326E+06						
11	0.	0.						

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 6

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	2.20935E+05	6.23893E+02	0.	0.	0.	0.	0.	0.
2	6.71988E+05	7.14853E+03	0.	0.	0.	0.	0.	0.
3	5.52118E+05	7.79385E+03	0.	0.	0.	0.	0.	0.
4	6.94156E+05	1.03202E+04	0.	0.	0.	0.	0.	0.
5	3.00879E+05	4.47212E+03	0.	0.	0.	0.	0.	0.
6	2.81452E+05	4.18338E+03	0.	0.	0.	0.	0.	0.
7	2.39382E+05	3.55798E+03	0.	0.	0.	0.	0.	0.
8	2.02571E+05	3.01101E+03	0.	0.	0.	0.	0.	0.
9	1.17922E+05	1.75277E+03	0.	0.	0.	0.	0.	0.
10	4.70934E+04	7.00121E+02	0.	0.	0.	0.	0.	0.
11	5.05895E+03	7.52109E+01	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 7

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	1.06338E+03	0.	0.	0.	0.	0.	0.
2	0.	3.48802E+02	0.	0.	0.	0.	0.	0.
3	0.	5.18926E+03	0.	0.	0.	0.	0.	0.
4	0.	1.11332E+04	0.	0.	0.	0.	0.	0.
5	0.	5.26457E+03	0.	0.	0.	0.	0.	0.
6	0.	5.67464E+03	0.	0.	0.	0.	0.	0.
7	0.	1.27514E+03	0.	0.	0.	0.	0.	0.
8	0.	7.09211E+03	0.	0.	0.	0.	0.	0.
9	0.	2.26932E+02	0.	0.	0.	0.	0.	0.
10	0.	3.79792E+02	0.	0.	0.	0.	0.	0.
11	1.42520E+04	4.39121E+03	0.	0.	0.	0.	0.	0.

	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	0.	0.	0.	0.	0.	0.	0.	0.
2	0.	0.	0.	0.	0.	0.	0.	0.
3	0.	0.	0.	0.	0.	0.	0.	0.
4	0.	0.	0.	0.	0.	0.	0.	0.
5	0.	0.	0.	0.	0.	0.	0.	0.
6	0.	0.	0.	0.	0.	0.	0.	0.
7	0.	0.	0.	0.	0.	0.	0.	0.
8	0.	0.	0.	0.	0.	0.	0.	0.
9	0.	0.	0.	0.	0.	0.	0.	0.
10	0.	0.	0.	0.	0.	0.	0.	0.
11	0.	0.	0.	0.	0.	0.	0.	0.

	GROUP 25	GROUP 26	GROUP
1	0.	0.	
2	0.	0.	
3	0.	0.	
4	0.	0.	
5	0.	0.	
6	0.	0.	
7	0.	0.	
8	0.	0.	
9	0.	0.	
10	0.	0.	
11	0.	0.	

TABLE III (continued)

## PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 8

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	0.	0.	0.	0.	0.	9.37874E+01	1.93561E+02	2.21888E+02
2	0.	0.	1.71839E-09	0.	0.	5.32567E+01	1.09912E+02	1.25998E+02
3	0.	0.	9.87717E+02	0.	0.	0.	0.	0.
4	0.	0.	1.03606E+04	1.36442E+03	0.	4.35306E+02	8.98396E+02	1.02987E+03
5	0.	0.	1.45601E+04	7.77100E+03	0.	1.63313E+02	3.37050E+02	3.86376E+02
6	0.	0.	1.69082E+02	0.	0.	2.81994E+01	5.81986E+01	6.67157E+01
7	0.	0.	0.	0.	0.	1.93922E+01	4.00221E+01	4.58792E+01
8	0.	0.	1.52622E+04	1.95021E+04	6.27877E+03	0.	0.	0.
9	0.	0.	7.69032E+03	7.44381E+03	4.87286E+03	2.57778E+01	5.32009E+01	6.09867E+01
10	0.	0.	3.11426E+01	1.28311E-06	0.	4.14384E+01	8.55217E+01	9.80374E+01
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	2.23797E+02	2.21119E+02	2.42586E+02	2.98104E+02	1.32015E+03	7.10347E+02	1.02204E+03	2.57990E+03
2	1.27082E+02	1.25561E+02	1.37751E+02	1.69277E+02	7.54183E+02	4.03367E+02	5.80359E+02	1.46498E+03
3	0.	0.	0.	0.	0.	0.	0.	0.
4	1.03874E+03	1.02630E+03	1.12594E+03	1.38363E+03	6.16450E+03	3.29702E+03	4.74371E+03	1.19744E+04
5	3.89701E+02	3.85037E+02	4.22419E+02	5.19093E+02	2.31273E+03	1.23694E+03	1.77969E+03	4.49242E+03
6	6.72899E+01	6.64846E+01	7.29392E+01	8.96320E+01	3.99340E+02	2.13583E+02	3.07300E+02	7.75708E+02
7	4.62741E+01	4.57203E+01	5.01590E+01	6.16384E+01	2.74619E+02	1.46877E+02	2.11325E+02	5.33441E+02
8	0.	0.	0.	0.	0.	0.	0.	0.
9	6.15116E+01	6.07754E+01	6.66758E+01	8.19351E+01	3.65047E+02	1.95242E+02	2.80912E+02	7.09097E+02
10	9.88812E+01	9.76978E+01	1.07183E+02	1.31713E+02	5.86822E+02	3.13856E+02	4.51572E+02	1.13989E+03
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	6.95854E+02	3.18827E+02	4.15311E+03	1.27955E+03	7.04133E+02	1.16405E+03	1.10672E+03	1.57163E+03
2	3.95137E+02	1.81044E+02	2.35832E+03	7.26587E+02	3.99838E+02	6.60999E+02	6.28447E+02	8.92443E+02
3	0.	0.	0.	0.	0.	0.	0.	0.
4	3.22975E+03	1.47981E+03	1.92763E+04	5.93893E+03	3.26817E+03	5.40284E+03	5.13677E+03	7.29460E+03
5	1.21170E+03	5.55177E+02	7.23186E+03	2.22810E+03	1.22612E+03	2.02698E+03	1.92715E+03	2.73670E+03
6	2.09225E+02	9.58627E+01	1.24873E+03	3.84727E+02	2.11714E+02	3.49999E+02	3.32763E+02	4.72548E+02
7	1.43880E+02	6.59231E+01	8.58729E+02	2.64570E+02	1.45592E+02	2.40688E+02	2.28835E+02	3.24963E+02
8	0.	0.	0.	0.	0.	0.	0.	0.
9	1.91258E+02	8.76308E+01	1.14150E+03	3.51690E+02	1.93534E+02	3.19944E+02	3.04188E+02	4.31969E+02
10	3.07452E+02	1.40868E+02	1.83498E+03	5.65350E+02	3.11110E+02	5.14317E+02	4.88988E+02	6.94400E+02
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	1.93692E+03	2.74529E+03						
2	1.09987E+03	1.55890E+03						
3	0.	0.						
4	8.99007E+03	1.27420E+04						
5	3.37279E+03	4.78041E+03						
6	5.82381E+02	8.25436E+02						
7	4.00494E+02	5.67638E+02						
8	0.	0.						
9	5.32371E+02	7.54554E+02						
10	8.55798E+02	1.21296E+03						
11	0.	0.						

## PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (OR MIXTURE) 9

	GROUP 1	GROUP 2	GROUP 3	GROUP 4	GROUP 5	GROUP 6	GROUP 7	GROUP 8
1	3.02437E+03	6.23893E+00	0.	0.	8.35174E+01	6.28725E+02	1.14120E+03	1.67712E+03
2	1.70523E+04	4.43434E+03	0.	0.	2.60129E+02	1.95827E+03	3.55447E+03	5.22367E+03
3	1.63258E+04	9.93186E+03	0.	0.	1.44668E+02	1.08907E+03	1.97678E+03	2.90509E+03
4	2.19653E+04	2.87388E+04	1.25377E+04	3.48632E+02	1.59843E+02	1.20330E+03	2.18413E+03	3.20981E+03
5	9.75407E+03	1.35094E+04	8.08374E+03	1.39198E+03	4.37119E+01	3.29066E+02	5.97290E+02	8.77781E+02
6	8.84559E+03	8.35735E+03	3.92596E+03	2.44633E+03	5.00812E+01	3.77015E+02	6.84322E+02	1.00568E+03
7	7.43308E+03	5.71770E+03	0.	0.	6.38980E+01	4.81028E+02	8.73110E+02	1.28314E+03
8	6.42976E+03	5.17704E+03	2.86119E+02	1.07464E+02	7.77474E+01	5.14253E+02	9.33425E+02	1.37177E+03
9	3.89595E+03	3.40283E+03	7.83186E+02	2.99078E+02	4.64665E+01	1.03167E+02	1.87260E+02	2.75198E+02
10	1.68796E+03	1.80488E+03	3.42248E+02	5.21400E+00	3.78326E+01	2.84806E+02	5.16954E+02	7.59719E+02
11	2.01764E+02	1.71043E+02	0.	0.	0.	0.	0.	0.
	GROUP 9	GROUP 10	GROUP 11	GROUP 12	GROUP 13	GROUP 14	GROUP 15	GROUP 16
1	2.16089E+03	2.46108E+03	2.57039E+03	3.78889E+03	6.26044E+03	8.76827E+03	1.14853E+04	1.43795E+04
2	6.73047E+03	7.66545E+03	8.00591E+03	1.18011E+04	1.94992E+04	2.73103E+04	3.57722E+04	4.47873E+04
3	3.74307E+03	4.26305E+03	4.45240E+03	6.56307E+03	1.08443E+04	1.51883E+04	1.98946E+04	2.49079E+04
4	4.13569E+03	4.71022E+03	4.91942E+03	7.25149E+03	1.19817E+04	1.67814E+04	2.19814E+04	2.75206E+04
5	1.13098E+03	1.28810E+03	1.34531E+03	1.98305E+03	3.27603E+03	4.58919E+03	6.01123E+03	7.52602E+03
6	1.29578E+03	1.47579E+03	1.54133E+03	2.27201E+03	3.75407E+03	5.25789E+03	6.88713E+03	8.62265E+03
7	1.65327E+03	1.88294E+03	1.96657E+03	2.89883E+03	4.78978E+03	6.70848E+03	8.78721E+03	1.10015E+04
8	1.76746E+03	2.01299E+03	2.10240E+03	3.09905E+03	5.12061E+03	7.17183E+03	9.39414E+03	1.17614E+04
9	3.54581E+02	4.03839E+02	4.21775E+02	6.21719E+02	1.02728E+03	1.43879E+03	1.88462E+03	2.35953E+03
10	9.78864E+02	1.11485E+03	1.16436E+03	1.71033E+03	2.83592E+03	3.97194E+03	5.20271E+03	6.51376E+03
11	0.	0.	0.	0.	0.	0.	0.	0.

TABLE III (continued)

	GROUP 17	GROUP 18	GROUP 19	GROUP 20	GROUP 21	GROUP 22	GROUP 23	GROUP 24
1	1.75506E+04	2.51324E+04	3.07659E+04	3.73396E+04	5.96108E+04	4.98860E+04	7.49449E+04	9.34241E+04
2	5.46644E+04	7.82792E+04	9.58256E+04	1.16300E+05	1.85668E+05	1.55378E+05	2.33429E+05	2.90985E+05
3	3.04010E+04	4.35341E+04	5.32924E+04	6.46792E+04	1.03257E+05	8.64119E+04	1.29819E+05	1.61828E+05
4	3.35898E+04	4.81005E+04	5.88823E+04	7.14635E+04	1.14088E+05	9.54759E+04	1.43436E+05	1.78803E+05
5	9.18576E+03	1.31540E+04	1.61025E+04	1.95430E+04	3.11995E+04	2.61096E+04	3.92251E+04	4.88969E+04
6	1.05242E+04	1.50707E+04	1.84488E+04	2.23907E+04	3.57456E+04	2.99141E+04	4.49407E+04	5.60217E+04
7	1.34277E+04	1.92285E+04	2.35386E+04	2.85680E+04	4.56074E+04	3.81671E+04	5.73393E+04	7.16775E+04
8	1.43552E+04	2.05566E+04	2.51644E+04	3.05412E+04	4.87575E+04	4.08033E+04	6.12997E+04	7.64144E+04
9	2.87988E+03	4.12398E+03	5.04838E+03	6.12705E+03	9.78154E+03	8.18579E+03	1.22977E+04	1.53300E+04
10	7.95027E+03	1.13847E+04	1.39367E+04	1.69145E+04	2.70031E+04	2.25979E+04	3.39493E+04	4.23202E+04
11	0.	0.	0.	0.	0.	0.	0.	0.
	GROUP 25	GROUP 26	GROUP					
1	7.69530E+04	2.15601E+05						
2	2.39683E+05	6.71526E+05						
3	1.33297E+05	3.73462E+05						
4	1.47279E+05	4.12635E+05						
5	4.02762E+04	1.12843E+05						
6	4.61449E+04	1.29285E+05						
7	5.88757E+04	1.64953E+05						
8	6.29422E+04	1.76347E+05						
9	1.26272E+04	3.53780E+04						
10	3.48590E+04	9.76652E+04						
11	0.	0.						

PHOTON ENERGY PRODUCTION SOURCE VECTORS AT INDICATED MESH INTERVALS

FOR MESH INTERVAL 1 BOUNDED BY RADII R= 0. AND R= 1.0000E+00 THE VECTOR IS									
2.12675162E+15	6.97604782E+14	1.03785212E+16	2.22663777E+16	1.05291495E+16	1.13492814E+16	2.55028620E+15	1.418042297E+16		
4.53863760E+14 7.59583350E+14 2.30344076E+16									
FOR MESH INTERVAL 2 BOUNDED BY RADII R= 1.0000E+00 AND R= 2.0000E+00 THE VECTOR IS									
2.12675162E+15	6.97604782E+14	1.03785212E+16	2.22663777E+16	1.05291495E+16	1.13492814E+16	2.55028620E+15	1.418042297E+16		
4.53863760E+14 7.59583350E+14 2.30344076E+16									
FOR MESH INTERVAL 3 BOUNDED BY RADII R= 2.0000E+00 AND R= 3.0000E+00 THE VECTOR IS									
2.12675162E+15	6.97604782E+14	1.03785212E+16	2.22663777E+16	1.05291495E+16	1.13492814E+16	2.55028620E+15	1.418042297E+16		
4.53863760E+14 7.59583350E+14 2.30344076E+16									
FOR MESH INTERVAL 4 BOUNDED BY RADII R= 3.0000E+00 AND R= 4.0000E+00 THE VECTOR IS									
4.43422585E+16	2.51795064E+16	2.96314993E+14	2.09464789E+17	8.46901758E+16	1.33832605E+16	9.16855284E+15	1.55188937E+16		
1.99086971E+16 1.96012534E+16 0.									
FOR MESH INTERVAL 5 BOUNDED BY RADII R= 4.0000E+00 AND R= 6.0000E+00 THE VECTOR IS									
4.43422585E+16	2.51795064E+16	2.96314993E+14	2.09464789E+17	8.46901758E+16	1.33832605E+16	9.16855284E+15	1.55188937E+16		
1.99086971E+16 1.96012534E+16 0.									
FOR MESH INTERVAL 6 BOUNDED BY RADII R= 6.0000E+00 AND R= 9.0000E+00 THE VECTOR IS									
4.43422585E+16	2.51795064E+16	2.96314993E+14	2.09464789E+17	8.46901758E+16	1.33832605E+16	9.16855284E+15	1.55188937E+16		
1.99086971E+16 1.96012534E+16 0.									
FOR MESH INTERVAL 7 BOUNDED BY RADII R= 9.0000E+00 AND R= 1.1000E+01 THE VECTOR IS									
4.43422585E+16	2.51795064E+16	2.96314993E+14	2.09464789E+17	8.46901758E+16	1.33832605E+16	9.16855284E+15	1.55188937E+16		
1.99086971E+16 1.96012534E+16 0.									
FOR MESH INTERVAL 8 BOUNDED BY RADII R= 1.1000E+01 AND R= 1.3000E+01 THE VECTOR IS									
1.66796902E+17	5.19681885E+17	2.89233013E+17	3.20355985E+17	8.79492646E+16	1.00472788E+17	1.27779453E+17	1.36584623E+17		
2.75088387E+16 7.56071349E+16 5.43850510E+12									
FOR MESH INTERVAL 9 BOUNDED BY RADII R= 1.3000E+01 AND R= 1.5000E+01 THE VECTOR IS									
1.66796902E+17	5.19681885E+17	2.89233013E+17	3.20355985E+17	8.79492646E+16	1.00472788E+17	1.27779453E+17	1.36584623E+17		
2.75088387E+16 7.56071349E+16 5.43850510E+12									

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REFERENCES

1. H. Honeck, "ENDF/B Specifications for an Evaluated Nuclear Data File for Reactor Applications," BNL 50066 (ENDF-102), Brookhaven National Laboratory (1966, revised 1967).
2. Donald J. Dudziak (Ed.), "ENDF/B Format Requirements for Shielding Applications," LA-3801 (ENDF-111), Los Alamos Scientific Laboratory (1967).
3. M. K. Drake, J. D. Garrison, and M. S. Allen, "Neutron and Gamma Ray Production Cross Sections for Sodium, Magnesium, Chlorine, Potassium, and Calcium," GA-7829 (NDL-TR-89), Vols. I to VI, General Atomics (1967).
4. Donald J. Dudziak, "Translation to ENDF/B and 'Physics' Checking of Cross Sections for Shielding," NE-3383-104-694 (ENDF-130), University of Virginia (1969).
5. Donald J. Dudziak and R. J. LaBauve, "Storage and Retrieval of Photon Production and Interaction Data in the ENDF/B System," Proceedings of Neutron Cross Sections and Technology Conference, NBS Special Publication 299, Vol. 2, 1101 (1968).
6. B. J. Toppel, A. L. Rago, and D. M. O'Shea, "MC<sup>2</sup>, A Code to Calculate Multigroup Cross Sections," ANL-7318, Argonne National Laboratory (1967).
7. K. D. Lathrop, "DTF-IV, A FORTRAN-IV Program for Solving the Multigroup Transport Equation with Anisotropic Scattering," LA-3373, Los Alamos Scientific Laboratory (1965).

APPENDIX A

COMMENTS CONCERNING CODE OPERATION AND SUBROUTINES

As shown in Fig. A.1, the LAPH code has been divided into three main parts, each of which is a primary overlay. The main overlay, OVERLAY (0,0), is very short and serves principally to define unlabelled COMMON and labelled COMMON/TAPES/ and to call the three primary overlays, namely, OVERLAY (1,0), (2,0), and (3,0). In OVERLAY (1,0), the input is read in DTF-IV format and binary Tape 5 is prepared for use as input to OVERLAY's (2,0) and (3,0); in OVERLAY (2,0), the photon production and energy production matrices for each material in each zone are calculated and written onto binary Tape 18; in OVERLAY (3,0), the matrices on Tape 18 are combined appropriately, and the photon source and energy source vectors are calculated.

A brief description of each of the subroutines follows.

OVERLAY (0,0)

PROGRAM MAIN serves to define unlabelled COMMON and labelled COMMON/TAPES/ and to call the three primary overlays.

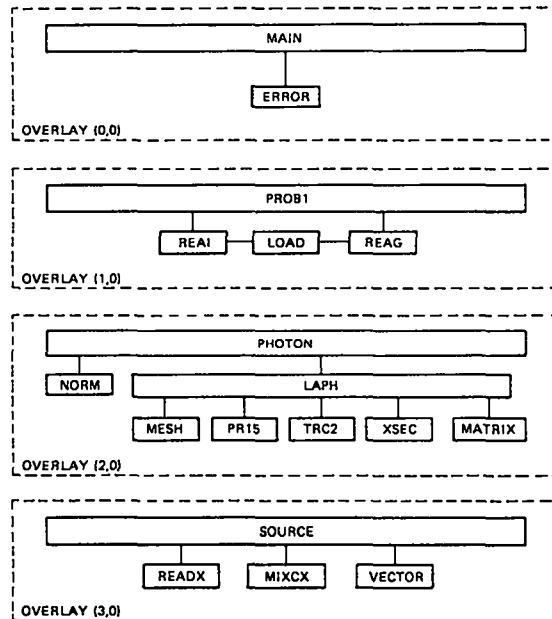


Fig. A.1. Arrangement of overlays and subroutines.

SUBROUTINE ERROR is called if there is an error in the input data or if any core storage allotments have been exceeded. An error stop number is printed, and execution is terminated. A complete catalog of the possible fatal error returns is included as a part of this subroutine. Other error messages are printed by the various subroutines when the error is nonfatal.

#### OVERLAY (1,0)

PROGRAM PROB1 reads all of the input data for the problem, does preliminary checking thereon, and arranges the data on binary Tape 5 in a form convenient for use in OVERLAY's (2,0) and (3,0).

SUBROUTINE REAI and SUBROUTINE REAG are DTF-IV routines. They are called by PROB1 to read integer and floating-point data, respectively, when these data are given in the DTF-IV format.

SUBROUTINE LOAD is another DTF-IV routine and is called by the two subroutines mentioned above. This routine interprets the DTF-IV control flags and fills out the integer and floating-point arrays accordingly.

#### OVERLAY (2,0)

PROGRAM PHOTON reads the input data from Tape 5 and supervises the calculations for each zone and each material within each zone.

SUBROUTINE INTG computes the integral of  $y(x)$  between two points  $x_1$  and  $x_2$ , where values of  $y(x)$  are given at  $x_3$  and  $x_4$  such that  $x_3 \leq x_1 < x_2 \leq x_4$ . The dependence of  $y(x)$  on  $x$  between the two tabulated points (e.g., linear-linear or log-log) must be specified.

FUNCTION LOCT locates the mesh interval in which a given variable lies.

SUBROUTINE TERP1 interpolates between two specified points of  $y(x)$  vs  $x$ , assuming a dependence (e.g., linear-linear or log-log) which must be specified.

SUBROUTINE LAPH supervises the calculation of the photon production and energy production matrices for each material.

SUBROUTINE NORM normalizes the fine-group weighting functions over each broad group.

SUBROUTINE RSF3 reads tabulated arrays from the ENDF/B data tape.

SUBROUTINE MESH forms the energy mesh to be used in the numerical integration over neutron

energy. The fine-group energy mesh is augmented with the energies at which the neutron cross sections are tabulated in File 3. Only those cross-section tables corresponding to reaction types specified in the input data are considered. This routine interprets the "MT = -1" command in the input specification and determines which MT numbers are to be used.

SUBROUTINE PR15 reads the photon production data from File 15 of the ENDF/B tape. For a continuous energy distribution under Option 1, the photon group yields,  $Y_g(E)$  and  $\tilde{Y}_g(E)$ , are calculated on either Track 1 or 2 and written onto Tape 15. For distributions under Option 1 at discrete gamma energies, the yields are written directly onto Tape 17. The appropriate transition and conditional probabilities under Option 2 are read from the ENDF/B tape and are written onto Tape 16 for later use in SUBROUTINE TRC2.

SUBROUTINE TRC2 reconstructs the microscopic photon production cross sections from the transition arrays (read from Tape 16) and the appropriate cross sections (read from the ENDF/B tape File 3), integrates over the neutron fine groups, and writes the results on Tape 16.

SUBROUTINE MATRIX reads the microscopic fine-group photon and energy production matrix elements ( $\tau$ 's and  $\rho$ 's) from Tape 16. It then performs the sum over fine groups which results in the photon production and energy production matrices for each reaction type. Finally, the sum over reaction types is taken to produce the  $G \times N$  matrices which are written onto Tape 18.

#### OVERLAY (3,0)

PROGRAM SOURCE supervises the calculation of the photon source and energy source vectors.

SUBROUTINE READX reads either the photon production or the energy production microscopic matrices from Tape 18.

SUBROUTINE MIXCX multiplies the microscopic matrices by the specified number densities and prints the macroscopic matrices.

SUBROUTINE VECTOR multiplies the macroscopic matrices by the appropriate flux vectors and the scalar renormalization constant to give the source vectors.

SUBROUTINE PUNCR punches both integer and floating-point arrays in DTF-IV format.







SYMBOL	REFERENCES
AWPSAV	200
C	200
EG	200
EMG	200
EMNB	200
EMNF	200
EXIT	13
GAMM	200
IFN	300 6=
IH	200
IJO	200
IRIS	200
ISI	300 5=
ISO	300 4=
IYO	200
IYM	200
MA	200
MAH	200
MC	200
MCR	200
MH	200
MS	200
MZ	200
NHG	200
NHNB	200
NHNF	200
NFG	200
NGAM	200
NGG	200
NHAT	200
NNM	200
NPM	200
OVERLAY	10 11 12
R	200
RV	200
RXSC	200
RXSF	200
SW	200
SXSC	200
SXSF	200
TAPES	300
XHD	200



1		SUBROUTINE ERROR (N)		ERROR
	C	PRINTS ERROR MESSAGE		ERROR
	C			ERROR
	C			ERROR
	C	CATALOGUE OF FATAL ERROR RETURNS		ERROR
	C			ERROR
	C	ERROR RETURN NUMBER	SUBROUTINE IN WHICH ERROR STOP OCCURRED AND SOURCE OF ERROR	ERROR
	C			ERROR
	C	100	PROB1 THE NEUTRON FINE AND BROAD GROUP ENERGY BOUNDARIES MUST BE GIVEN IN ORDER OF DECREASING MAGNITUDE.	ERROR
	C			ERROR
	C	101	PROB1 THE MT NUMBERS FOR A GIVEN MATERIAL MUST BE GIVEN IN ASCENDING ORDER.	ERROR
	C			ERROR
	C	200	INTG THE FLAG INDICATING DEPENDENCE OF Y(X) ON X MUST BE 1, 2, 3, 4, OR 5.	ERROR
	C			ERROR
	C	301	TEPP1 IT IS INCORRECT TO INTERPOLATE BETWEEN TWO POINTS WHICH ARE AT THE SAME ABSCISSA.	ERROR
	C			ERROR
	C	302	TERP1 INTERPOLATION CODE FLAG MUST BE POSITIVE.	ERROR
	C			ERROR
	C	303	TERP1 ARGUMENT OF LOG IS ZERO OR NEGATIVE.	ERROR
	C			ERROR
	C	400	MESH THE AUGMENTED FINE GROUP ENERGY MESH MUST NOT HAVE MORE THAN 2000 POINTS.	ERROR
	C			ERROR
	C	500	PR15 THERE MUST NOT BE MORE THAN 100 ENTRIES IN THE LOLF12 ARRAY.	ERROR
	C			ERROR
	C	501	PR15 AT THIS POINT IN THE CODE, THE NEUTRON ENERGY SHOULD NOT LIE OUTSIDE THE RANGE OF ENERGIES FOR WHICH THE PHOTON YIELD IS TABULATED FOR THIS LAW.	ERROR
	C			ERROR
	C	502	PR15 ERROR IN DETERMINING INTERPOLATION CODE.	ERROR
	C			ERROR
	C	503	PR15 THE LOLF11 ARRAY MUST NOT HAVE MORE THAN 500 ENTRIES.	ERROR
	C			ERROR
	C	600	TRC2 ERROR IN DETERMINING FROM WHICH LEVEL IN A CASCADE A TRANSITION OCCURS.	ERROR
	C			ERROR
	C	601	TRC2 LEVEL ENERGY SHOULD LIE WITHIN THIS ENERGY MESH.	ERROR
	C			ERROR
	C	602	TRC2 ENMAX MUST LIE WITHIN NEUTRON FINE GROUP ENERGY MESH.	ERROR
	C			ERROR

C				ERROR
C	603	TRC2	ERROR IN DETERMINING INTERPOLATION CODE.	ERROR
C				ERROR
C	700	XSEC	WHEN INTEGRATING OVER THE NEUTRON FINE GROUP, EVERY VALUE OF THE INTEGRAND MUST BE FOR ONE PARTICULAR GAMMA GROUP.	ERROR
C				ERROR
C	701	XSEC	AT THIS POINT IN THE CODE, THERE SHOULD BE AN INTERPOLATION CODE FOR THIS NEUTRON ENERGY.	ERROR
C				ERROR
C	702	XSEC	CROSS SECTIONS IN FILE 3 CANNOT BE FOUND CORRESPONDING TO THE MT NUMBER WRITTEN ON TAPE 15 OR TAPE 17.	ERROR
C				ERROR
C	800	SOURCE	THE TOTAL AMOUNT OF STORAGE REQUIRED FOR THE PHOTON PRODUCTION MATRICES, THE NEUTRON FLUXES, AND THE SOURCE VECTORS MUST NOT EXCEED 30000 CORE LOCATIONS.	ERROR
C				ERROR
C	900	READX	IFLAG MUST BE EITHER 1 OR 2.	ERROR
C				ERROR
2			COMMON /TAPES/ ISI,ISO,IEN	ERROR
3	5		WRITE (ISO,10) N	TAPES
4			CALL EXIT	ERROR
				ERROR
5	10		FORMAT (11H ERROR STOP,I6)	ERROR
6			END	ERROR

SYMBOL	= = = = =	REFERENCES	= = = = =
5	-	3*	
10	-	3WR	5*
ERROR	-	1	
EXIT	-	4	
IEN	-	2C0	
ISI	-	2C0	
ISO	-	2C0	3WR
N	-	1AG	3WR
TAPES	-	2C0	



I N D E X

OVERLAY(LAPH,1,0)

PAGE 9

1 OVERLAY(LAPH,1,0)

PROB1

I N D E X

PROGRAM PROB1

PAGE 10

1 PROGRAM PROB1

PROB1

C READS THE INPUT FOR THE PROBLEM IN DTF FORMAT AND PREPARES TAPE 5  
C IN BINARY FOR USE AS INPUT TO OVERLAY (LAPH,2,0) WHERE THE PHOTON  
C AND ENERGY PRODUCTION MATRICES ARE CALCULATED.

PROB1

PROB1

PROB1

PROB1

PROB1

2 COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I  
IWO,IZM,MA(100),MH(50),MC(50),MCR,MM,MS,MZ(10),NBG,NENB,NENF,NFG,NG  
2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW  
3(100),SXSC(100),SXS(100),XMD(50),AWRSAV

BLANK

BLANK

BLANK

BLANK

3 COMMON /TAPES/ ISI,ISO,IEN

TAPES

4 COMMON /TEST/ IPRILD,IPRILT

TEST

5 DIMENSION MZT(126), MTN(126), PHI(5000), TITLE(12)

PROB1

6 IPRILD=0

PROB1

7 IPRILT=0

PROB1

C THESE INDICATORS ARE TESTED IN SUBROUTINE LOAD AND CONTROL EXTRA  
C OUTPUT WHICH IS PRINTED IN DTF FORMAT.

PROB1

PROB1

C IF IPRILD IS NON-ZERO, THE OP, CNT, AND NUMERIC FIELDS ON EACH  
C CARD WILL BE PRINTED AS EACH CARD IS READ. IF IPRILD IS ZERO,  
C NO PRINTING WILL TAKE PLACE.

PROB1

PROB1

C IF IPRILT IS ZERO, THE FULL ARRAY WILL BE PRINTED OUT. IF IPRILT  
C IS NON-ZERO, ONLY THE ARRAY NAME AND COUNT WILL BE PRINTED.

PROB1

PROB1

8 READ (20,130) (TITLE(I),I=1,11),NTID

PROB1

9 WRITE (ISO,135) NTID,(TITLE(I),I=1,11)

PROB1

10 HEAD (ISI,125) ID,(TITLE(I),I=1,11)

PROB1

11 WRITE (ISO,140) ID,(TITLE(I),I=1,11)

PROB1

12 HEAD (ISI,145) NGG,NFG,NBG,IZM,IM,MS,MCR,MM,NPM,IRES,IWO,IOO

PROB1

13 WRITE (ISO,150) NGG,NFG,NBG,IZM,IM,MS,MCR,MM,NPM,IRES,IWO,IOO

PROB1

14 CALL REAG (C,1,6HRENORM,6H CONST)

PROB1

15 CALL REAI (NMAT,IZM,6HNO MAT,6HS/ZONE)

PROB1

16 WRITE (ISO,155) (I,NMAT(I),I=1,IZM)

PROB1

17 I=2\*MCR

PROB1

18 CALL REAI (NNM,I,6HNNM AR,6HRAY )

PROB1

19 WRITE (ISO,160) (NNM(II),II=1,I)

PROB1

20 CALL REAI (MZT,MCR,6HMZT AR,6HRAY )

PROB1

21 CALL REAI (MTN,MM,6HMTN NU,6HMBERS )

PROB1

22 WRITE (ISO,165)

PROB1

23 K=1

PROB1

24 KK=0

PROB1

25 DO 5 I=1,MCR

PROB1

26 KK=KK+MZT(I)

PROB1

27 WRITE (ISO,170) I,(MTN(J),J=K,KK)

PROB1

28 K=KK+1

PROB1

29 IF (IWO,NE.0) GO TO 10

PROB1

30 CALL REAG (EG,NGG,6HEGAMMA,6H BAR )

PROB1

31 10 NGAM=NGG+1

PROB1

32 NENF=NFG+1

PROB1

33 NENB=NBG+1

PROB1

34 CALL REAG (EMG,NGAM,6HGAMMA ,6HROUNDS)

PROB1

35 CALL REAG (EMNF,NENF,6HNEUTRO,6HNFINE)

PROB1

36		CALL REAG (EMNB,NENB,6HNEUTRO,6HN BRD)	PROB1
37		IF (IWO.NE.0) GO TO 20	PROB1
38		DO 15 I=1,NGG	PROB1
39		IF (EG(I).LE.EMG(I).AND.EG(I).GE.EMG(I+1)) GO TO 15	PROB1
40		EHOLD=EG(I)	PROB1
41		EG(I)=(EMG(I)+EMG(I+1))/2.0	PROB1
42		WRITE (ISO,175) I,EHOLD,EMG(I),EMG(I+1),EG(I)	PROB1
43	15	CONTINUE	PROB1
44	20	DO 25 I=1,NGG	PROB1
45	25	IF (EMG(I).LE.EMG(I+1)) GO TO 40	PROB1
46		DO 30 I=1,NFG	PROB1
47	30	IF (EMNF(I).LE.EMNF(I+1)) GO TO 40	PROB1
48		DO 35 I=1,NBG	PROB1
49	35	IF (EMNH(I).LE.EMNH(I+1)) GO TO 40	PROB1
50		GO TO 45	PROB1
51	40	CALL ERROR (100)	PROB1
52	45	DO 50 I=1,NGAM	PROB1
53		K=NGAM+1-I	PROB1
54	50	GAMM(K)=EMG(I)	PROB1
55		MATC=1	PROB1
56		IMIN=1	PROB1
57		IMAX=0	PROB1
58		IF (IRES.EQ.1) GO TO 60	PROB1
59		DO 55 I=1,NFG	PROB1
60	55	RW(I)=0.0	PROB1
61	60	DO 115 II=1,IZM	PROB1
62		KNO=NMAT(II)	PROB1
63		K=0	PROB1
64		DO 85 J=1,KNO	PROB1
65		IF (IRES.NE.1) GO TO 85	PROB1
66		READ (ISI,180) TITLE	PROB1
67		WRITE (ISO,185) TITLE	PROB1
68		CALL REAG (RXSC,NFG,6HRXSC ,6H )	PROB1
69		DO 65 I=1,NFG	PROB1
70		K=K+1	PROB1
71	65	PHI(K)=RXSC(I)	PROB1
72		READ (ISI,180) TITLE	PROB1
73		WRITE (ISO,185) TITLE	PROB1
74		CALL REAG (RXSF,NFG,6HRXSF ,6H )	PROB1
75		DO 70 I=1,NFG	PROB1
76		K=K+1	PROB1
77	70	PHI(K)=RXSF(I)	PROB1
78		READ (ISI,180) TITLE	PROB1
79		WRITE (ISO,185) TITLE	PROB1
80		CALL REAG (SXSC,NFG,6HSXSC ,6H )	PROB1
81		DO 75 I=1,NFG	PROB1
82		K=K+1	PROB1
83	75	PHI(K)=SXSC(I)	PROB1
84		READ (ISI,180) TITLE	PROB1
85		WRITE (ISO,185) TITLE	PROB1

86		CALL REAG (SXSF,NFG,6HSXSF ,6H )	PROB1
87		DO 80 I=1,NFG	PROB1
88		K=K+1	PROB1
89	80	PHI(K)=SXSF(I)	PROB1
90	85	CONTINUE	PROB1
91		IF (IRES.NE.1) GO TO 90	PROB1
92		READ (ISI,180) TITLE	PROB1
93		WRITE (ISO,185) TITLE	PROB1
94		CALL REAG (RW,NFG,6HRW ,6H )	PROB1
95	90	READ (ISI,180) TITLE	PROB1
96		WRITE (ISO,185) TITLE	PROB1
97		CALL REAG (SW,NFG,6HSW ,6H )	PROB1
98		IF (IRES.EQ.1) WRITE (5) (RW(I),I=1,NFG)	PROB1
99		WRITE (5) (SW(I),I=1,NFG)	PROB1
100		KMIN=1	PROB1
101		KMAX=NFG	PROB1
102		DO 110 J=1,KNO	PROB1
103		IMAX=IMAX+MZT(MATC)	PROB1
104		MATC2=MATC+MATC	PROB1
105		MAT=NNM(MATC2)	PROB1
106		WRITE (5) MAT,MZT(MATC),(MTN(I),I=IMIN,IMAX)	PROB1
107		IF (IMIN.EQ.IMAX) GO TO 105	PROB1
108		IMM1=IMAX-1	PROB1
109		DO 95 I=IMIN,IMM1	PROB1
110	95	IF (MTN(I+1).LE.MTN(I)) GO TO 100	PROB1
111		GO TO 105	PROB1
112	100	CALL ERROR (101)	PROB1
	C	HERE WE ARE TESTING THAT THE MT NUMBERS FOR A GIVEN MATERIAL ARE	PROB1
	C	IN ASCENDING ORDER.	PROB1
113	105	MATC=MATC+1	PROB1
114		IMIN=IMAX+1	PROB1
115		IF (IRES.NE.1) GO TO 110	PROB1
116		WRITE (5) (PHI(K),K=KMIN,KMAX)	PROB1
117		KMIN=KMAX+1	PROB1
118		KMAX=KMAX+NFG	PROB1
119		WRITE (5) (PHI(K),K=KMIN,KMAX)	PROB1
120		KMIN=KMAX+1	PROB1
121		KMAX=KMAX+NFG	PROB1
122		WRITE (5) (PHI(K),K=KMIN,KMAX)	PROB1
123		KMIN=KMAX+1	PROB1
124		KMAX=KMAX+NFG	PROB1
125		WRITE (5) (PHI(K),K=KMIN,KMAX)	PROB1
126		KMIN=KMAX+1	PROB1
127		KMAX=KMAX+NFG	PROB1
128	110	CONTINUE	PROB1
129	115	CONTINUE	PROB1
130		I=IM+1	PROB1
131		CALL REAG (R,I,6HRADII ,6H )	PROB1
132		CALL REAI (MA,IM,6HZONE N,6HUMBERS)	PROB1
133		CALL REAI (MZ,IZM,6HMIXTUR,6HE NOS )	PROB1



134	CALL REAI (MB,MS,6HMIX TA,6HBLE )	PROB1
135	CALL REAI (MC,MS,6HMIX CO,6HMMAND )	PROB1
136	CALL REAG (XMD,MS,6HMIX DE,6HNSITY )	PROB1
137	IF (100.EQ.10*(100/10)) RETURN	PROB1
	C FLUXES ARE NOT READ IN FOR 100=0, 10, OR 20.	PROB1
138	I=IM*NBG	PROB1
139	CALL REAG (PHI,I,6HNEUTRO,6HN FLUX)	PROB1
140	KMIN=1	PROB1
141	KMAX=IM	PROB1
142	DO 120 I=1,NBG	PROB1
143	WRITE (5) (PHI(K),K=KMIN,KMAX)	PROB1
144	KMIN=KMAX+1	PROB1
145	120 KMAX=KMAX+IM	PROB1
146	RETURN	PROB1
	C	PROB1
147	125 FORMAT (I6,11A6)	PROB1
148	130 FORMAT (11A6,I4)	PROB1
149	135 FORMAT (*1ENDF/8 TAPE I. D. =*,I5,6X,11A6)	PROB1
150	140 FORMAT (////,*, LAPH PROBLEM ID=*,I6,11A6)	PROB1
151	145 FORMAT (12I6)	PROB1
152	150 FORMAT (* INTEGER PARAMETERS	PROB1
	1 IM MS NCR MM NPM NFG NRG IZM	PROB1
	2/,24X,12(2X,I6)	PROB1
153	155 FORMAT (* NUMBER OF NUCLIDES IN EACH ZONE*,/,11X,*ZONE*.2X,*NUMBER	PROB1
	1 OF NUCLIDES *,/(10X,I5,5X,I5))	PROB1
154	160 FORMAT (* NUCLIDE SEQUENCE NUMBER NUCLIDE*,/(12X12*-----	PROB1
	1-----*,I5))	PROB1
155	165 FORMAT (* NUCLIDE SEQUENCE NUMBER MT NUMBERS*)	PROB1
156	170 FORMAT (15X,I5,15X,20I4)	PROB1
157	175 FORMAT (* ERROR IN THE EFFECTIVE AVERAGE ENERGY INPUT FOR GROUP*,I	PROB1
	15,/,* THE VALUE EG(I)=*,1PE14.6,* SHOULD LIE BETWEEN THE BOUNDARIE	PROB1
	2S EMG(I)=*,1PE14.6,* AND EMG(I+1)=*,1PE14.6*/,* THE MIDPOINT OF TH	PROB1
	3E ENERGY INTERVAL HAS BEEN USED. EG(I) HAS BEEN REPLACED BY*,1PE14	PROB1
	*.6)	PROB1
158	180 FORMAT (12A6)	PROB1
159	185 FORMAT (/,2X,12A6)	PROB1
160	END	PROB1

SYMBOL	REFERENCES
5	25 28*
10	24 31*
15	35 39 43*
20	37 44*
25	44 45*
30	46 47*
35	48 49*
40	45 47 49 51*
45	50 52*
50	52 54*
55	59 60*
60	58 61*
65	69 71*
70	75 77*
75	81 83*
80	87 89*
85	64 65 90*
90	91 95*
95	109 110*
100	110 112*
105	107 111 113*
110	102 115 128*
115	61 129*
120	142 145*
125	10RD 147*
130	8RD 148*
135	9WR 149*
140	11WR 150*
145	12RD 151*
150	13WR 152*
155	16WR 153*
160	19WR 154*
165	22WR 155*
170	27WR 156*
175	42WR 157*
180	66RD 72RD 78RD 84RD 92RD 95RD 158*
185	67WR 73WR 79WR 85WR 93WR 96WR 159*
A WRS AV	2CO
C	2CO 14AG
EG	2CO 30AG 39 40 41= 42WR
EHOLD	40= 42WR
ENG	2CO 34AG 39 41 42WR 45 54
EMNH	2CO 36AG 49
EMNF	2CO 35AG 47
ERROR	51 112
GAMM	2CO 54=
I	8RD 9WR 10RD 11WR 16WR 17= 18AG 19WR 25 26 27WR 38 39 40 41 42WR 44 45 46 47

	PROGRAM PROB1									
	48	49	52	53	54	59	60	69	71	75
	77	81	83	87	89	98WR	99WR	106WR	109	110
	130=	131AG	138=	139AG	142					
IN	-	10RD	11WR							
IFN	-	3CO								
IT	-	19WR	61	62						
IM	-	2CO	12RD	13WR	130	132AG	138	141	145	
IMAX	-	57=	103=	106WR	107	108	114			
IMIN	-	56=	106WR	107	109	114=				
IMM1	-	108=	109							
IND	-	2CO	12RD	13WR	137					
IPRILU	-	4CO	6=							
IPRILT	-	4CO	7=							
IRIS	-	2CO	12RD	13WP	58	65	91	98	115	
ISI	-	3CO	10RD	12RD	66RD	72RD	78RD	84RD	92RD	95RD
ISO	-	3CO	9WR	11WR	13WR	16WR	19WR	22WR	27WR	42WR
		73WR	79WR	85WR	93WR	96WR				67WR
IWD	-	2CO	12RD	13WR	29	37				
I7M	-	2CO	12RD	13WR	15AG	16WR	61	133AG		
J	-	27WR	64	102						
K	-	23=	27WR	28=	53=	54	63=	70=	71	76=
		82=	83	88=	89	116WR	119WR	122WR	125WR	143WR
KK	-	24=	26=	27WR	28					77
KMAX	-	101=	116WR	117	118=	119WR	120	121=	122WR	123
		125WR	126	127=	141=	143WR	144	145=		124=
KMIN	-	103=	116WR	117=	119WR	120=	122WR	123=	125WR	126=
		143WR	144=							140=
KND	-	62=	64	102						
MA	-	2CO	132AG							
MAT	-	105=	106WR							
MATC	-	55=	103	104	106WR	113=				
MATC2	-	104=	105							
MR	-	2CO	134AG							
MC	-	2CO	135AG							
MCR	-	2CO	12RD	13WR	17	20AG	25			
IM	-	2CO	12RD	13WR	21AG					
MS	-	2CO	12RD	13WR	134AG	135AG	136AG			
MTN	-	5DI	21AG	27WR	106WR	110				
M7	-	2CO	133AG							
M7T	-	5DI	20AG	26	103	106WR				
NHG	-	2CO	12RD	13WR	33	48	138	142		
NFNH	-	2CO	33=	36AG						
NFNF	-	2CO	32=	35AG						
NFG	-	2CO	12RD	13WR	32	46	59	68AG	69	74AG
		80AG	81	86AG	87	94AG	97AG	98WR	99WR	101
		121	124	127						118
NGAM	-	2CO	31=	34AG	52	53				
NGG	-	2CO	12RD	13WR	30AG	31	38	44		
NMAT	-	2CO	15AG	16WP	62					
NNM	-	2CO	18AG	19WR	105					

I N D E X

PROGRAM PROB1

NPM	-	2CO	12RD	13WP						
NTID	-	HRD	9WR							
PHI	-	50I	71=	77=	83=	89=	116WR	119WR	122WR	125WR 139AG
R	-	143WR								
RFAG	-	2CO	131AG							
	-	14	30	34	35	36	68	74	80	86 94
	-	97	131	136	139					
RFAI	-	15	18	20	21	132	133	134	135	
RETURN	-	137	146							
RW	-	2CO	60=	94AG	98WR					
RXSC	-	2CO	68AG	71						
RXSF	-	2CO	74AG	77						
SW	-	2CO	97AG	99WR						
SXSC	-	2CO	80AG	83						
SXSF	-	2CO	86AG	89						
TAPES	-	3CO								
TFT	-	4CO								
TITLE	-	50I	8RD	9WR	10RD	11WR	66RD	67WR	72RD	73WR 78RD
	-	79WR	84RD	85WP	92RD	93WR	95RD	96WR		
XMD	-	2CO	136AG							



I N D E X

SUBROUTINE REAI (IARRAY,NCOUNT,HOL1,HOL2)

PAGE 17

1	SUBROUTINE REAI (IARRAY,NCOUNT,HOL1,HOL2)	REAI
2	COMMON /TEST/ IPRILD,IPRILT	TEST
3	DIMENSION IARRAY(1)	REAI
4	CALL LOAD (IARRAY,IARRAY,0,NCOUNT,HOL1,HOL2,IPRILD,IPRILT)	REAI
5	RETURN	REAI
6	END	REAI

I N D E X

SUBROUTINE REAI (IARRAY,NCOUNT,HOL1,HOL2)

PAGE 18

SYMBOL	=====	REFERENCES	=====
HOL1	- 1AG		
HOL2	- 1AG		
IARRAY	- 1AG	3DI 4AG	
IPRILD	- 2CO		
IPRILT	- 2CO		
LOAD	- 4		
NCOUNT	- 1AG		
REAI	- 1		
RETURN	- 5		
TFST	- 2CO		

I N D E X

SUBROUTINE REAG (ARRAY,NCOUNT,HOL1,HOL2)

PAGE 19

1	SUBROUTINE REAG (ARRAY,NCOUNT,HOL1,HOL2)	REAG
2	COMMON /TEST/ IPRILD,IPRILT	TEST
3	DIMENSION ARRAY(j)	REAG
4	CALL LOAD (ARRAY,ARRAY,1,NCOUNT,HOL1,HOL2,IPRILD,IPRILT)	REAG
5	RETURN	REAG
6	END	REAG

I N D E X

SUBROUTINE REAG (ARRAY,NCOUNT,HOL1,HOL2)

PAGE 20

SYMBOL	=====	REFERENCES	=====
ARRAY	- 4AG		
ARRAY	- 1AG	3DI 4AG	
HOL1	- 1AG	4AG	
HOL2	- 1AG	4AG	
IPRILD	- 2CO	4AG	
IPRILT	- 2CO	4AG	
LOAD	- 4		
NCOUNT	- 1AG	4AG	
REAG	- 1		
RETURN	- 5		
TFST	- 2CO		

SUBROUTINE LOAD (VECP,IVECP,ITYPIN,ICDES,HOL1,HOL2,IPRCRD,IPRCV)

1		SUBROUTINE LOAD (VECP,IVECP,ITYPIN,ICDES,HOL1,HOL2,IPRCRD,IPRCV)	LOAD
	C		LOAD
	C	THIS ROUTINE INTERPRETS THE DTF-IV CONTROL FLAGS AND FILLS OUT THE	LOAD
	C	INTEGER AND FLOATING POINT ARRAYS ACCORDINGLY.	LOAD
	C		LOAD
2		COMMON /TAPES/ NINP,NOUT,IEN	LOAD
3		DIMENSION VECP(1), IVECP(1)	LOAD
4		DIMENSION IOP(6), ICOUNT(6), FL(6), IFX(6)	LOAD
	C	THE PURPOSE OF THIS CODE IS TO READ BOTH	LOAD
	C	THE STANDARD DTF FLOATING POINT FORMAT	LOAD
	C	AND THE STANDARD DTF FIXED POINT FORMAT.	LOAD
	C	CALLING SEQUENCE ENTRIES )	LOAD
	C	VECP IS THE FLOATING POINT VECTOR TO BE LOADED.	LOAD
	C	IVECP IS THE FIXED POINT VECTOR TO BE LOADED.	LOAD
	C	ICDES IS THE COUNT OF THE BLOCK.	LOAD
	C	ITYPIN IS THE TYPE OF BLOCK TO BE LOADED.	LOAD
	C	IF THIS INDICATOR IS ZERO, THE CODE	LOAD
	C	ASSUMES THE BLOCK TO BE LOADED	LOAD
	C	IS FIXED POINT.	LOAD
	C	IF THIS INDICATOR IS NON ZERO, THE CODE	LOAD
	C	ASSUMES THE BLOCK TO BE LOADED IS FLOATING	LOAD
	C	POINT.	LOAD
	C	HOL1 IS A SET OF HOLLERITH CHARACTERS	LOAD
	C	TO BE PRINTED AS A TITLE.	LOAD
	C	HOL2 IS A SECOND SET OF HOLLERITH CHARACTERS	LOAD
	C	TO BE PRINTED AS A TITLE IMMEDIATELY	LOAD
	C	FOLLOWING HOL1. A SET OF HOLLERITH CHARACTERS	LOAD
	C	CONSIST OF A WORD IN THE 1 A 6 FORMAT.	LOAD
	C	IPRCRD IS THE PRINT INDIVIDUAL CARDS	LOAD
	C	AS THEY ARE READ INDICATOR. IF THIS INDICATOR	LOAD
	C	IS NON ZERO, EACH INDIVIDUAL CARD WILL BE	LOAD
	C	PRINTED AS IT IS READ. IF THE INDICATOR IS ZERO,	LOAD
	C	NO PRINTING WILL TAKE PLACE FOR AN INDIVIDUAL CARD.	LOAD
	C	IPRCV IS THE CORRECT VECTOR PRINT INDICATOR.	LOAD
	C	IF THIS INDICATOR IS ZERO, THE FULL VECTOR	LOAD
	C	WILL BE PRINTED. IF THIS INDICATOR IS	LOAD
	C	NON ZERO, ONLY THE VECTOR NAME AND COUNT	LOAD
	C	WILL BE PRINTED.	LOAD
	C	COMMON PARAMTERS )	LOAD
	C	NINP IS THE SYSTEM INPUT UNIT NUMBER.	LOAD
	C	NOUT IS THE SYSTEM OUTPUT UNIT NUMBER.	LOAD
	C	THE STANDARD DTF CARD IS COMPOSED OF SIX	LOAD
	C	FIELDS OF LENGTH TWELVE. EACH FIELD IS	LOAD
	C	SUB DIVIDED INTO AN OPERATION FIELD, A	LOAD
	C	COUNT FIELD AND A NUMERIC FIELD.	LOAD
	C	THE OPERATION FIELD HAS A LENGTH OF ONE.	LOAD
	C	THE FOLLOWING NUMERIC VALUES ARE PERMITTED.	LOAD
	C	A VALUE OF ZERO OR BLANK INDICATE JUST THE NUMBER IS TO	LOAD
	C	BE LOADED. THE COUNT FIELD IS DISREGARDED.	LOAD
	C	A VALUE OF ONE INDICATES REPEAT THE NUMBER IN THE	LOAD

SUBROUTINE LOAD (VECP,IVECP,ITYP1N,ICDES,HOL1,HOL2,IPRCRD,IPRCV)

C NUMERIC FIELD. THE NUMBER IN THE NUMERIC FIELD WILL BE ENTERED INTO THE ARRAY A LOAD  
C TOTAL NUMBER OF TIMES AS INDICATED BY THE COUNT FIELD. THE COUNT FIELD MUST BE POSITIVE NON ZERO. LOAD  
C A VALUE OF TWO INDICATES THAT LINEAR INTERPOLATION IS DESIRED. THE INTERPOLATION IS DONE BETWEEN THIS VALUE AND THE SUCCESSIVE VALUE OF THE NEXT ENTRY. THIS SUCCESSIVE VALUE MAY ALSO HAVE AN OPERATION. THE NUMBER OF LINEAR INTERPOLATANTS IS GIVEN BY THE COUNT FIELD. THIS MUST BE GREATER THAN ZERO. INTERPOLATION IS LIMITED TO FLOATING POINT BLOCKS. LOAD  
C A VALUE OF THREE INDICATES THE END OF THE BLOCK. THE COUNT FIELD AND NUMERIC FIELD ARE DISREGARDED. AT THIS POINT THE NUMBER OF ENTRIES ARE CHECKED AGAINST THE DESIRED NUMBER. A VALUE OF FOUR INDICATES AN OPERATION WHICH REPEATS THE NUMERIC FIELD TO THE END OF THE BLOCK. THIS WILL BE DONE ONLY IF ENTRIES ARE STILL TO BE FILLED. THE COUNT FIELD IS DISREGARDED AND A TERMINAL OPERATION MUST FOLLOW THIS OPERATION. A VALUE OF 5 INDICATES THAT THE NUMBER IN THE NUMERIC FIELD IS TO BE REPEATED 10 \* THE NUMBER IN THE COUNT FIELD. A VALUE OF NINE INDICATES THAT THE REMAINING FIELDS OF THE CARD ARE TO BE DISREGARDED. THE COUNT HAS A FIELD LENGTH OF TWO AND IS DISREGARDED EXCEPT FOR THE REPEAT AND INTERPOLATION OPERATIONS. LOAD  
C THE NUMERIC FIELD HAS A LENGTH OF NINE AND MUST BE FLOATING POINT OR FIXED POINT AS THE DATA BEING READ INDICATES. LOAD  
C TEMPORARY STORAGE )  
C IEPRT IS THE ERROR INDICATOR. LOAD  
C ICNRD IS THE COUNT READ. LOAD  
C ICNET IS THE COUNT ENTERED. LOAD  
C ICNTS IS THE TEST COUNT. LOAD  
C ITYRD IS THE TYPE READ INDICATOR. LOAD  
C INORD IS THE NUMBER OF COMPLETE FIELDS ON A CARD. LOAD  
C IDX IS THE FIELD INDEX. LOAD  
C IDY IS A STORE INDEX. LOAD  
C INDIT IS THE INTERPOLATION INDICATOR. LOAD  
C IDZ IS A CURRENT INDEX. LOAD  
C DEL IS THE DELTA FOR INTERPOLATION. LOAD  
C ICNIT IS THE COUNT FIELD OF THE INTERPOLATION OPERATION. LOAD  
C IPEPRT IS THE LIST INPUT CARD INDICATOR. LOAD

	C	IF THIS INDICATOR IS MINUS NON ZERO, NO	LOAD
	C	CARD INPUT WILL BE LISTED. IF THIS INDICATOR	LOAD
	C	IS ZERO OR GREATER, THE INPUT CARDS WILL	LOAD
	C	BE LISTED AS THEY ARE READ.	LOAD
	C	ICRDNW IS THE CURRENT CARD NUMBER PROCESSED.	LOAD
	C	TEMPORARY STORAGE BLOCKS J	LOAD
	C	IOP IS THE OPERATION BLOCK.	LOAD
	C	ICOUNT IS THE COUNT BLOCK.	LOAD
	C	IFX IS THE FIXED POINT NUMERIC BLOCK.	LOAD
	C	FL IS THE FLOATING POINT NUMERIC BLOCK.	LOAD
	C	SET LIST INDICATOR.	LOAD
5		IPERRT=-1	LOAD
6		IF (IAPCRD.NE.0) IPERRT=0	LOAD
	C	INITIAL INDICATORS.	LOAD
7		IERRT=1	LOAD
8		ICNRD=0	LOAD
9		ICNET=0	LOAD
10		ICNTS=ICDES	LOAD
11		ITYRD=ITYPIN	LOAD
12		INORD=6	LOAD
13		INDIT=0	LOAD
14		ICRDNW=0	LOAD
15		IF (IPERRT.LT.0) GO TO 5	LOAD
16		WRITE (NOUT,265) HOL1,HOL2	LOAD
	C	READ A CARD.	LOAD
17	5	CONTINUE	LOAD
18		IF (ITYRD.EQ.0) GO TO 25	LOAD
	C	READ FLOATING POINT.	LOAD
19		READ (NINP,200) (IOP(I),ICOUNT(I),FL(I),I=1,INORD)	LOAD
20		ICRDNW=ICRDNW+1	LOAD
21		IF (IPERRT) 20,10,15	LOAD
	C	FIRST PASS TITLE.	LOAD
22	10	CONTINUE	LOAD
23		WRITE (NOUT,270)	LOAD
24	15	CONTINUE	LOAD
25		IPERRT=IPERRT+1	LOAD
26		WRITE (NOUT,275) IPERRT,(IOP(I),ICOUNT(I),FL(I),I=1,INORD)	LOAD
27	20	CONTINUE	LOAD
28		GO TO 45	LOAD
	C	READ FIXED POINT.	LOAD
29	25	CONTINUE	LOAD
30		READ (NINP,205) (IOP(I),ICOUNT(I),IFX(I),I=1,INORD)	LOAD
31		ICRDNW=ICRDNW+1	LOAD
32		IF (IPERRT) 40,30,35	LOAD
	C	FIRST PASS TITLE.	LOAD
33	30	CONTINUE	LOAD
34		WRITE (NOUT,280)	LOAD
35	35	CONTINUE	LOAD
36		IPERRT=IPERRT+1	LOAD
37		WRITE (NOUT,285) IPERRT,(IOP(I),ICOUNT(I),IFX(I),I=1,INORD)	LOAD



38	40	CONTINUE	LOAD
39	45	CONTINUE	LOAD
40		DO 125 IDX=1,INORU	LOAD
	C	CHECK FOR END OF CARD.	LOAD
41		IF (IOP(IDX),EQ.9) GO TO 5	LOAD
	C	RETURN ON PASS TWO OF INTERPOLATION.	LOAD
42	50	CONTINUE	LOAD
43		IDY=1	LOAD
44		IF (INDIT,EQ.0) GO TO 55	LOAD
	C	INTERPOLATION PASS TWO.	LOAD
45		INDIT=-1	LOAD
	C	CHECK FOR TERMINAL OPERATION.	LOAD
46		IF (IOP(IDX),EQ.3) GO TO 130	LOAD
47		UEL=(FL(IDX)-VECP(ICNET))/DEL	LOAD
48		IDY=ICNIT	LOAD
49		GO TO 95	LOAD
	C	CHECK FOR OPERATIONS.	LOAD
50	55	CONTINUE	LOAD
51		IF (IOP(IDX),GT.0) GO TO 65	LOAD
	C	CHECK ZERO COUNT.	LOAD
52		IF (ICOUNT(IDX),EQ.0) GO TO 60	LOAD
53		WRITE (NOUT,290)	LOAD
54		WRITE (NOUT,295)	LOAD
55		WRITE (NOUT,300) ICRDNW,IDX,HOL1,HOL2	LOAD
56		WRITE (NOUT,290)	LOAD
	C	PROCESS BLANK OPERATION.	LOAD
57	60	CONTINUE	LOAD
58		GO TO 95	LOAD
	C	OPERATION FIELD NOT BLANK.	LOAD
59	65	CONTINUE	LOAD
60		IF (IOP(IDX),GT.5) GO TO 170	LOAD
61		IDZ=IOP(IDX)	LOAD
62		GO TO (85,75,130,70,80), IDZ	LOAD
	C	REPEAT TO THE END OF THE BLOCK.	LOAD
63	70	CONTINUE	LOAD
64		IDY=ICNTS-ICNET	LOAD
65		IF (IDY) 125,125,95	LOAD
	C	INTERPOLATION PASS ONE.	LOAD
66	75	CONTINUE	LOAD
67		IF (ITYRD,EQ.0) GO TO 175	LOAD
68		IF (ICOUNT(IDX),LE.0) GO TO 180	LOAD
69		ICNIT=ICOUNT(IDX)	LOAD
70		IDZ=ICNIT+1	LOAD
71		DEL=FLOAT(IDZ)	LOAD
72		INDIT=1	LOAD
73		GO TO 95	LOAD
	C	NUMBER OF REPEATS TIMES TEN. (IOP = 5 )	LOAD
74	80	CONTINUE	LOAD
75		IDY=10	LOAD
76		IDY=IDY*ICOUNT(IDX)	LOAD

77		GO TO 90	LOAD
	C	REPEAT.	LOAD
78	85	CONTINUE	LOAD
79		IDY=ICOUNT(IDX)	LOAD
80	90	CONTINUE	LOAD
81		IF (IDY.LE.0) GO TO 190	LOAD
	C	ENTER ARRAY.	LOAD
82	95	CONTINUE	LOAD
83		DO 115 IDZ=1,IDY	LOAD
84		ICNRD=ICNRD+1	LOAD
85		IF (ICNRD.GT.ICNTS) GO TO 115	LOAD
86		ICNET=ICNET+1	LOAD
87		IF (ITYRD.EQ.0) GO TO 110	LOAD
	C	FLOATING POINT ENTRY.	LOAD
88		IF (INDIT) 100,105,105	LOAD
89	100	CONTINUE	LOAD
90		VECP(ICNET)=VECP(ICNET-1)+DEL	LOAD
91		GO TO 115	LOAD
92	105	CONTINUE	LOAD
93		VECP(ICNET)=FL(IDX)	LOAD
94		GO TO 115	LOAD
	C	FIXED POINT ENTRY.	LOAD
95	110	CONTINUE	LOAD
96		IVECP(ICNET)=IFX(IDX)	LOAD
	C	END OF IDZ LOOP.	LOAD
97	115	CONTINUE	LOAD
	C	CHECK FOR INTERPOLATION PASS TWO.	LOAD
98		IF (INDIT) 120,125,125	LOAD
99	120	CONTINUE	LOAD
100		INDIT=0	LOAD
101		GO TO 50	LOAD
	C	END OF IDX LOOP.	LOAD
102	125	CONTINUE	LOAD
103		GO TO 5	LOAD
	C	TERMINAL OPERATION.	LOAD
104	130	CONTINUE	LOAD
	C	CHECK FOR INTERPOLATION COMPLETED.	LOAD
105		IF (INDIT.NE.0) GO TO 185	LOAD
	C	CHECK COUNT.	LOAD
106		IF (ICNRD-ICNTS) 165,135,155	LOAD
	C	ENTERED BLOCK COUNT CORRECT.	LOAD
107	135	CONTINUE	LOAD
108		IERRT=0	LOAD
109		IDZ=ICNTS	LOAD
110		WRITE (NOUT,210) HOL1,HOL2,ICNTS	LOAD
	C	TEST FOR TITLE PRINT ONLY.	LOAD
111		IF (IPRCV.NE.0) GO TO 150	LOAD
	C	PRINT BLOCK.	LOAD
112	140	CONTINUE	LOAD
113		IF (IDZ.LE.0) GO TO 150	LOAD

## SUBROUTINE LOAD (VECP,IVECP,ITYPIN,ICDES,HOL1,HOL2,IPRCRD,IPRCV)

114		IF (ITYRD.EQ.0) GO TO 145	LOAD
115		WRITE (NOUT,215) (VECP(I),I=1,INDZ)	LOAD
116		GO TO 150	LOAD
117	140	CONTINUE	LOAD
118		WRITE (NOUT,220) (VECP(I),I=1,INDZ)	LOAD
	C	RETURN.	LOAD
119	150	CONTINUE	LOAD
120		IF (IERRT.NE.0) GO TO 195	LOAD
121		RETURN	LOAD
	C	TOO MANY ENTRIES IN THE BLOCK.	LOAD
122	150	CONTINUE	LOAD
123		WRITE (NOUT,225)	LOAD
124	160	CONTINUE	LOAD
125		WRITE (NOUT,230) ICNRD,ICNTS,HOL1,HOL2	LOAD
126		INDZ=ICNET	LOAD
127		GO TO 140	LOAD
	C	TOO FEW ENTRIES IN THE BLOCK.	LOAD
128	160	CONTINUE	LOAD
129		WRITE (NOUT,235)	LOAD
130		GO TO 160	LOAD
	C	ILLEGAL OPERATION.	LOAD
131	170	CONTINUE	LOAD
132		WRITE (NOUT,240)	LOAD
133		GO TO 160	LOAD
	C	INTERPOLATION ON A FIXED POINT BLOCK.	LOAD
134	170	CONTINUE	LOAD
135		WRITE (NOUT,245)	LOAD
136		GO TO 160	LOAD
	C	ZERO OR LESS ON COUNT FOR INTERPOLATION.	LOAD
137	180	CONTINUE	LOAD
138		WRITE (NOUT,250)	LOAD
139		GO TO 160	LOAD
	C	INTERPOLATION OPERATION NOT COMPLETED.	LOAD
140	180	CONTINUE	LOAD
141		WRITE (NOUT,255)	LOAD
142		GO TO 160	LOAD
	C	ZERO OR LESS COUNT ON REPEATS.	LOAD
143	190	CONTINUE	LOAD
144		WRITE (NOUT,260)	LOAD
145		GO TO 160	LOAD
	C	OBTAIN NEXT CASE DUE TO AN ERROR.	LOAD
146	190	CONTINUE	LOAD
147		WRITE (NOUT,305)	LOAD
148		CALL EXIT	LOAD
	C		LOAD
149	200	FORMAT (6(I1,I2,E9.4))	LOAD
150	205	FORMAT (6(I1,I2,I9))	LOAD
151	210	FORMAT (1H02A6,I6)	LOAD
152	215	FORMAT (1H 1P10E12.4)	LOAD
153	220	FORMAT (1H 10I12)	LOAD

SUBROUTINE LOAD (VECP,IVECP,ITYPIN,ICDES,HOL1,HOL2,IPIRCRD,IPIRCV)

154	225	FORMAT (73H0 COUNT READ DESIRED BLOCK NAME - ERROR TOO MAN	LOAD
		1Y ENTRIES LOADED. )	LOAD
155	230	FORMAT (1H 2112,2X,2A6)	LOAD
156	235	FORMAT (72H0 COUNT READ DESIRED BLOCK NAME - ERROR TOO FEW	LOAD
		1 ENTRIES LOADED. )	LOAD
157	240	FORMAT (73H0 COUNT READ DESIRED BLOCK NAME - ERROR ILLEGAL	LOAD
		1 OPERATION FOUND. )	LOAD
158	245	FORMAT (98H0 COUNT READ DESIRED BLOCK NAME - ERROR INTERPO	LOAD
		1LATION OPERATION REQUEST IN A FIXED BLOCK. )	LOAD
159	250	FORMAT (96H0 COUNT READ DESIRED BLOCK NAME - ERROR ZERO OR	LOAD
		1 LESS COUNT FOR INTERPOLATION OPERATION. )	LOAD
160	255	FORMAT (94H0 COUNT READ DESIRED BLOCK NAME - ERROR THE INT	LOAD
		1ERPOLATION OPERATION IS NOT COMPLETED. )	LOAD
161	260	FORMAT (89H0 COUNT READ DESIRED BLOCK NAME - ERROR ZERO OR	LOAD
		1 LESS COUNT FOR REPEAT OPERATION. )	LOAD
162	265	FORMAT (35H0 LOADING CARD READ OF BLOCK NAMED 2A6)	LOAD
163	270	FORMAT (119H0 CARD OP CNT NUMERIC OP CNT NUMERIC OP CNT NUME	LOAD
		1RIC OP CNT NUMERIC OP CNT NUMERIC OP CNT NUMERIC FLOATING. )	LOAD
164	275	FORMAT (1H I5,6(1X,I2,1X,I3,1X,1P1E9,2))	LOAD
165	280	FORMAT (116H0 CARD OP CNT NUMERIC OP CNT NUMERIC OP CNT NUME	LOAD
		1RIC OP CNT NUMERIC OP CNT NUMERIC OP CNT NUMERIC FIXED. )	LOAD
166	285	FORMAT (1H I5,6(1X,I2,1X,I3,1X,I9))	LOAD
167	290	FORMAT (77H0***** )	LOAD
		1***** )	LOAD
168	295	FORMAT (77H CAPD FIELD NAMED BLOCK**BLANK OPERATION AND NON ZE	LOAD
		1RO COUNT ENCOUNTERED. )	LOAD
169	300	FORMAT (1H ,I6,I6,2X,2A6)	LOAD
170	305	FORMAT (* ERROR - - EXIT CALLED FROM SUBROUTINE LOAD DUE TO I	LOAD
		INPUT ERROR*)	LOAD
171		END	LOAD

SYMBOL	=====	REFERENCES	=====
5	- 15	17*	41 103
10	- 21	22*	
15	- 21	24*	
20	- 21	27*	
25	- 18	29*	
30	- 32	33*	
35	- 32	35*	
40	- 32	38*	
45	- 28	39*	
50	- 42*	101	
55	- 44	50*	
60	- 52	57*	
65	- 51	59*	
70	- 62	63*	
75	- 62	66*	
80	- 62	74*	
85	- 62	78*	
90	- 77	80*	
95	- 49	58	65 73 82*
100	- 88	89*	
105	- 88	92*	
110	- 87	95*	
115	- 83	85	91 94 97*
120	- 98	99*	
125	- 40	65	98 102*
130	- 46	62	104*
135	- 106	107*	
140	- 112*	127	
145	- 114	117*	
150	- 111	113	116 119*
155	- 106	122*	
160	- 124*	130	133 136 139 142 145
165	- 106	128*	
170	- 60	131*	
175	- 67	134*	
180	- 68	137*	
185	- 105	140*	
190	- 81	143*	
195	- 126	146*	
200	- 149D	149*	
205	- 30KD	150*	
210	- 110WR	151*	
215	- 115WR	152*	
220	- 118WR	153*	
225	- 123WR	154*	
230	- 125WR	155*	
235	- 129WR	156*	
240	- 132WR	157*	

245	-	135WR	158*																		
250	-	138WR	159*																		
255	-	141WR	160*																		
260	-	144WR	161*																		
265	-	16WR	162*																		
270	-	23WR	163*																		
275	-	26WR	164*																		
280	-	34WR	165*																		
285	-	37WR	166*																		
290	-	53WR	56WR	167*																	
295	-	54WR	168*																		
300	-	55WR	169*																		
305	-	147WR	170*																		
DFL	-	47=	71=	90																	
EXIT	-	148																			
FL	-	40I	19RD	26WR	47	93															
FLOAT	-	71																			
HOL1	-	1AG	16WR	55WR	110WR	125WR															
HOL2	-	1AG	16WR	55WR	110WR	125WR															
I	-	19RD	26WR	30RD	37WR	115WR	118WR														
ICDES	-	1AG	10																		
ICNET	-	9=	47	64	86=	90	93	96	126												
ICNIT	-	48	69=	70																	
ICNRD	-	8=	84=	85	106	125WR															
ICNTS	-	10=	64	85	106	109	110WR	125WR													
ICOUNT	-	40I	19RD	26WR	30RD	37WR	52	68	69	76	79										
ICRDNW	-	14=	20=	31=	55WR																
INDY	-	40	41	46	47	51	52	55WR	60	61	68										
INDY	-	69	76	79	93	96															
INDY	-	43=	48=	64=	65	75=	76=	79=	81	83											
INDZ	-	61=	62	70=	71	83	109=	113	115WR	118WR	126=										
INFN	-	2C0																			
IPRRT	-	7=	108=	120																	
IX	-	40I	30RD	37WR	96																
INDIT	-	13=	44	45=	72=	88	98	100=	105												
INORD	-	12=	19RD	26WR	30RD	37WR	40														
INP	-	40I	19RD	26WR	30RD	37WR	41	46	51	60	61										
IPERRI	-	5=	6=	15	21	25=	26WR	32	36=	37WR											
IPRCRU	-	1AG	6																		
IPRCV	-	1AG	111																		
ITYPIN	-	1AG	11																		
ITYRD	-	11=	18	67	87	114															
IVECP	-	1AG	3DI	96=																	
LOAD	-	1																			
NINP	-	2C0	19RD	30RD																	
NOUIT	-	2C0	16WR	23WR	26WR	34WR	37WR	53WR	54WR	55WR	56WR										
		110WR	115WR	118WR	123WR	125WR	129WR	132WR	135WR	138WR	141WR										
		144WR	147WR																		
RETURN	-	121																			
TAPES	-	2C0																			

VECP	-	1AG	3DI	47	90=	93=	115WR	118WR														
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I N D E X

OVERLAY (LAPH,2,0)

PAGE 31

1 OVFRLAY(LAPH,2,0)

PHOTON

I N D E X

PROGRAM PHOTON

PAGE 32

1 PROGRAM PHOTON

PHOTON

C

PHOTON

C

PHOTON READS THE INPUT DATA FROM TAPES AND SUPERVISES THE  
CALCULATIONS FOR EACH ZONE AND EACH MATERIAL WITHIN EACH ZONE.

PHOTON

C

PHOTON

2

COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I  
1WO,IZM,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NRG,NENH,NENF,NFG,NG  
2AN,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW  
3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV

HLANK

HLANK

HLANK

HLANK

3

COMMON /TAPES/ ISI,ISO,IEN

TAPES

4

COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M

OVER1

ITSL

OVER1

5

REWIND 5

PHOTON

6

DO 20 IZON=1,IZM

PHOTON

C

SET UP THE PARAMETERS FOR THIS ZONE

PHOTON

7

IF (IRES.EQ.1) READ (5) (RW(I),I=1,NFG)

PHOTON

8

READ (5) (SW(I),I=1,NFG)

PHOTON

9

CALL NORM

PHOTON

10

KNO=NMAT(IZON)

PHOTON

11

DO 20 I=1,KNO

PHOTON

C

SET UP THE PARAMETERS FOR THE I-TH MATERIAL IN THIS ZONE.

PHOTON

12

READ (5) MATX,MTSL,(MTNO(J),J=1,M[ISL)

PHOTON

13

REWIND IEN

PHOTON

14

REWIND 20

PHOTON

15

S

READ (20,25) MAT

PHOTON

16

IF (MAT.NE.MATX) GO TO 5

PHOTON

17

BACKSPACE 20

PHOTON

C

RXSC IS USED AS TEMPORARY STORAGE HERE.

PHOTON

18

10

READ (20,30) (RXSC(J),J=1,11),MAT,MF,MT

PHOTON

19

WRITE (IEN,30) (RXSC(J),J=1,11),MAT,MF,MT

PHOTON

20

IF (MAT.NE.0) GO TO 10

PHOTON

21

REWIND IEN

PHOTON

22

IF (IRES.NE.1) GO TO 15

PHOTON

23

READ (5) (RXSC(J),J=1,NFG)

PHOTON

24

READ (5) (RXSF(J),J=1,NFG)

PHOTON

25

READ (5) (SXSC(J),J=1,NFG)

PHOTON

26

READ (5) (SXSF(J),J=1,NFG)

PHOTON

27

15

WRITE (ISO,35) IZON,I

PHOTON

C

THIS WRITE STATEMENT IS INCLUDED SO THAT ANY ERROR STOPS CAN BE

PHOTON

C

MORE EASILY TRACED DOWN.

PHOTON

23

CALL LAPH

PHOTON

29

20

CONTINUE

PHOTON

30

RETURN

PHOTON

C

PHOTON

31

25

FORMAT (66X,I4)

PHOTON

32

30

FORMAT (11A6,I4,I2,I3)

PHOTON

33

35

FORMAT (\* -----ZONE\*,I4,\* -----MATERIAL\*,I4,\* -----\*)

PHOTON

34

END

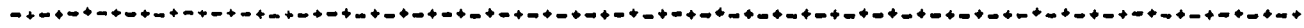
PHOTON

SYMBOL	=====	REFERENCES	=====
S	- 15*	16	
17	- 18*	20	
15	- 22	27*	
20	- 6	11	29*
25	- 15RD	31*	
30	- 18RD	19WR	32*
35	- 27WR	33*	
AWRSAV	- 200		
C	- 200		
EALUG	- 400		
EG	- 200		
EMG	- 200		
EMNB	- 200		
EMNF	- 200		
GAMM	- 200		
I	- 7RD	11	27WR
IALUG	- 400		
IFN	- 300	13	19WR 21
IL01	- 400		
IL02	- 400		
IM	- 200		
I00	- 200		
IPES	- 200	7	22
ISI	- 300		
ISO	- 300	27WR	
I40	- 200		
IYDA	- 400		
IXSD	- 400		
I7M	- 200	6	
IZON	- 6	19	27WR
J	- 12RD	18RD	19WR 23RD 24RD 25RD 26RD
KNO	- 10*	11	
LAPH	- 28		
MA	- 200		
MAT	- 15RD	16	18RD 19WR 20
MATX	- 400	12RD	16
M4	- 200		
MC	- 200		
MCR	- 200		
MF	- 18RD	19WR	
M4	- 200		
M5	- 200		
M1	- 18RD	19WR	
MTNO	- 400	12RD	
MTSL	- 400	12RD	
M7	- 200		
NRG	- 200		
NENB	- 200		



PROGRAM PHOTON

NFNF	-	200						
NFG	-	200	7RD	8RD	23RD	24RD	25RD	26RD
NGAM	-	200						
NGG	-	200						
NHAT	-	200	10					
NHM	-	200						
NORM	-	9						
NPM	-	200						
OVFL	-	400						
R	-	200						
RETURN	-	30						
Rw	-	200	7RD					
RXSC	-	200	18RD	19WR	23RD			
RXSF	-	200	24RD					
Sw	-	200	8RD					
SXSC	-	200	25RD					
SXSF	-	200	26RD					
TAPES	-	300						
X40	-	200						



## SUBROUTINE INTG (X3,Y3,X4,Y4,X1,X2,I,ANS)

```

1      SUBROUTINE INTG (X3,Y3,X4,Y4,X1,X2,I,ANS)          INTG
      C      COMPUTE INTEGRAL OF Y(X) BETWEEN X1 AND X2 WITH INTERPOLATION CODE INTG
2      5      ANS=0.0                                       INTG
3      IF (X4-X3) 85,85,10                                  INTG
4      10     IP=I                                          INTG
5      IF (IP) 15,15,20                                     INTG
6      15     CALL ERROR (200)                              INTG
7      20     IF (IP-5) 25,25,15                           INTG
8      25     GO TO (30,35,40,55,70), IP                   INTG
      C      Y=CONSTANT                                     INTG
9      30     ANS=(X2-X1)*Y3                                INTG
10     GO TO 85                                             INTG
      C      Y LINEAR IN X                                  INTG
11     35     B=(Y4-Y3)/(X4-X3)                             INTG
12     A=Y3-B*X3                                           INTG
13     ANS=(X2-X1)*(A+0.5*B*(X2+X1))                       INTG
14     GO TO 85                                             INTG
      C      Y LINEAR IN LN(X)                             INTG
15     40     IF ((X3.LE.0.0).OR.(X4.LE.0.0)) GO TO 35    INTG
16     B=(Y4-Y3)/ALOG(X4/X3)                               INTG
17     Z=(X2-X1)/X1                                        INTG
18     IF (ABS(Z)-0.15) 45,45,50                           INTG
19     45     ANS=(X2-X1)*(Y3+B*ALOG(X1/X3))+(0.5*B*X1*Z*Z)*(1.0+Z*(-0.33333333+
20     1Z*(0.16666667-0.1*Z)))                              INTG
21     GO TO 85                                             INTG
21     50     ANS=(X2-X1)*(Y3+B*ALOG(X1/X3))+R*X1*(1.0+(X2/X1)*(ALOG(X2/X1)-1.0)
22     1)                                                    INTG
22     GO TO 85                                             INTG
      C      LN(Y) LINEAR IN X                              INTG
23     55     IF ((Y3.LE.0.0).OR.(Y4.LE.0.0)) GO TO 35    INTG
24     B=ALOG(Y4/Y3)/(X4-X3)                               INTG
25     A=ALOG(Y3)-B*X3                                     INTG
26     Z=(X2-X1)*B                                         INTG
27     IF (ABS(Z)-.1) 60,60,65                              INTG
28     60     ANS=EXP(A+B*X1)*(X2-X1)*(1.0+Z*(.5+.16666667*Z)) INTG
29     GO TO 85                                             INTG
30     65     ANS=EXP(A+B*X1)*(EXP(Z)-1.0)/Z               INTG
31     GO TO 85                                             INTG
      C      LN(Y) LINEAR IN LN(X)                         INTG
32     70     IF ((X3.LE.0.0).OR.(X4.LE.0.0)) GO TO 55    INTG
33     IF ((Y3.LE.0.0).OR.(Y4.LE.0.0)) GO TO 40          INTG
34     B=ALOG(Y4/Y3)/ALOG(X4/X3)                          INTG
35     Z=(B+1.0)*ALOG(X2/X1)                               INTG
36     IF (ABS(Z)-0.1) 75,75,80                           INTG
37     75     ANS=Y3*X1*((X1/X3)**B)*ALOG(X2/X1)*(1.0+Z*(.5+.16666667*Z)) INTG
38     GO TO 85                                             INTG
39     80     ANS=Y3*X1*((X1/X3)**B)*((X2/X1)**(B+1.0))-1.0)/(B+1.0) INTG
40     85     CONTINUE                                       INTG
41     RETURN                                              INTG
42     END                                                  INTG

```

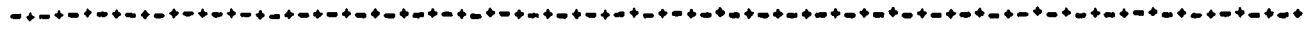
SUBROUTINE INTG (X3,Y3,X4,Y4,X1,X2,I,ANS)

SYMBOL	REFERENCES
5	2*
10	3 4*
15	5 6* 7
20	5 7*
25	7 8*
30	8 9*
35	8 11* 15 23
40	8 15* 33
45	18 19*
50	18 21*
55	8 23* 32
60	27 28*
65	27 30*
70	8 32*
75	36 37*
80	30 39*
85	3 10 14 20 22 29 31 38 40*
A	12= 13 25= 28 30
ARS	18 27 36
ALOG	16 19 21 24 25 34 35 37
ANS	1AG 2= 9= 13= 19= 21= 28= 30= 37= 39=
H	11= 12 13 16= 19 21 24= 25 26 28
	30 34= 35 37 39
ERROR	6
EXP	28 30
I	1AG 4
INTG	1
IP	4= 5 7 8
RETURN	41
X1	1AG 9 13 17 19 21 26 28 30 35
	37 39
X2	1AG 9 13 17 19 21 26 28 35 37
	39
X3	1AG 3 11 12 15 16 19 21 24 25
	32 34 37 39
X4	1AG 3 11 15 16 24 32 34
Y3	1AG 9 11 12 16 19 21 23 24 25
	33 34 37 39
Y4	1AG 11 16 23 24 33 34
Z	17= 18 19 26= 27 28 30 35= 36 37



1		FUNCTION LOCT (E,EK,N)	LOCT
	C	BRACKETS EK IN E SO THAT EK.GE.E(LOCT) AND EK.LT.E(LOCT+1)	LOCT
	C	IF EK CANNOT BE BRACKETED, LOCT=-1	LOCT
2		DIMENSION E(1)	LOCT
3		M=N-1	LOCT
4		DO 5 I=1,M	LOCT
5	5	IF ((EK.GE.E(I)).AND.(EK.LT.E(I+1))) GO TO 15	LOCT
6		IF (E(N).NE.EK) GO TO 10	LOCT
7		LOCT=M	LOCT
8		RETURN	LOCT
9	10	LOCT=-1	LOCT
10		RETURN	LOCT
11	15	LOCT=I	LOCT
12		RETURN	LOCT
13		END	LOCT

SYMBOL	=====	REFERENCES	=====
5	- 4	5*	
10	- 6	9*	
15	- 5	11*	
E	- 1AG	2DI	5 6
EK	- 1AG	5	6
I	- 4	5	11
LOCT	- 1	7=	9= 11=
M	- 3=	4	7
N	- 1AG	3	6
RETURN	- 8	10	12



## SUBROUTINE TERP1 (X1,Y1,X2,Y2,X,Y,I)

```

1      SUBROUTINE TERP1 (X1,Y1,X2,Y2,X,Y,I)
C      =====INTERPOLATE ONE PT.
C      (X1,Y1) AND (X2,Y2) ARE END PTS. OF THE LINE
C      (X,Y) IS INTERPOLATED POINT
C      I=INTERPOLATION CODE
C      NOTE - IF A NEGATIVE OR ZERO ARGUMENT OF A LOG IS DETECTED, THE
C              INTERPOLATION IS AUTOMATICALLY CHANGED FROM LOG TO LINEAR.
C      ERROR STOPS - 301 (X1=X2,DISCONTINUITY)
C                   302 (INTERPOLATION CODE IS OUT OF RANGE)
C                   303 (ZERO OR NEGATIVE ARGUMENT FOR INTERPOLATED PT.)
2      5      XA=X1
3      YA=Y1
4      XB=X2
5      YB=Y2
6      XP=X
7      II=I
8      IF (XA,EQ,XB) CALL ERROR (301)
9      IF (II) 10,10,15
10     10     CALL ERROR (302)
11     15     IF (II-5) 20,20,10
12     20     GO TO (25,30,35,60,75), II
13     25     YP=YA
14     GO TO 105
15     30     YP=YA+(XP-XA)*(YB-YA)/(XB-XA)
16     GO TO 105
17     35     IF (XA) 30,30,40
18     40     IF (XB) 30,30,45
19     45     IF (XP) 50,50,55
20     50     CALL ERROR (303)
21     55     YP=YA+ALOG(XP/XA)*(YB-YA)/ALOG(XB/XA)
22     GO TO 105
23     60     IF (YA) 30,30,65
24     65     IF (YB) 30,30,70
25     70     YP=YA*EXP((XP-XA)*ALOG(YB/YA)/(XB-XA))
26     GO TO 105
27     75     IF (YA) 35,35,80
28     80     IF (YB) 35,35,85
29     85     IF (XA) 70,70,90
30     90     IF (XB) 70,70,95
31     95     IF (XP) 50,50,100
32     100    YP=YA*EXP(ALOG(XP/XA)*ALOG(YB/YA)/ALOG(XB/XA))
33     105    Y=YP
34     RETURN
35     END

```

SUBROUTINE TERP1 (X1,Y1,X2,Y2,X,Y,I)

SYMBOL	REFERENCES		
5	2*		
1n	9	10*	11
1s	9	11*	
2n	11	12*	
2s	12	13*	
3n	12	15*	17 18 23 24
3s	12	17*	27 28
4n	17	18*	
4s	18	19*	
5n	19	20*	31
5s	19	21*	
6n	12	23*	
6s	23	24*	
7n	24	25*	29 30
7s	12	27*	
8n	27	28*	
8s	28	29*	
9n	29	30*	
9s	30	31*	
1n0	31	32*	
1n5	14	16	22 26 33*
ALOG	21	25	32
ERROR	8	10	20
EXP	25	32	
I	1AG	7	
I1	7=	9	11 12
RETURN	34		
TERP1	1		
X	1AG	6	
X1	1AG	2	
X2	1AG	4	
X4	2=	8	15 17 21 25 29 32
X8	4=	8	15 18 21 25 30 32
X8	6=	15	19 21 25 31 32
Y	1AG	33=	
Y1	1AG	3	
Y2	1AG	5	
Y4	3=	13	15 21 23 25 27 32
Y8	5=	15	21 24 25 28 32
Y8	13=	15=	21= 25= 32= 33

1		SUBROUTINE LAPH	LAPH
	C		LAPH
	C	LAPH SUPERVISES THE CALCULATION OF THE PHOTON PRODUCTION AND	LAPH
	C	ENERGY PRODUCTION MATRICES FOR EACH MATERIAL.	LAPH
	C		LAPH
2		COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M	OVER1
		ITSL	OVER1
3		COMMON /BOOK/ LOILF2,LOLF12(100),LOILF1,LOLF11(500),NR16,NROW(100)	BOOK
4		IXDA=0	LAPH
5		IXSD=0	LAPH
6		ILO1=0	LAPH
7		ILO2=0	LAPH
	C	ILO2 IS THE NUMBER OF DISCRETE EXCITATION LEVELS BEING CONSIDERED	LAPH
	C	FOR THIS MATERIAL. IN OTHER WORDS, THERE ARE ILO2 SECTIONS WITH	LAPH
	C	LO=2 READ FROM FILE 15.	LAPH
	C	ILO1 IS THE TOTAL NUMBER OF YIELDS FOR NEUTRON FINE GROUPS AND	LAPH
	C	GAMMA GROUPS AS CALCULATED USING THE LO=1, LF=1 DATA ON FILE 15.	LAPH
	C	IXSD IS THE TOTAL NUMBER OF YIELDS CALCULATED USING LO=1, LF=2	LAPH
	C	DATA ON FILE 15.	LAPH
	C	IXDA IS THE TOTAL NUMBER OF CASCADE GAMMA RAYS RECONSTRUCTED FROM	LAPH
	C	THE FIXED NUMBER OF DISCRETE LEVELS.	LAPH
	C	ILO1, ILO2, AND IXSD ARE INCREMENTED IN SUBROUTINE PR15 WHILE	LAPH
	C	IXDA IS INCREMENTED IN TRC2.	LAPH
8		NR16=0	LAPH
9		LOILF1=0	LAPH
10		LOILF2=0	LAPH
11		REWIND 15	LAPH
12		REWIND 16	LAPH
13		REWIND 17	LAPH
14		IF (MTNO(1).EQ.0) GO TO 10	LAPH
15		CALL MESH	LAPH
16		CALL PR15	LAPH
17		IF (ILO2.EQ.0) GO TO 5	LAPH
18		CALL TRC2	LAPH
19	5	CALL XSEC	LAPH
20	10	CALL MATRIX	LAPH
21		RETURN	LAPH
22		END	LAPH

SYMBOL	REFERENCES
S	17 19*
IN	14 20*
BOOK	3C0
EAUG	2C0
IAUG	2C0
ILO1	2C0 6=
ILO2	2C0 7= 17
IXDA	2C0 4=
IXSD	2C0 5=
LAPH	1
L01LF1	3C0 9=
L01LF2	3C0 10=
L01LF11	3C0
L01LF12	3C0
MATRIX	20
MATX	2C0
MESH	15
MTNG	2C0 14
MTSL	2C0
Np16	3C0 8=
NPOW	3C0
OVER1	2C0
PR15	16
RETURN	21
TPC2	18
XSEC	19





1		SUBROUTINE NORM	NORM
	C		NORM
	C	IN THIS ROUTINE THE FINE GROUP WEIGHTING FUNCTIONS ARE NORMALIZED	NORM
	C	OVER EACH BROAD GROUP.	NORM
2		COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I	BLANK
		1WO,IZM,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NBB,NENB,NENF,NFG,NG	BLANK
		2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW	BLANK
		3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV	BLANK
3		DO 20 I=1,NBG	NORM
4		SUMR=0.0	NORM
5		SUMS=0.0	NORM
6		IFST=0	NORM
7		DO 10 J=2,NENF	NORM
8		IF ((EMNF(J).LT.EMNR(I)).AND.(EMNF(J).GE.EMNR(I+1))) GO TO 5	NORM
9		GO TO 10	NORM
10	5	SUMS=SUMS+SW(J-1)	NORM
11		SUMR=SUMR+RW(J-1)	NORM
12		IF (IFST.EQ.0) IFST=J-1	NORM
13		ILST=J-1	NORM
14	10	CONTINUE	NORM
15		DO 20 K=IFST,ILST	NORM
16		IF (SUMR.EQ.0.0) GO TO 15	NORM
17		RW(K)=RW(K)/SUMR	NORM
18	15	CONTINUE	NORM
19		IF (SUMS.EQ.0.0) GO TO 20	NORM
20		SW(K)=SW(K)/SUMS	NORM
21	20	CONTINUE	NORM
22		RETURN	NORM
	C		NORM
23		END	NORM

SYMBOL	REFERENCES
5	8 10*
1^	7 9 14*
15	16 18*
2^	3 15 19 21*
A*RSAY	200
C	200
EG	200
ENG	200
EMNH	200 8
EMNF	200 8
GAMM	200
I	3 8
IFST	6= 12 15
I1ST	13= 15
IM	200
INO	200
IPES	200
I40	200
I7M	200
J	7 8 10 11 12 13
K	15 17 20
MA	200
MR	200
MC	200
MCR	200
MM	200
MS	200
MZ	200
N1G	200 3
NFNB	200
NFNF	200 7
NFG	200
NGAM	200
NGG	200
N1AT	200
N1M	200
NORM	1
NPM	200
R	200
RETURN	22
R11	200 11 17=
RYSC	200
RXSF	200
S1MR	4= 11= 16 17
S1MS	5= 10= 19 20
SW	200 10 20=
SXSC	200
SXSF	200

X11D	200
------	-----



```

1      SUBROUTINE RSF3                                RSF3
2      COMMON /TAPES/ ISI,ISO,IEN                    TAPES
3      COMMON /READ/ NR,NP,MAT,MF,MT,NBT(20),INT(20),E(2000),X(2000)  READ
      C NR=NO. OF INTERPOLATION BREAK PTS.          RSF3
      C NP=NO. OF CROSS SECTION, NEUTRON ENERGY PAIRS  RSF3
      C NBT(I) CONTAINS THE INDEX OF THE LAST PT. CORRESPONDING TO THE IN= RSF3
      C TERPOLATION CODE GIVEN IN INT(I)            RSF3
4      READ (IEN,10) NR,NP,MAT,MF,MT,(NBT(N),INT(N),N=1,NR)  RSF3
5      READ (IEN,15) (E(N),X(N),N=1,NP)              RSF3
6      READ (IEN,5) MAT,MF,MT                       RSF3
7      READ (IEN,5) MAT,MF,MT                       RSF3
8      RETURN                                        RSF3
      C
9      5      FORMAT (66X,I4,I2,I3)                  PSF3
10     10     FORMAT (44X,2I11,I4,I2,I3/(6I11))      PSF3
11     15     FORMAT (6E11.4)                       RSF3
12     END                                           RSF3

```

SYMBOL	REFERENCES
S	6RD 7RD 9*
I <sup>n</sup>	4RD 10*
I <sup>s</sup>	5RD 11*
E	3CD 5RD
IEN	2CD 4RD 5RD 6RD 7RD
INT	3CD 4RD
ISI	2CD
ISO	2CD
MAT	3CD 4RD 6RD 7RD
MF	3CD 4RD 6RD 7RD
MT	3CD 4RD 6RD 7RD
N	4RD 5RD
NBT	3CD 4RD
NP	3CD 4RD 5RD
NR	3CD 4RD
READ	3CD
RETURN	8
RSF3	1
TAPES	2CD
X	3CD 5RD

```

1      SUBROUTINE MESH                                          MESH
      C
      C      FORMS ENERGY MESH FOR INTEGRATION DETERMINED BY OVERLAYING THE MESH
      C      NEUTRON FINE GROUP ENERGY MESH AND THE CROSS SECTION MESH IN FILE3 MESH
      C      THIS ROUTINE ALSO PROVIDES FOR THE OPTION THAT ALL PHOTON MESH
      C      PRODUCTION DATA WHICH EXIST IN FILE 15 ARE USED WHEN MT=-1 IS MESH
      C      SPECIFIED. NOTE THAT ALL REACTION TYPES (MT NUMBERS) INCLUDED IN MESH
      C      FILE 15 ARE INCLUDED IN FILE 3. MESH
      C
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I BLANK
      C      IWO,IZH,MA(100),MR(50),MC(50),MCR,MM,MS,MZ(10),NBG,NENB,NENF,NFG,NG BLANK
      C      2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW BLANK
      C      3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV BLANK
3      COMMON /TAPES/ ISI,ISO,IEN TAPES
4      COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M OVER1
      C      ITSL OVER1
5      COMMON /READ/ NR,NP,MAT,MF,MT,NBT(20),INT(20),E(2000),X(2000) READ
6      DIMENSION MV(40) MESH
7      ILEVEL=1 MESH
8      IAUG=NENF MESH
9      DO 5 I=1,NENF MESH
10     K=NENF+1-I MESH
11     5 EAUG(I)=EMNF(K) MESH
12     REWIND IEN MESH
13     READ (IEN,150) AWRSAV MESH
14     10 READ (IEN,190) MAT,MF,MT MESH
15     IF (MF.NE.3) GO TO 10 MESH
16     15 DO 35 I=1,MTSL MESH
17     IF (MT.EQ.MTNO(I)) GO TO 60 MESH
18     IF (MTNO(I).NE.-1) GO TO 35 MESH
      C      THE FOLLOWING TEST IS VERY SIGNIFICANT. IF PHOTON PRODUCTION DATA MESH
      C      ARE GIVEN IN FILE 15 FOR MT=4, THESE DATA ARE USED WHEN MT=-1 ONLY MESH
      C      IF DATA ARE NOT GIVEN FOR ANY MT SUCH THAT 5.LE.MT.LE.15 OR MESH
      C      51.LE.MT.LE.80. MESH
19     JMAX=ILEVEL-1 MESH
20     IF (JMAX.EQ.0) GO TO 60 MESH
21     DO 20 J=1,JMAX MESH
22     20 IF ((MT.GT.4.AND.MT.LE.15.AND.MV(J).EQ.4).OR.(MT.GE.51.AND.MT.LE.8
      C      10.AND.MV(J).EQ.4)) GO TO 25 MESH
23     GO TO 60 MESH
24     25 ILEVEL=ILEVEL-1 MESH
25     IF (J.EQ.ILEVEL) GO TO 60 MESH
26     JJ=J MESH
27     DO 30 J=JJ,ILEVEL MESH
28     30 MV(J)=MV(J+1) MESH
29     GO TO 60 MESH
30     35 CONTINUE MESH
31     CALL RSF3 MESH
32     IF (MF.NE.0) GO TO 15 MESH
33     40 IF (MTNO(1).EQ.-1) GO TO 50 MESH

```

34	45	GO TO 75	MESH
35	50	MTSL=ILEVEL-1	MESH
36		DO 55 I=1,MTSL	MESH
37	55	MTNO(I)=MV(I)	MESH
38		WRITE (ISO,195) MTSL,(MTNO(I),I=1,MTSL)	MESH
39		GO TO 45	MESH
40	60	MV(ILEVEL)=MT	MESH
41		CALL RSF3	MESH
42		K=1	MESH
43		IMAX=IAUG-1	MESH
44		DO 65 I=1,IMAX	MESH
45		X(K)=EAUG(I)	MESH
46		K=K+1	MESH
47		DO 65 J=1,NP	MESH
48		IF (E(J),LE,EAUG(I),OR,E(J),GE,EAUG(I+j)) GO TO 65	MESH
49		X(K)=E(J)	MESH
50		K=K+1	MESH
51	65	CONTINUE	MESH
52		X(K)=EAUG(IAUG)	MESH
53		DO 70 I=1,K	MESH
54	70	EAUG(I)=X(I)	MESH
55		IAUG=K	MESH
56		ILEVEL=ILFVEL+1	MESH
57		IF (MF,NE,0) GO TO 15	MESH
58		GO TO 40	MESH
	C	THIS PART OF THE SUBROUTINE ADDS TO THE UNION OF THE SETS THOSE	MESH
	C	ENERGIES AT WHICH THE YIELDS ARE TABULATED IN FILE 15 FOR LO=1,	MESH
	C	LF=1,2 FOR THOSE MT NUMBERS INCLUDED IN THE PROBLEM.	MESH
59	75	READ (IEN,155) LO,MAT,MF,MT	MESH
60		IF (MF,NE,15) GO TO 75	MESH
61		GO TO 85	MESH
62	80	READ (IEN,160) LO,NK,MAT,MF,MT	MESH
63		IF (MF,EQ,0) GO TO 145	MESH
64	85	DO 90 I=1,MTSL	MESH
65	90	IF (MT,EQ,MTNO(I)) GO TO 100	MESH
66	95	READ (IEN,190) MAT,MF,MT	MESH
67		IF (MF,EQ,0) GO TO 145	MESH
68		IF (MT,EQ,0) GO TO 80	MESH
69		GO TO 95	MESH
70	100	IF (LO,EQ,2) GO TO 140	MESH
71		(STOR=)	MESH
72		READ (IEN,165) NR,NP	MESH
73		READ (IEN,170) (NN,NN,I=1,NR)	MESH
74		READ (IEN,175) (XX,XX,I=1,NP)	MESH
75		DO 125 J=1,NK	MESH
76		READ (IEN,180) LF,NR,NP	MESH
77		IF (LF,EQ,2) GO TO 110	MESH
78		READ (IEN,170) (NN,NN,I=1,NR)	MESH
79		READ (IEN,175) (XX,XX,I=1,NP)	MESH
80		READ (IEN,165) NRRN,NTRS	MESH

81		READ (IEN,170) (NN,NN,I=1,NBPN)	MESH
82		DO 105 K=1,NTBS	MESH
83		ISTOR=ISTOR+1	MESH
84		READ (IEN,185) E(ISTOR),NBR2,NPR2	MESH
85		READ (IEN,170) (NN,NN,I=1,NBR2)	MESH
86		READ (IEN,175) (XX,XX,I=1,NPR2)	MESH
87	100	CONTINUE	MESH
88		GO TO 125	MESH
89	110	READ (IEN,170) (NN,NN,I=1,NR)	MESH
90		READ (IEN,175) (E(I),XX,I=1,NP)	MESH
91		K=1	MESH
92		IMAX=IAUG-1	MESH
93		DO 115 I=1,IMAX	MESH
94		X(K)=EAUG(I)	MESH
95		K=K+1	MESH
96		DO 115 JJ=1,NP	MESH
97		IF (E(JJ).LE.EAUG(I).OR.E(JJ).GE.EAUG(I+1)) GO TO 115	MESH
98		X(K)=E(JJ)	MESH
99		K=K+1	MESH
100	110	CONTINUE	MESH
101		X(K)=EAUG(IAUG)	MESH
102		DO 120 I=1,K	MESH
103	120	EAUG(I)=X(I)	MESH
104		IAUG=K	MESH
105	125	CONTINUE	MESH
106		IF (ISTOR.EQ.0) GO TO 140	MESH
107		K=1	MESH
108		IMAX=IAUG-1	MESH
109		DO 130 I=1,IMAX	MESH
110		X(K)=EAUG(I)	MESH
111		K=K+1	MESH
112		DO 130 J=1,ISTOR	MESH
113		IF (E(J).LE.EAUG(I).OR.E(J).GE.EAUG(I+1)) GO TO 130	MESH
114		X(K)=E(J)	MESH
115		K=K+1	MESH
116	130	CONTINUE	MESH
117		X(K)=EAUG(IAUG)	MESH
118		DO 135 I=1,K	MESH
119	135	EAUG(I)=X(I)	MESH
120		IAUG=K	MESH
121	140	READ (IEN,190) MAT,MF,MT	MESH
122		IF (MT.EQ.0) GO TO 80	MESH
123		GO TO 140	MESH
124	145	IF (IAUG.GT.2000) CALL ERROR (400)	MESH
125		RETURN	MESH
		C	MESH
126	150	FORMAT (11X,E11.4)	MESH
127	155	FORMAT (22X,I11,33X,I4,I2,I3)	MESH
128	160	FORMAT (22X,I11,22X,I11,I4,I2,I3)	MESH
129	165	FORMAT (44X,2I11)	MESH

130	170	FORMAT (6I11)	MESH
131	175	FORMAT (6E11.4)	MESH
132	180	FORMAT (33X,3I11)	MESH
133	185	FORMAT (11X,E11.4,22X,2I11)	MESH
134	190	FORMAT (66X,I4,I2,I3)	MESH
135	195	FORMAT (* UNDER THE OPTION PROVIDED WHEN INPUT MT=-1 IS USED, THERE WILL BE *I4,* REACTION TYPES USED AS FOLLOWS - */>(* 2NO(I)=*,20I4,/))	MESH
136		END	MESH

SYMBOL	REFERENCES
5	9 11*
11	14* 15
15	16* 32 57
20	21 22*
25	22 24*
30	27 28*
35	16 18 30*
40	33* 58
45	34* 39
50	33 35*
55	36 37*
60	17 20 23 25 29 40*
65	44 47 48 51*
70	53 54*
75	34 59* 60
80	62* 68 122
85	61 64*
90	64 65*
95	66* 69
100	65 70*
105	82 87*
110	77 89*
115	93 96 97 100*
120	102 103*
125	75 88 105*
130	109 112 113 116*
135	118 119*
140	74 106 121* 123
145	63 67 124*
150	13RD 126*
155	59RD 127*
160	62RD 128*
165	72RD 80RD 129*
170	73RD 78RD 81RD 85RD 89RD 130*
175	74RD 79RD 86RD 90RD 131*
180	76RD 132*
185	64RD 133*
190	14RD 66RD 121RD 134*
195	38WX 135*
A4RSAV	2C0 13RD
C	2C0
E	5C0 48 49 84RD 90RD 97 98 113 114
EAUG	4C0 11= 45 48 52 54= 94 97 101 103=
	110 113 117 119=
EG	2C0
EMG	2C0
EMNB	2C0
EMNF	2C0 11

ERROR	-	124									
GAMM	-	2C0									
I	-	9	10	11	16	17	18	36	37	38WR	44
		45	48	53	54	64	65	73RD	74RD	78RD	79RD
		81RD	85RD	86RD	89RD	90RD	93	94	97	102	103
		109	110	113	118	119					
IAUG	-	4C0	8=	43	52	55=	92	101	104=	108	117
		120=	124								
IFN	-	3C0	12	13RD	14RD	59RD	62RD	66RD	72RD	73RD	74RD
		76RD	78RD	79RD	80RD	81RD	84RD	85RD	86RD	89RD	90RD
		121RD									
ILEVEL	-	7=	19	24=	25	27	35	40	56=		
ILO1	-	4C0									
ILO2	-	4C0									
IM	-	2C0									
IMAX	-	43=	44	92=	93	108=	109				
INT	-	5C0									
IOD	-	2C0									
INES	-	2C0									
ISI	-	3C0									
ISO	-	3C0	38WR								
ISTOR	-	71=	83=	84RD	106	112					
IWO	-	2C0									
IYDA	-	4C0									
IYSD	-	4C0									
I7M	-	2C0									
J	-	21	22	25	26	27	28	47	48	49	75
		112	113	114							
J1	-	26=	27	96	97	98					
JMAX	-	19=	20	21							
K	-	10=	11	42=	45	46=	49	50=	52	53	55
		82	91=	94	95=	98	99=	101	102	104	107=
		110	111=	114	115=	117	118	120			
LF	-	76RD	77								
LO	-	59RD	62RD	70							
MA	-	2C0									
MAT	-	5C0	14RD	59RD	62RD	66RD	121RD				
MATX	-	4C0									
MP	-	2C0									
MC	-	2C0									
MCR	-	2C0									
MESH	-	1									
MF	-	5C0	14RD	15	32	57	59RD	60	62RD	63	66RD
		67	121RD								
MM	-	2C0									
MS	-	2C0									
MT	-	5C0	14RD	17	22	40	59RD	62RD	65	66RD	68
		121RD	122								
MTNO	-	4C0	17	18	33	37=	38WR	65			
MTSL	-	4C0	16	35=	36	38WR	64				



MV	-	6D1	22	28=	37	40=						
M7	-	2C0										
NRG	-	2C0										
NHR2	-	84RD	85RD									
NHRN	-	80RD	81RD									
NHT	-	5C0										
NFNB	-	2C0										
NFNH	-	2C0	8	9	10							
NFG	-	2C0										
NGAM	-	2C0										
NGG	-	2C0										
NK	-	62RD	75									
NMAT	-	2C0										
NN	-	73RD	78RD	81RD	85RD	89RD						
NNM	-	2C0										
NP	-	5C0	47	72RD	74RD	76RD	79RD	90RD	96			
NPM	-	2C0										
NPR2	-	84RD	86RD									
NP	-	5C0	72RD	73RD	76RD	78RD	89RD					
NTHS	-	80RD	82									
OVER1	-	4C0										
R	-	2C0										
RFAD	-	5C0										
RFTURN	-	125										
RSF3	-	31	41									
Rw	-	2C0										
RxSC	-	2C0										
RxSF	-	2C0										
Sw	-	2C0										
SxSC	-	2C0										
SxSF	-	2C0										
TAPES	-	3C0										
X	-	5C0	45=	49=	52=	54	94=	98=	101=	103	110=	
		114=	117=	119								
XND	-	2C0										
XY	-	74RD	79RD	86RD	90RD							

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1      SUBROUTINE PR15
C
C      THIS ROUTINE READS THE PHOTON PRODUCTION DATA FROM FILE 15 OF THE
C      ENDF/B TAPE. FOR A CONTINUOUS ENERGY DISTRIBUTION UNDER OPTION 1,
C      THE PHOTON GROUP YIELDS, Y AND YTLDA, ARE CALCULATED ON EITHER
C      TRACK 1 OR 2 AND WRITTEN ONTO TAPE 15.
C      FOR DISTRIBUTIONS UNDER OPTION 1 AT DISCRETE GAMMA
C      ENERGIES, THE YIELDS ARE WRITTEN DIRECTLY ONTO TAPE 17.
C      FOR OPTION 2 THE TRANSITIONAL PROBABILITIES AND
C      CONDITIONAL PROBABILITIES ARE READ FROM THE ENDF/B TAPE AND
C      WRITTEN ONTO TAPE 16 FOR LATER USE IN SUBROUTINE TRC2.
C
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I
BLANK
1WO,IZM,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NBG,NENB,NENF,NFG,NG
BLANK
2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW
BLANK
3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV
BLANK
COMMON /TAPES/ ISI,ISO,IEN
TAPES
4      COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M
OVER1
1TSL
OVER1
5      COMMON /READ/ NR,NP,MAT,MF,MT,NBT(20),INT(20),E(2000),X(2000)
READ
6      COMMON /BULK/ Y1(2000),Y2(2000),YINT(2000),YNEW(2000),EG1(2000),EG
BULK1
12(2000),NBT1(20),IBT1(20),NBT2(20),IBT2(20)
BULK1
7      COMMON /SAVE/ SAVE(1000,4),ISAVE(1000)
SAVE1
8      COMMON /BOOK/ LO1LF2,LOLF2(100),LO1LF1,LOLF1(500),NR16,NROW(100)
BOOK
9      DIMENSION SAVEL(4000),NBTN(20),INTN(20)
PR15
10     EQUIVALENCE (SAVEL(1),SAVE(1,1))
PR15
11     EXTERNAL LOCT
PR15
12     REWIND IEN
PR15
13     5 READ (IEN,250) MAT,MF,MT
PR15
14     IF (MF.NE.3) GO TO 5
PR15
15     10 READ (IEN,230) LO,LG,MAT,MF,MT
PR15
16     IF (MF.NE.15) GO TO 10
PR15
17     GO TO 20
PR15
18     15 READ (IEN,245) ZA,AWR,LO,LG,IT1,NK,MAT,MF,MT
PR15
19     IF (MF.EQ.0) GO TO 225
PR15
20     20 CONTINUE
PR15
21     DO 25 I=1,MTSL
PR15
22     25 IF (MT.EQ.MTNO(I)) GO TO 35
PR15
C     IS THIS MT REQUIRED
PR15
C     SKIP TO NEXT SECTION IF MT NOT REQUIRED
PR15
23     30 READ (IEN,250) MAT,MF,MT
PR15
24     IF (MF.EQ.0) GO TO 225
PR15
C     END OF FILE 15- RETURN
PR15
25     IF (MT.EQ.0) GO TO 15
PR15
26     GO TO 30
PR15
27     35 IF (LO.EQ.2) GO TO 205
PR15
C     READ TOTAL YIELD TABLE (FOR ALL LAWS)
PR15
28     READ (IEN,245) ZA,AWR,LO,LG,NR,NP
PR15
29     READ (IEN,255) (NBT(I),INT(I),I=1,NR)
PR15
30     READ (IEN,260) (E(I),X(I),I=1,NP)
PR15

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31    C      NOW GET TOTAL YIELD FOR EACH ENERGY IN EAUG ARRAY. PR15
      ILAW=0 PR15
32    C      LOOP ONCE FOR EACH LAW PR15
      READ (IEN,245) ZA,AWR,LO,LF,NR,NP PR15
33    IF (LF.EQ.1) GO TO 70 PR15
      C      THIS SECTION OF THE CODE FOR LO=1, LF=2 PR15
34    READ (IEN,255) (NBT(I),INT(I),I=1,NR) PR15
35    READ (IEN,260) (E(I),X(I),I=1,NP) PR15
36    IF (AWR.GT.EMG(1).OR.AWR.LT.EMG(NGAM)) GO TO 65 PR15
37    ISTAR=1 PR15
38    IKX=0 PR15
39    DO 55 I=1,IAUG PR15
40    ILO=LOCT(E,EAUG(I),NP) PR15
41    IF (ILO.EQ.-1) GO TO 55 PR15
42    IHI=ILO+1 PR15
43    DO 45 J=1,NR PR15
44    45 IF (IHI.LE.NBT(J)) GO TO 50 PR15
45    50 IXSD=IXSD+1 PR15
46    CALL TERP1 (E(ILO),X(ILO),E(IHI),X(IHI),EAUG(I),SAVE(ISTAR,2),INT(
      IJ)) PR15
      C      SAVE(ISTAR,2) NOW CONTAINS THE INTERPOLATED YIELD PR15
47    SAVE(ISTAR,1)=EAUG(I) PR15
48    SAVE(ISTAR,3)=AWR*SAVE(ISTAR,2) PR15
      C      AWR CONTAINS PHOTON ENERGY PR15
49    ISTAR=ISTAR+1 PR15
50    IF (ISTAR.LE.1000) GO TO 55 PR15
51    WRITE (17) ((SAVE(IX,J),J=1,3),IX=1,1000),MT,AWR PR15
52    IKX=IKX+1 PR15
53    ISTAR=1 PR15
54    55 CONTINUE PR15
55    IF (ISTAR.EQ.1.AND.IKX.EQ.n) GO TO 65 PR15
56    ISTAR=ISTAR-1 PR15
57    IF (ISTAR.EQ.0) GO TO 60 PR15
58    WRITE (17) ((SAVE(IX,J),J=1,3),IX=1,ISTAR),MT,AWR PR15
59    60 L01LF2=L01LF2+1 PR15
60    IF (L01LF2.GT.100) CALL ERROR (500) PR15
61    L01LF2(L01LF2)=ISTAR+IKX*1000 PR15
62    ISTAR=1 PR15
63    65 ILAW=ILAW+1 PR15
64    IF (ILAW.LT.NK) GO TO 40 PR15
65    GO TO 220 PR15

      C PR15
      C FOR EACH GAMMA ENERGY THERE IS A SINGLE ENTRY IN THE L01LF2 ARRAY PR15
      C INDICATING THE TOTAL NUMBER OF VALUES OF THE PHOTON YIELD WHICH PR15
      C HAVE BEEN INTERPOLATED. THERE ARE A TOTAL OF L01LF2 ENTRIES IN PR15
      C THIS ARRAY. THIS ARRAY IS FEDED IN SUBROUTINE XSEC FOR READING PR15
      C TAPE 17. THE SUM OF ALL THE L01LF2 ELEMENTS IN THE L01LF2 ARRAY PR15
      C IS IXSD. PR15
      C PR15
      C PR15
```

	C	THIS SECTION OF THE CODE FOR LO=1, LF=1	PR15
66	70	READ (IEN,255) (NBT(I),INT(I),I=1,NR)	PR15
67		READ (IEN,260) (E(I),X(I),I=1,NP)	PR15
	C	COMPUTE TOTAL YIELD FOR EACH ENERGY FOR THIS LAW	PR15
68		IFST=0	PR15
69		WRITE (ISO,265)	PR15
70		READ (IEN,245) ZA,AWR,LO,LG,NBRN,NTBS	PR15
71		READ (IEN,255) (NBTN(I),INTN(I),I=1,NBRN)	PR15
72		ITAB=1	PR15
73	75	CONTINUE	PR15
74		READ (IEN,245) ZA,EN2,LO,LG,NBR2,NPR2	PR15
75		READ (IEN,255) (NBT2(I),IBT2(I),I=1,NBR2)	PR15
76		READ (IEN,260) (EG2(I),Y2(I),I=1,NPR2)	PR15
77		IF (IFST.NE.0) GO TO 95	PR15
78	80	EN1=EN2	PR15
79		NBR1=NBR2	PR15
80		NPR1=NPR2	PR15
81		DO 85 I=1,NBR2	PR15
82		NBT1(I)=NBT2(I)	PR15
83	85	IBT1(I)=IBT2(I)	PR15
84		DO 90 I=1,NPR2	PR15
85		EG1(I)=EG2(I)	PR15
86	90	Y1(I)=Y2(I)	PR15
87		IFST=1	PR15
88		GO TO 75	PR15
89	95	DO 115 I=1,NPR2	PR15
90		ILO=LOCT(EG1,EG2(I),NPR1)	PR15
91		IF (ILO.NE.-1) GO TO 100	PR15
92		YNEW(I)=0.0	PR15
93		GO TO 115	PR15
94	100	IHI=ILO+1	PR15
95		DO 105 J=1,NBR1	PR15
96	105	IF (IHI.LE.NBT1(J)) GO TO 110	PR15
97	110	CALL TERP1 (EG1(ILO),Y1(ILO),EG1(IHI),Y1(IHI),EG2(I),YNEW(I),IBT1(IJ))	PR15
		CONTINUE	PR15
98	115	CONTINUE	PR15
	C	WE NOW HAVE 2 COINCIDENT TABLES	PR15
99		DO 200 II=1,NGG	PR15
100		KP=II+1	PR15
101		ISTOR=1	PR15
102		IKX=0	PR15
103		IPRINT=1	PR15
104		DO 190 IQWE=1,IAUG	PR15
105		EN=EAUG(IQWE)	PR15
106		IF ((EN.LT.EN1).OR.(EN.GT.EN2)) GO TO 100	PR15
107		DO 120 J=1,NBRN	PR15
108	120	IF (ITAB.LT.NBTN(J)) GO TO 125	PR15
109	125	DO 130 IQ=1,NPR2	PR15
110	130	CALL TERP1 (EN1,YNEW(IQ),EN2,Y2(IQ),EN,YINT(IQ),INTN(J))	PR15
	C	TABLE FOR EN IS NOW IN YINT(I.....NPR2)	PR15

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111      ILO1=ILO1+1                                PR15
112      ANS=0.0                                    PR15
113      ANS1=0.0                                    PR15
114      ILO=LOCT(EG2,GAMM(II),NPR2)                PR15
115      IHI=LOCT(EG2,GAMM(KP),NPR2)               PR15
116      XLOLIM=GAMM(II)                           PR15
117      XUPLIM=GAMM(KP)                           PR15
118      IF (ILO.NE.-1) GO TO 135                   PR15
119      IF ((GAMM(II).LT.EG2(1)).AND.(GAMM(KP).LT.EG2(1))) GO TO 160 PR15
120      ILO=1                                       PR15
121      XLOLIM=EG2(1)                               PR15
122      130 IF (IHI.NE.-1) GO TO 140                PR15
123      IF ((GAMM(II).GT.EG2(NPR2)).AND.(GAMM(KP).GT.EG2(NPR2))) GO TO 160 PR15
124      IHI=NPR2                                     PR15
125      XUPLIM=EG2(NPR2)                           PR15
126      140 IF (IHI.NE.ILO) GO TO 145              PR15
127      YL=EG2(ILO)*YINT(ILO)                      PR15
128      YH=EG2(ILO+1)*YINT(ILO+1)                 PR15
129      CALL INTG (EG2(ILO),YL,EG2(ILO+1),YH,XLOLIM,XUPLIM,2,ANS) PR15
130      CALL INTG (EG2(ILO),YINT(ILO),EG2(ILO+1),YINT(ILO+1),XLOLIM,XUPLIM PR15
      1,2,ANS1)
131      GO TO 160                                    PR15
132      145 IHI=IHI+1                               PR15
133      IMP=IHI-2                                    PR15
134      JK=ILO+1                                    PR15
      C FIRST PARTIAL INTEGRAL                      PR15
      C USE GAMMA ENERGIES AS WEIGHTS              PR15
135      YL=EG2(ILO)*YINT(ILO)                      PR15
136      YH=EG2(JK)*YINT(JK)                       PR15
137      CALL INTG (EG2(ILO),YL,EG2(JK),YH,XLOLIM,EG2(JK),2,ANS) PR15
138      CALL INTG (EG2(ILO),YINT(ILO),EG2(JK),YINT(JK),XLOLIM,EG2(JK),2,AN PR15
      1S1)
139      IF (IMP.LT.JK) GO TO 155                   PR15
140      DO 150 I=JK,IMP                             PR15
141      IL=I+1                                       PR15
      C MIDDLE INTEGRALS BETWEEN TABULATED POINTS PR15
142      YL=YINT(I)*EG2(I)                          PR15
143      YH=YINT(IL)*EG2(IL)                        PR15
144      CALL INTG (EG2(I),YL,EG2(IL),YH,EG2(I),EG2(IL),2,A) PR15
145      ANS=ANS+A                                    PR15
146      CALL INTG (EG2(I),YINT(I),EG2(IL),YINT(IL),EG2(I),EG2(IL),2,A) PR15
147      ANS1=ANS1+A                                  PR15
148      150 CONTINUE                                 PR15
149      150 CONTINUE                                 PR15
      C FINAL PARTIAL INTEGRAL                      PR15
150      I=IHI-1                                     PR15
151      YL=YINT(I)*EG2(I)                          PR15
152      YH=YINT(IHI)*EG2(IHI)                     PR15
153      CALL INTG (EG2(I),YL,EG2(IHI),YH,EG2(I),XUPLIM,2,A) PR15
154      ANS=ANS+A                                    PR15

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155      CALL INTG (EG2(I),YINT(I),EG2(IHI),YINT(IHI),EG2(I),XUPLIM,2,A)      PR15
156      ANS1=ANS1+A                                                              PR15
157      160  IF (ANS.EQ.0.0) GO TO 190                                          PR15
158      EHAT=ANS/ANS1                                                            PR15
159      IF (IWO.EQ.1) GO TO 165                                                 PR15
160      KLZ=NGAM-I                                                               PR15
161      SAVE(ISTOR,2)=ANS1                                                       PR15
162      SAVE(ISTOR,3)=ANS1*EG(KLZ)                                             PR15
163      GO TO 170                                                                PR15
164      165  SAVE(ISTOR,2)=ANS/((GAMM(II)+GAMM(KP))/2.0)                       PR15
165      SAVE(ISTOR,3)=ANS                                                       PR15
166      170  IF (IPRINT.EQ.0) GO TO 175                                         PR15
167      WRITE (ISO,270) ILO1,MT,GAMM(II),GAMM(KP),ANS,ANS1,EHAT              PR15
168      IPRINT=0                                                                PR15
169      175  ILO=LOCT(E,EN,NP)                                                  PR15
170      IF (ILO.EQ.-1) CALL ERROR (501)                                         PR15
171      IHI=ILO+1                                                                PR15
172      DO 180 J=1,NR                                                           PR15
173      180  IF (IHI.LE.MBT(J)) GO TO 185                                       PR15
174      CALL ERROR (502)                                                         PR15
175      185  CALL TERP1 (E(ILO),X(ILO),E(IHI),X(IHI),EN,XINT,INT(J))          PR15
176      SAVE(ISTOR,2)=SAVE(ISTOR,2)*XINT                                       PR15
C      SAVE(ISTOR,2) HAS THE INTEGRAL OF THE PHOTON GROUP YIELD FROM EG      PR15
C      TO EG+1                                                                    PR15
177      SAVE(ISTOR,3)=SAVE(ISTOR,3)*XINT                                       PR15
C      SAVE(ISTOR,3) HAS THE INTEGRAL OF THE PHOTON GROUP ENERGY YIELD      PR15
C      FROM EG TO EG+1                                                            PR15
178      SAVE(ISTOR,1)=EN                                                        PR15
C      SAVE(ISTOR,1) HAS THE NEUTRON ENERGY                                    PR15
C      GAMM(KP) HAS THE UPPER LIMIT OF THE GAMMA ENERGY INTERVAL.          PR15
179      ISAVE(ISTOR)=MT                                                         PR15
180      ISTOP=ISTOR+1                                                           PR15
181      IF (ISTOR.LE.1000) GO TO 190                                           PR15
182      WRITE (15) ((SAVE(IX,J),J=1,3),IX=1,1000),MT,GAMM(KP)                PR15
183      IKX=IKX+1                                                                PR15
184      ISTOP=1                                                                  PR15
185      190  CONTINUE                                                           PR15
186      IF (ISTOR.EQ.1.AND.IKX.EQ.0) GO TO 200                                  PR15
187      ISTOP=ISTOR-1                                                           PR15
188      IF (ISTOR.EQ.0) GO TO 195                                              PR15
189      WRITE (15) ((SAVE(IX,J),J=1,3),IX=1,ISTOR),MT,GAMM(KP)              PR15
190      195  LOL1F1=LO1LF1+1                                                    PR15
191      IF (LO1LF1.GT.500) CALL ERROR (503)                                    PR15
192      LOLF1(LO1LF1)=ISTOR+IKX*1000                                          PR15
193      200  CONTINUE                                                           PR15
C      FOR EACH GAMMA GROUP THERE IS AN ENTRY IN THE LOLF11 ARRAY            PR15
C      INDICATING THE NUMBER OF NEUTRON FINE GROUPS OVER WHICH IT HAS        PR15
C      BEEN POSSIBLE TO INTEGRATE. THIS ARRAY HAS LO1LF1 ELEMENTS WHICH      PR15
C      ARE USED IN SUBROUTINE XSEC WHILE READING TAPE 15. THE SUM OF        PR15

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	C	ALL THE LOLF1 ELEMENTS IN THE LOLF11 ARRAY IS ILO1.	PR15
	C		PR15
	C	HAVE ALL TABLES FOR THIS LAW BEEN CHECKED	PR15
194		ITAB=ITAB+1	PR15
195		IF (ITAB.LT.NTBS) GO TO 80	PR15
196		ILAW=ILAW+1	PR15
197		IF (ILAW.GE.NK) GO TO 220	PR15
198		GO TO 40	PR15
	C	HEADS IN A SECTION FOR LO=2	PR15
	C	THIS SECTION OF THE CODE FOR TRANSITION PROBABILITY ARRAYS	PR15
199	205	ILO2=ILO2+1	PR15
200		READ (IEN,235) SAVEL(1),NTM2	PR15
	C	HEADS NO. OF TRANSITION PAIRS AND STATE ENERGY	PR15
201		IF (LG.EQ.2) GO TO 210	PR15
202		NTM2=2*NTM2+1	PR15
203		GO TO 215	PR15
204	210	NTM2=3*NTM2+1	PR15
205	215	READ (IEN,240) (SAVEL(I),I=2,NTM2)	PR15
206		WRITE (16) SAVEL(1),MT,LG,NTM2,(SAVEL(I),I=2,NTM2)	PR15
	C	PROCESS LO=2 SECTION	PR15
207	220	CONTINUE	PR15
208		HEAD (IEN,245) ZA,AWR,LO,LG,IT1,NK,MAT,MF,MT	PR15
	C	HEAD SEND RECORD AND CHECK FOR EOF	PR15
209		IF (MF.NE.0) GO TO 15	PR15
210	225	RETURN	PR15
	C		PR15
	C		PR15
	C		PR15
211	230	FORMAT (30X,I3,8X,I3,22X,I4,I2,I3)	PR15
212	235	FORMAT (E11.4,44X,I11)	PR15
213	240	FORMAT (6E11.4)	PR15
214	245	FORMAT (2E11.4,4I11,I4,I2,I3)	PR15
215	250	FORMAT (66X,I4,I2,I3)	PR15
216	255	FORMAT (6I11)	PR15
217	260	FORMAT (6E11.4)	PR15
218	265	FORMAT (60X,*OUTPUT FROM PR15*,/* INDEX ILO1 MT NUMBER 1 GAMMA ENERGY RANGE NUMERATOR DENOMINATOR 2 EHAT*)	PR15
219	270	FORMAT (2I10,5X,2E18.8,3E18.8)	PR15
220		END	PR15

SYMBOL		= = = = =	= = = = =	= = = = =	REFERENCES	= = = = =	= = = = =	= = = = =	= = = = =
5	-	13*	14						
10	-	15*	16						
15	-	16*	25	209					
20	-	17	20*						
25	-	21	22*						
30	-	23*	26						
35	-	22	27*						
40	-	32*	64	198					
45	-	43	44*						
50	-	44	45*						
55	-	39	41	50	54*				
60	-	57	59*						
65	-	36	55	63*					
70	-	33	66*						
75	-	73*	88						
80	-	78*	195						
85	-	81	83*						
90	-	84	86*						
95	-	77	89*						
100	-	91	94*						
105	-	95	96*						
110	-	96	97*						
115	-	89	93	98*					
120	-	107	108*						
125	-	108	109*						
130	-	109	110*						
135	-	118	122*						
140	-	122	126*						
145	-	126	132*						
150	-	141	148*						
155	-	139	149*						
160	-	119	123	131	157*				
165	-	159	164*						
170	-	163	166*						
175	-	166	169*						
180	-	172	173*						
185	-	173	175*						
190	-	104	106	157	181	185*			
195	-	188	190*						
200	-	99	186	193*					
205	-	27	199*						
210	-	201	204*						
215	-	203	205*						
220	-	65	197	207*					
225	-	19	24	210*					
230	-	15RD	211*						
235	-	206RD	212*						
240	-	205RD	213*						



SUBROUTINE PR15

245	-	16RD	28RD	32RD	70RD	74RD	208RD	214*				
250	-	13RD	23RD	215*								
255	-	29RD	34RD	66RD	71RD	75RD	216*					
260	-	30RD	35RD	67RD	76RD	217*						
265	-	69WR	218*									
270	-	167WR	219*									
A	-	144AG	145	146AG	147	153AG	154	155AG	156			
ANS	-	112=	129AG	137AG	145=	154=	157	158	164	165	167WR	
ANS1	-	113=	130AG	138AG	147=	156=	158	161	162	167WR		
A.R	-	14RD	28RD	32RD	36	48	51WR	58WR	70RD	208RD		
A-RSAV	-	2CU										
BROK	-	8CU										
BULK	-	6CU										
C	-	2CU										
E	-	5CU	30RD	35RD	40	46AG	67RD	169	175AG			
EAUG	-	4CU	40	46AG	47	105						
EA	-	2CU	162									
EA1	-	6CU	85=	90	97AG							
EA2	-	6CU	76RD	85	90	97AG	114	115	119	121	123	
		125	127	128	129AG	130AG	135	136	137AG	138AG	142	
		143	144AG	146AG	151	152	153AG	155AG				
E4AT	-	158=	167WR									
E4G	-	2CU	36									
E4NH	-	2CU										
E4NF	-	2CU										
E41	-	105=	106	110AG	169	175AG	178					
E42	-	78=	106	110AG								
E42	-	74RD	78	106	110AG							
EQRRR	-	60	170	174	191							
G4MM	-	2CU	114	115	116	117	119	123	164	167WR	182WR	
		189WR										
I	-	21	22	29RD	30RD	34RD	35RD	39	40	46AG	47	
		66RD	67RD	71RD	75RD	76RD	81	82	83	84	85	
		86	89	90	92	97AG	140	141	142	144AG	146AG	
		150=	151	153AG	155AG	205RD	206WR					
I4UG	-	4CU	39	104								
I4T1	-	6CU	83=	97AG								
I4T2	-	6CU	75RD	83								
I4N	-	3CU	12	13RD	15RD	18RD	23RD	28RD	29RD	30RD	32RD	
		34RD	35RD	66RD	67RD	70RD	71RD	74RD	75RD	76RD	200RD	
		205RD	208RD									
I4ST	-	68=	77	87=								
I4I	-	42=	44	46AG	94=	96	97AG	115=	122	124=	126	
		132=	133	150	152	153AG	155AG	171=	173	175AG		
I7	-	99	100	114	116	119	123	160	164	167WR		
I4X	-	38=	52=	55	61	102=	183=	186	192			
I4	-	141=	143	144AG	146AG							
I4AW	-	31=	63=	64	196=	197						
I4O	-	40=	41	42	46AG	90=	91	94	97AG	114=	118	
		120=	126	127	128	129AG	130AG	134	135	137AG	138AG	

SUBROUTINE PR15

		169=	170	171	175AG															
ILO1	-	4CO	111=	167WR																
ILO2	-	4CO	199=																	
IV	-	2CO																		
IMP	-	133=	139	140																
INT	-	5CO	29RD	34RD	46AG	66RD	175AG													
INTG	-	129	130	137	138	144	146	153	155											
INTN	-	90I	71RD	110AG																
IOO	-	2CO																		
IPRINT	-	103=	166	168=																
IO	-	109	110AG																	
IQWE	-	104	105																	
IQES	-	2CO																		
ISAVE	-	7CO	179=																	
ISJ	-	3CO																		
ISO	-	3CO	69WR	167WR																
ISTOR	-	37=	46AG	47	48	49=	50	53=	55	56=	57									
		58WR	61	62=	101=	161	162	164	165	176	177									
		178	179	180=	181	184=	186	187=	188	189WR	192									
IT1	-	18RD	208RD																	
ITAB	-	72=	108	194=	195															
IWO	-	2CO	159																	
IX	-	51WR	58WR	182WP	189WR															
IXDA	-	4CO																		
IXSD	-	4CO	45=																	
I7M	-	2CO																		
J	-	43	44	46AG	51WR	58WR	95	96	97AG	107	108									
		110AG	172	173	175AG	182WR	189WR													
JK	-	134=	136	137AG	138AG	139	140													
KLZ	-	160=	162																	
KO	-	100=	115	117	119	123	164	167WR	182WR	189WR										
LF	-	32RD	33																	
LG	-	15RD	18RD	28RD	70RD	74RD	201	206WR	208RD											
LO	-	15RD	18RD	27	28RD	32RD	70RD	74RD	208RD											
LO1LF1	-	8CO	190=	191	192															
LO1LF2	-	8CO	59=	60	61															
LOCT	-	11EX	40	90	114	115	169													
LOLF11	-	8CO	192=																	
LOLF12	-	8CO	61=																	
MA	-	2CO																		
MAT	-	5CO	13RD	15RD	18RD	23RD	20ARD													
MATX	-	4CO																		
MR	-	2CO																		
MC	-	2CO																		
MCR	-	2CO																		
MF	-	5CO	13RD	14	15RD	16	18RD	19	23RD	24	20ARD									
		209																		
MM	-	2CO																		
MS	-	2CO																		
MT	-	5CO	13RD	15RD	18RD	22	23RD	25	51WR	58WR	167WR									

	179	182WR	189WR	206WR	208RD						
MTNO	-	4CO	22								
MTSL	-	4CO	21								
M7	-	2CO									
NRG	-	2CO									
NRR1	-	79=	95								
NRR2	-	74RD	75RD	79	81						
NRRN	-	70RD	71RD	107							
NHT	-	5CO	29RD	34RD	44	66RD	173				
NHT1	-	6CO	82=	96							
NHT2	-	6CO	75RD	82							
NHTN	-	4DI	71RD	108							
NFNB	-	2CO									
NFNF	-	2CO									
NFG	-	2CO									
NGAM	-	2CO	36	160							
NGG	-	2CO	99								
NK	-	18RD	64	197	208RD						
NMAT	-	2CO									
NAM	-	2CO									
NP	-	5CO	28RD	30RD	32RD	35RD	40	67RD	169		
NPM	-	2CO									
NPR1	-	80=	90								
NPR2	-	74RD	76RD	80	84	89	109	114	115	123	124
		125									
NP	-	5CO	28RD	29RD	32RD	34RD	43	66RD	172		
NR16	-	8CO									
NR0W	-	8CO									
NTBS	-	70RD	195								
NTM2	-	200RD	202=	204=	205RD	206WR					
OVER1	-	4CO									
PR15	-	1									
R	-	2CO									
RFAID	-	5CO									
RFURU	-	210									
RW	-	2CO									
RXSC	-	2CO									
RXSF	-	2CO									
SAVE	-	7CO	10EQ	46AG	47=	48=	51WR	58WR	161=	162=	164=
		165=	176=	177=	178=	182WR	189WR				
SAVEL	-	9DI	10EQ	200RD	205RD	206WR					
Sw	-	2CO									
SXSC	-	2CO									
SXSF	-	2CO									
TAPES	-	3CO									
TFRPI	-	46	97	110	175						
X	-	5CO	30RD	35RD	46AG	67RD	175AG				
XJNT	-	175AG	176	177							
XIOLIM	-	116=	121=	129AG	130AG	137AG	138AG				
XMD	-	2CO									

XIOLIM	-	117=	125=	129AG	130AG	153AG	155AG				
Y1	-	6CO	86=	97AG							
Y2	-	6CO	76RD	86	110AG						
YH	-	128=	129AG	136=	137AG	143=	144AG	152=	153AG		
YTNT	-	6CO	110AG	127	128	130AG	135	136	138AG	142	143
		146AG	151	152	155AG						
YL	-	127=	129AG	135=	137AG	142=	144AG	151=	153AG		
YNEW	-	6CO	92=	97AG	110AG						
ZA	-	18RD	28RD	32RD	70RD	74RD	208RD				

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1      SUBROUTINE TRC2                                TRC2
C
C      THIS SUBROUTINE PROCESSES LO=2, FILE 15 INFORMATION. TRC2
C      IT RECONSTRUCTS THE MICROSCOPIC PHOTON PRODUCTION CROSS SECTIONS TRC2
C      FROM THE TRANSITION ARRAYS AS READ FROM TAPE 16 AND THE TRC2
C      APPROPRIATE CROSS SECTIONS AS READ FROM THE ENDF/B TAPE. TRC2
C      INTEGRATES OVER THE NEUTRON FINE GROUPS, MULTIPLIES BY THE TRC2
C      NORMALIZED FINE GROUP WEIGHTING FUNCTIONS, AND WRITES THE RESULTS TRC2
C      ON TAPE 16. TRC2
C
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I BLANK
1WO,IZH,MA(100),MH(50),MC(50),MCR,MH,MS,MZ(10),NBG,NENB,NENF,NFG,NG BLANK
2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW BLANK
3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV BLANK
3      COMMON /TAPES/ ISI,ISO,IEN TAPES
4      COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M OVER1
ITSL OVER1
5      COMMON /READ/ NR,NP,MAT,MF,MT,NBT(20),INT(20),E(2000),X(2000) READ
6      COMMON /BULK/ XLO2(40,50),LO1(40),LO2(40),LO3(40),EE1(50),FF2(50), BULK2
ITP1(50),TP2(50),XDAT(1952,4),LEVL(1952) BULK2
7      COMMON /SAVE/ SAVE(1000,4),ISAVE(1000) SAVE1
8      COMMON /BOOK/ LO1LF2,LO1LF2(100),LO1LF1,LO1LF1(500),NR16,NP0W(100) BOOK
9      DIMENSION CSEC(2000) TRC2
10     EQUIVALENCE (CSEC(1),XLO2(1,1)) TRC2
C      IEE IS THE INDEX FOR THE STORAGE IN EITHER THE EE1 OR EE2 ARRAYS TRC2
C      WHICHEVER ARRAY IS CURRENT. TRC2
C      ITP=INDEX OF CURRENT TRANSITION PAIR TRC2
C      IECP=INDEX FOR OBTAINING ENERGIES IN EE (INPUT) TRC2
C      NL02=INDE OF ROW IN XLO2,LO2 TRC2
C      ILO2=NO. ROWS IN XLO2,LO2 TRC2
C      IXDA=ROW FOR STORAGE IN XDAT TRC2
C      NOEE=SWITCH TO DETERMINE CURRENT EE ARRAY, TAKES VALUE +1 OR -1. TRC2
C      TAPE 16 WAS WRITTEN IN PR15. TRC2
11     REWIND 16 TRC2
12     DO 5 I=1,ILO2 TRC2
13     READ (16) XLO2(I,1),LO1(I),LO2(I),II,(XLO2(I,J),J=2,II) TRC2
14     LO3(I)=II TRC2
C      THE LO1 ARRAY HAS THE MT NUMBER, LO2 THE LG, LO3 THE NUMBER OF TRC2
C      ENTRIES. TRC2
C      BEGINNING OF THE PORTION OF TRC2 IN WHICH THE CASCADES ARE TRC2
C      RECONSTRUCTED. TRC2
15     IXDA=0 TRC2
16     DO 45 IRPR=1,ILO2 TRC2
17     NL02=IRPR TRC2
18     NOEE=1 TRC2
19     NEN=1 TRC2
20     IP=1.0 TRC2
21     IECP=1 TRC2
22     IEE=0 TRC2
23     ESR=XLO2(NL02,1) TRC2

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24		GO TO 20	TRC2
25	10	CONTINUE	TRC2
26		DO 15 NLO2=1,ILO2	TRC2
27	15	IF (ESR.EQ.XLO2(NLO2,1)) GO TO 20	TRC2
28		CALL ERROR (600)	TRC2
29	20	NT=L03(NLO2)	TRC2
30		NTT=2	TRC2
31		IF (L02(NLO2).EQ.2) NTT=3	TRC2
32		DO 30 ITP=2,NT,NTT	TRC2
33		IXDA=IXDA+1	TRC2
34		K=ITP+1	TRC2
35		KK=ITP+2	TRC2
36		XDAT(IXDA,1)=XLO2(IRPR,1)	TRC2
	C	INITIAL (HIGHEST) ENERGY ASSOCIATED WITH THIS CASCADE.	TRC2
37		XDAT(IXDA,2)=XLO2(NLO2,1)	TRC2
	C	ENERGY LEVEL FROM WHICH THIS TRANSITION OCCURS.	TRC2
38		XDAT(IXDA,3)=XLO2(NLO2,K)*TP	TRC2
39		IF (L02(NLO2).EQ.2) XDAT(IXDA,3)=XDAT(IXDA,3)*XLO2(NLO2,KK)	TRC2
	C	PROBABILITY FOR GAMMA EMISSION DURING DECAY TO ASSOCIATED LEVEL.	TRC2
40		XDAT(IXDA,4)=XDAT(IXDA,2)-XLO2(NLO2,ITP)	TRC2
	C	ENERGY OF THE EMITTED PHOTON	TRC2
41		LEVL(IXDA)=L01(IRPR)	TRC2
	C	THIS IS THE MT NUMBER CORRESPONDING TO THE ENERGY LEVEL FROM WHICH	TRC2
	C	THE CASCADE ORIGINATES.	TRC2
42		IF (XLO2(NLO2,ITP).EQ.0.0) GO TO 30	TRC2
43		IEE=IEE+1	TRC2
44		IF (NOEE.GT.0) GO TO 25	TRC2
45		TP1(IEE)=XLO2(NLO2,K)*TP	TRC2
46		EE1(IEE)=XLO2(NLO2,ITP)	TRC2
47		GO TO 30	TRC2
48	25	EE2(IEE)=XLO2(NLO2,ITP)	TRC2
49		TP2(IEE)=XLO2(NLO2,K)*TP	TRC2
50	30	CONTINUE	TRC2
51		IECR=IECR+1	TRC2
52		IF (IECR.LE.NEN) GO TO 35	TRC2
53		NOEE=-NOEE	TRC2
54		NEN=IEE	TRC2
55		IF (NEN.EQ.0) GO TO 45	TRC2
56		IECR=1	TRC2
57		IEE=0	TRC2
58	35	IF (NOEE.LT.0) GO TO 40	TRC2
59		ESP=EE1(IECR)	TRC2
60		TP=TP1(IECR)	TRC2
61		GO TO 10	TRC2
62	40	ESP=EE2(IECR)	TRC2
63		TP=TP2(IECR)	TRC2
64		GO TO 10	TRC2
65	45	CONTINUE	TRC2
	C	END OF CASCADE RECONSTRUCTION.	TRC2
	C	NOW MUST INTRODUCE THE CROSS SECTIONS FROM FILE 3.	TRC2

66		ENMAX=XLO2(ILO2,i)*(AWRSV+1.0)/AWRSV	TRC2
67		XDAT(IXDA+1,1)=999.347	TRC2
68		REWIND IEN	TRC2
69		REWIND 16	TRC2
70	50	READ (IEN,140) MAT,MF,MT	TRC2
71		IF (MF.NE.3) GO TO 50	TRC2
72		III=0	TRC2
73	55	III=III+1	TRC2
74		IF (III.GT.IXDA) RETURN	TRC2
75	60	IF (MT.EQ.LEVL(III)) GO TO 65	TRC2
76		CALL RSF3	TRC2
77		IF (MF.NE.0) GO TO 60	TRC2
78	65	CALL RSF3	TRC2
79		DO 70 I=1,IAUG	TRC2
80	70	CSEC(I)=0.0	TRC2
81		I1=LOCT(EAUG,XDAT(III,1),IAUG)	TRC2
82		IF (I1.EQ.-1) CALL ERROR (601)	TRC2
83		I2=LOCT(EAUG,ENMAX,IAUG)	TRC2
84		IF (I2.EQ.-1) CALL ERROR (602)	TRC2
	C	GETS THE CROSS SECTIONS FOR A PARTICULAR MT AND STORES THEM AWAY.	TRC2
85		DO 85 I=1,IAUG	TRC2
86		EN=EAUG(I)	TRC2
87		ILO=LOCT(E,EN,NP)	TRC2
88		IF (ILO.EQ.-1) GO TO 85	TRC2
89		IHI=ILO+1	TRC2
90		DO 75 J=1,NR	TRC2
91	75	IF (IHI.LE.NBT(J)) GO TO 80	TRC2
92		CALL ERROR (603)	TRC2
93	80	CALL TERP1 (E(ILO),X(ILO),E(IHI),X(IHI),EN,CSEC(I),INT(J))	TRC2
94	85	CONTINUE	TRC2
	C	NOW PROCEED TO INTEGRATE OVER THE FINE GROUPS.	TRC2
	C	THE NEUTRON INTEGRALS ARE DONE USING ORDINATES ONLY AT THOSE	TRC2
	C	ENERGIES INCLUDED IN THE UNION OF THE SETS OF NEUTRON ENERGIES	TRC2
	C	IN FILE 3 AND THE NEUTRON FINE GROUP ENERGY MESH.	TRC2
95		DO 120 II=1,NFG	TRC2
96		IF (EMNF(II+1).GT.ENMAX) GO TO 120	TRC2
97		IF (EMNF(II).LT.XDAT(III,1)) GO TO 120	TRC2
98		KP=II+1	TRC2
99		ANS=0.0	TRC2
100		ILO=LOCT(EAUG,EMNF(KP),IAUG)	TRC2
101		IHI=LOCT(EAUG,EMNF(II),IAUG)	TRC2
102		XLOLIM=EMNF(KP)	TRC2
103		XUPLIM=EMNF(II)	TRC2
104		IF (ILO.GT.I1) GO TO 90	TRC2
105		ILO=I1	TRC2
106		XLOLIM=XDAT(III,i)	TRC2
107	90	IF (IHI.LE.I2) GO TO 95	TRC2
108		IHI=I2	TRC2
109		XUPLIM=ENMAX	TRC2
110	95	IF (IHI.NE.ILO) GO TO 100	TRC2

```

111      CALL INTG (EAUG(ILO),CSEC(ILO),EAUG(ILO+1),CSEC(ILO+1),XL0LIM,XUPL TRC2
      1IM,2,ANS) TRC2
112      GO TO 115 TRC2
113      100 IHI=IHI+1 TRC2
114      IMP=IHI-2 TRC2
115      JK=ILO+1 TRC2
      C FIRST PARTIAL INTEGRAL TRC2
116      CALL INTG (EAUG(ILO),CSEC(ILO),EAUG(JK),CSEC(JK),XL0LIM,EAUG(JK),2 TRC2
      1,ANS) TRC2
117      IF (IMP.LT.,JK) GO TO 110 TRC2
118      DO 105 I=JK,IMP TRC2
119      IL=I+1 TRC2
      C MIDDLE INTEGRALS BETWEEN THE TABULATED FINE GROUP BOUNDARIES. TRC2
120      CALL INTG (EAUG(I),CSEC(I),EAUG(IL),CSEC(IL),EAUG(I),EAUG(IL),2,A) TRC2
121      ANS=ANS+A TRC2
122      105 CONTINUE TRC2
123      110 CONTINUE TRC2
      C FINAL PARTIAL INTEGRAL TRC2
124      I=IHI-1 TRC2
125      CALL INTG (EAUG(I),CSEC(I),EAUG(IHI),CSEC(IHI),EAUG(I),XUPLIM,2,A) TRC2
126      ANS=ANS+A TRC2
127      115 CONTINUE TRC2
      C ANS NOW CONTAINS THE INTEGRAL OVER ONE FINE GROUP OF SIGMA(E) TRC2
      C FOR THIS MT NUMBER. TRC2
128      EE1(II)=(ANS/(EMNF(II)-EMNF(KP)))*SW(II) TRC2
129      120 CONTINUE TRC2
130      ISTOP=1 TRC2
131      125 DO 130 I=1,NFG TRC2
132      IF (EMNF(I+1).GT.ENMAX) GO TO 130 TRC2
133      IF (EMNF(I).LT.XDAT(III,1)) GO TO 130 TRC2
134      SAVE(ISTOR,1)=EMNF(I) TRC2
135      SAVE(ISTOR,2)=XDAT(III,3)*EE1(I) TRC2
136      SAVE(ISTOR,3)=SAVE(ISTOR,2)*XDAT(III,4) TRC2
137      SAVE(ISTOR,4)=XDAT(III,4) TRC2
138      ISTOP=ISTOR+1 TRC2
139      130 CONTINUE TRC2
140      IF (XDAT(III,1).EQ.XDAT(III+1,1)) GO TO 135 TRC2
141      NR16=NR16+1 TRC2
142      ISTOP=ISTOR-1 TRC2
143      NROW(NR16)=ISTOR TRC2
144      WRITE (16) ((SAVE(IX,J),J=1,4),IX=1,ISTOR) TRC2
145      GO TO 55 TRC2
146      135 III=III+1 TRC2
147      GO TO 125 TRC2
      C TRC2
148      140 FORMAT (66X,I4,I2,I3) TRC2
149      END TRC2

```

SYMBOL	=	=	=	=	=	=	=	=	=	REFERENCES	=	=	=	=	=	=	=	=	=	
5	-	12	14*																	
1	-	25*	61	64																
15	-	26	27*																	
21	-	24	27	29*																
25	-	44	48*																	
31	-	32	42	47	50*															
35	-	52	58*																	
41	-	58	62*																	
45	-	16	55	65*																
51	-	70*	71																	
55	-	73*	145																	
61	-	75*	77																	
65	-	75	78*																	
71	-	79	80*																	
75	-	90	91*																	
81	-	91	93*																	
85	-	85	88	94*																
91	-	104	107*																	
95	-	107	110*																	
101	-	110	113*																	
105	-	114	122*																	
111	-	117	123*																	
115	-	112	127*																	
121	-	95	96	97	129*															
125	-	131*	147																	
131	-	131	132	133	139*															
135	-	140	146*																	
141	-	70RD	148*																	
A	-	120AG	121	125AG	126															
AMS	-	99=	111AG	116AG	121=	126=	128													
AMRSV	-	2C0	66																	
BOOK	-	8C0																		
BULK	-	6C0																		
C	-	2C0																		
CONF	-	9DI	10EQ	80=	93AG	111AG	116AG	120AG	125AG											
E	-	5C0	37	93AG																
EAJG	-	4C0	81	83	86	100	101	111AG	116AG	120AG	125AG									
EF1	-	6C0	46=	59	128=	135														
EF2	-	6C0	48=	62																
EG	-	2C0																		
ENG	-	2C0																		
ENH	-	2C0																		
ENHF	-	2C0	96	97	100	101	102	103	128	132	133									
	-	134																		
ET	-	86=	87	93AG																
ENMAX	-	66=	83	96	109	132														
ERROR	-	2H	82	84	92															
ESR	-	23=	27	59=	62=															



SUBROUTINE TRC2

GAMM	-	2CO									
I	-	12	13RD	14	79	80	85	86	93AG	118	119
		120AG	124=	125AG	131	132	133	134	135		
Ij	-	81=	82	104	105						
Ij	-	83=	84	107	108						
IAUG	-	4CO	79	81	83	85	100	101			
IFCR	-	21=	51=	52	56=	59	60	62	63		
IFE	-	22=	43=	45	46	48	49	54	57=		
IFN	-	3CO	68	70RD							
IHI	-	89=	91	93AG	101=	107	108=	110	113=	114	124
		125AG									
II	-	13RD	14	95	96	97	98	101	103	128	
III	-	72=	73=	74	75	81	97	106	133	135	136
		137	140	146=							
IL	-	119=	120AG								
ILO	-	87=	88	89	93AG	100=	104	105=	110	111AG	115
		116AG									
II.01	-	4CO									
II.02	-	4CO	12	16	26	66					
IM	-	2CO									
IMP	-	114=	117	118							
INT	-	5CO	93AG								
INTG	-	111	116	120	125						
I00	-	2CO									
I4FS	-	2CO									
I7PR	-	16	17	36	41						
ISAVE	-	7CO									
ISI	-	3CO									
ISO	-	3CO									
ISTOR	-	130=	134	135	136	137	138=	142=	143	144WR	
I7P	-	32	34	35	40	42	46	48			
I40	-	2CO									
I4	-	144WR									
IYDA	-	4CO	15=	33=	36	37	38	39	40	41	67
		74									
IYSD	-	4CO									
I7M	-	2CO									
J	-	13RD	90	91	93AG	144WR					
Jk	-	115=	116AG	117	118						
K	-	34=	38	45	49						
Kk	-	35=	39								
Kj	-	98=	100	102	128						
LFVL	-	6CO	41=	75							
L01	-	6CO	13RD	41							
L01LF1	-	3CO									
L01LF2	-	8CO									
L02	-	6CO	13RD	31	39						
L03	-	6CO	14=	29							
L0CT	-	81	83	87	100	101					
L0LF11	-	8CO									

LOLF12	-	800																			
MA	-	200																			
MAT	-	500	70RD																		
MATX	-	400																			
MA	-	200																			
MC	-	200																			
MCR	-	200																			
MF	-	500	70RD	71	77																
MH	-	200																			
MS	-	200																			
MT	-	500	70RD	75																	
MTNO	-	400																			
MTSL	-	400																			
MZ	-	200																			
NAG	-	200																			
NPT	-	500	91																		
NFN	-	19=	52	54=	55																
NFNH	-	200																			
NFNF	-	200																			
NFG	-	200	95	131																	
NSAM	-	200																			
NSG	-	200																			
NI,02	-	17=	23	26	27	29	31	37	38	39	40										
		42	45	46	48	49															
NMAT	-	200																			
NMM	-	200																			
NOEC	-	18=	44	53=	58																
NP	-	500	87																		
NPM	-	200																			
NP	-	500	90																		
NR16	-	800	141=	143																	
NROW	-	800	143=																		
NT	-	29=	32																		
NTT	-	30=	31=	32																	
OVER1	-	400																			
R	-	200																			
READ	-	500																			
RETURN	-	74																			
RSEF3	-	76	78																		
RJ	-	200																			
RXSC	-	200																			
RYSF	-	200																			
SAVE	-	700	134=	135=	136=	137=	144WR														
SM	-	200	128																		
SXSC	-	200																			
SXSF	-	200																			
TAPES	-	300																			
TRP1	-	93																			
TP	-	20=	38	45	49	60=	63=														
TP1	-	600	45=	60																	

TP2	-	600	49=	63																	
TRC2	-	1																			
X	-	500	93AG																		
XDAT	-	600	36=	37=	38=	39=	40=	67=	81	97	106										
		133	135	136	137	140															
XI,02	-	600	10EQ	13RD	23	27	36	37	38	39	40										
		42	45	46	48	49	66														
XI,OLIM	-	102=	106=	111AG	116AG																
XID	-	200																			
XI,PLIM	-	103=	109=	111AG	125AG																

```

1      SUBROUTINE XSEC                                XSEC
C                                          XSEC
C      THIS SUBROUTINE OBTAINS THE APPROPRIATE CROSS SECTIONS FROM FILE 3 XSEC
C      AND MULTIPLIES THEM BY THE YIELDS WHICH ARE READ FROM TAPES 15 AND XSEC
C      17. THE INTEGRATION OVER NEUTRON ENERGY USING EITHER TRACK A OR B XSEC
C      IS CARRIED OUT AND THE RESULTS ARE MULTIPLIED BY THE NORMALIZED XSEC
C      FINE GROUP WEIGHTING FUNCTIONS. FINALLY, THE RESULTS ARE WRITTEN XSEC
C      ONTO TAPE 16.                                XSEC
C                                          XSEC
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,I00,IRES,I  RLANK
      IWO,IZM,MA(100),MR(50),MC(50),MCR,MM,MS,MZ(10),NBG,NENB,NENF,NFG,NG  RLANK
      ZAM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),PXSC(100),SXSF(100),SW  RLANK
      3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV  RLANK
3      COMMON /TAPES/ ISI,ISO,IEN  TAPES
4      COMMON /OVER1/ EAUG(2000),IAUG,ILO1,ILO2,IXDA,IXSD,MATX,MTNO(40),M  OVER1
      ITSL  OVER1
5      COMMON /READ/ NR,NP,MAT,MF,MT,NRT(20),INT(20),E(2000),X(200*)  RFAD
6      COMMON /BULK/ XDAT(3020,3),EX(3020)  XSEC
7      COMMON /SAVE/ SAVE(1000,4),ISAVE(1000)  SAVE1
8      COMMON /HOOK/ LO1,LF2,LOLF12(100),LOLFI1,LOLF11(500),NR16,NROW(100)  HOOK
9      EXTERNAL LOCT  XSEC
10     IF (IXSD.EQ.0.AND.ILO1.EQ.0) RETURN  XSEC
C      THESE TAPES WERE WRITTEN IN PR15. TAPE 15 HAS LO=1, LF=1  XSEC
C      INFORMATION WHILE TAPE 17 HAS LO=1, LF=2 INFORMATION.  XSEC
11     REWIND 15  XSEC
12     REWIND 17  XSEC
13     ICOUNT=0  XSEC
14     IFLOW=1  XSEC
15     ISTORE=1  XSEC
16     5 REWIND IEN  XSEC
17     10 READ (IEN,175) MAT,MF,MT  XSEC
18     IF (MF.NE.3) GO TO 10  XSEC
19     MTX=MT  XSEC
20     CALL RSF3  XSEC
21     15 GO TO (20,40,170), IFLOW  XSEC
22     20 IF (IXSD.NE.0) GO TO 25  XSEC
23     IFLOW=2  XSEC
24     GO TO 15  XSEC
25     25 ICOUNT=ICOUNT+1  XSEC
26     IMIN=1  XSEC
27     NPTS=LOLF12(ICOUNT)  XSEC
28     N=NPTS/1000  XSEC
29     IF (N.EQ.0) GO TO 35  XSEC
30     IMAX=1000  XSEC
31     DO 30 II=1,N  XSEC
32     READ (17) ((XDAT(I,J),J=1,3),I=IMIN,IMAX),LLEVL,XDAT4  XSEC
33     IMIN=IMIN+1000  XSEC
34     IMAX=IMAX+1000  XSEC
35     30 CONTINUE  XSEC
36     35 IF (IMIN.EQ.NPTS) GO TO 60  XSEC

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37		READ (17) ((XDAT(I,J),J=1,3),I=IMIN,NPTS),LLEVEL,XDAT4	XSEC
38		GO TO 60	XSEC
	C	ILO1 IS THE NUMBER OF ENTRIES FOR LO=1, LF=1.	XSEC
39	40	IF (ILO1.NE.0) GO TO 45	XSEC
40		IFLOW=3	XSEC
41		GO TO 15	XSEC
42	45	ICOUNT=ICOUNT+1	XSEC
43		IMIN=1	XSEC
44		NPTS=LOLF11(ICOUNT)	XSEC
45		N=NPTS/1000	XSEC
46		IF (N.EQ.0) GO TO 55	XSEC
47		IMAX=1000	XSEC
48		DO 50 II=1,N	XSEC
49		READ (15) ((XDAT(I,J),J=1,3),I=IMIN,IMAX),LLEVEL,XDAT4	XSEC
50		IMIN=IMIN+1000	XSEC
51		IMAX=IMAX+1000	XSEC
52	50	CONTINUE	XSEC
53	55	IF (IMIN.EQ.NPTS) GO TO 60	XSEC
54		READ (15) ((XDAT(I,J),J=1,3),I=IMIN,NPTS),LLEVEL,XDAT4	XSEC
55	60	CONTINUE	XSEC
	C	THE XDAT ARRAY FOR A PARTICULAR MT NUMBER HAS NOW BEEN READ IN	XSEC
	C	COMPLETELY FROM TAPE FILES.	XSEC
56	65	IF (MTX.EQ.LLEVEL) GO TO 70	XSEC
57		IF (MF.EQ.0) CALL ERROR (702)	XSEC
58		MTX=MT	XSEC
59		CALL RSF3	XSEC
60		GO TO 65	XSEC
61	70	CONTINUE	XSEC
	C	TRACK A (IRES=0) AND TRACK B (IRES=1) TESTS.	XSEC
62		IF (IRES.EQ.0) GO TO 75	XSEC
	C	FOR TRACK A GO AT ONCE TO STATEMENT 71.	XSEC
	C	FOR TRACK B TRANSFER TO STMT 71 EXCEPT FOR FISSION AND CAPTURE.	XSEC
63		IF (MTX.EQ.18.OR.MTX.EQ.102) GO TO 105	XSEC
	C	THIS TRANSFER ELIMINATES LOOKING UP THE CROSS SECTIONS FROM	XSEC
	C	FILE 3. FOR THESE MATERIALS UNDER TRACK B, USE THE INPUT VALUES.	XSEC
64	75	DO 100 I=1,NPTS	XSEC
65		EN=XDAT(I,1)	XSEC
66		ILO=LOCT(E,EN,NP)	XSEC
67		IF (ILO.NE.-1) GO TO 80	XSEC
68		CSEC=0.0	XSEC
69		GO TO 95	XSEC
70	80	IHI=ILO+1	XSEC
71		DO 85 J=1,NR	XSEC
72	85	IF (IHI.LE.NBT(J)) GO TO 90	XSEC
73		WRITE (ISO,180) MAT,MF,MT	XSEC
74		CALL ERROR (701)	XSEC
75	90	CALL TERP1 (E(ILO),X(ILO),E(IHI),X(IHI),EN,CSEC,INT(J))	XSEC
76	95	XDAT(I,2)=XDAT(I,2)*CSEC	XSEC
77		XDAT(I,3)=XDAT(I,3)*CSEC	XSEC
78	100	CONTINUE	XSEC

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79      195  CONTINUE                                XSEC
C      NOW PROCEED TO INTEGRATE OVER THE NEUTRON FINE GROUPS. XSEC
C      STOPE THE RESULTS IN THE ORDER E(L+1), PLANE Y INTEGRAL, TILDA Y XSEC
C      INTEGRAL, GAMMA RAY ENERGY OR ELSE THE UPPER LIMIT OF THE GAMMA XSEC
C      RANGE.                                       XSEC
80      DO 110 J=1,NPTS                               XSEC
81      110  EX(J)=XDAT(J,1)                           XSEC
82      DO 155 II=1,NFG                               XSEC
83      KP=II+1                                       XSEC
84      ANS=0.0                                       XSEC
85      ANS1=0.0                                       XSEC
86      ILO=LOCT(EX,EMNF(KP),NPTS)                   XSEC
87      IHI=LOCT(EX,EMNF(II),NPTS)                   XSEC
88      XLOLIM=EMNF(KP)                               XSEC
89      XUPLIM=EMNF(II)                               XSEC
90      IF (ILO.NE.-1) GO TO 115                       XSEC
91      IF ((EMNF(KP).LT.EX(1)).AND.(EMNF(II).LT.EX(1))) GO TO 140 XSEC
92      ILO=1                                          XSEC
93      XLOLIM=EX(1)                                   XSEC
94      115  IF (IHI.NE.-1) GO TO 120                   XSEC
95      IF ((EMNF(KP).GT.EX(NPTS)).AND.(EMNF(II).GT.EX(NPTS))) GO TO 140 XSEC
96      IHI=NPTS-1                                     XSEC
97      XUPLIM=EX(NPTS)                               XSEC
98      120  IF (IHI.NE.ILO) GO TO 125                   XSEC
99      CALL INTG (EX(ILO),XDAT(ILO,2),EX(ILO+1),XDAT(ILO+1,2),XLOLIM,XUPL XSEC
100     1IM,2,ANS1)                                    XSEC
101     CALL INTG (EX(ILO),XDAT(ILO,3),EX(ILO+1),XDAT(ILO+1,3),XLOLIM,XUPL XSEC
102     1IM,2,ANS)                                    XSEC
103     GO TO 140                                       XSEC
104     125  IHI=IHI+1                                   XSEC
105     IMP=IHI-2                                       XSEC
106     JK=ILO+1                                       XSEC
107     C      FIRST PARTIAL INTEGRAL                    XSEC
108     CALL INTG (EX(ILO),XDAT(ILO,2),EX(JK),XDAT(JK,2),XLOLIM,EX(JK),2,A XSEC
109     1NS1)                                           XSEC
110     CALL INTG (EX(ILO),XDAT(ILO,3),EX(JK),XDAT(JK,3),XLOLIM,EX(JK),2,A XSEC
111     1NS)                                           XSEC
112     IF (IMP.LT.JK) GO TO 135                       XSEC
113     DO 130 I=JK,IMP                                 XSEC
114     IL=I+1                                          XSEC
115     C      MIDDLE INTEGRALS BETWEEN THE TABULATED FINE GROUP BOUNDARIES. XSEC
116     CALL INTG (EX(I),XDAT(I,2),EX(IL),XDAT(IL,2),EX(I),EX(IL),2,A) XSEC
117     ANS1=ANS1+A                                     XSEC
118     CALL INTG (EX(I),XDAT(I,3),EX(IL),XDAT(IL,3),EX(I),EX(IL),2,A) XSEC
119     ANS=ANS+A                                       XSEC
120     CONTINUE                                       XSEC
121     130  CONTINUE                                       XSEC
122     135  CONTINUE                                       XSEC
123     C      FINAL PARTIAL INTEGRAL                    XSEC
124     I=IHI-1                                         XSEC
125     CALL INTG (EX(I),XDAT(I,2),EX(IHI),XDAT(IHI,2),EX(I),XUPLIM,2,A) XSEC

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118      ANS1=ANS1+A                                XSEC
119      CALL INTG (EX(I),XDAT(I,3),EX(IHI),XDAT(IHI,3),EX(I),XUPLIM,2,A) XSEC
120      ANS=ANS+A                                    XSEC
121      140 CONTINUE                                XSEC
122      IF (ANS.EQ.0.0.AND.ANS1.EQ.0.0) GO TO 155 XSEC
C      ANS NOW CONTAINS THE INTEGRAL OF SIGMA(E)*YTILDA(E) XSEC
C      ANS1 CONTAINS THE INTEGRAL OF SIGMA(E)*Y(E) XSEC
C      THAT IS TRUE EXCEPT FOR MT=18 AND 102 ON TRACK B. XSEC
123      ANS=ANS/(EMNF(II)-EMNF(KP)) XSEC
124      ANS1=ANS1/(EMNF(II)-EMNF(KP)) XSEC
125      SAVE(ISTOR,1)=EMNF(II) XSEC
C      TRACK A (IRES=0) AND TRACK B (IRES=1) TESTS XSEC
126      IF (IRES.EQ.0) GO TO 145 XSEC
127      IF (MTX.NE.18.AND.MTX.NE.102) GO TO 145 XSEC
C      MT = 18 FOR FISSION MT=102 FOR CAPTURE XSEC
128      IF (MTX.EQ.18) FAC= SXSF(II)*SW(II)+RXSF(II)*RW(II) XSEC
129      IF (MTX.EQ.102) FAC= SXSC(II)*SW(II)+RXSC(II)*RW(II) XSEC
130      SAVE(ISTOR,2)=ANS1*FAC XSEC
131      SAVE(ISTOR,3)=ANS*FAC XSEC
132      GO TO 150 XSEC
133      145 SAVE(ISTOR,2)=ANS1*SW(II) XSEC
134      SAVE(ISTOR,3)=ANS*SW(II) XSEC
135      150 SAVE(ISTOR,4)=XDAT4 XSEC
136      ISTOP=ISTOR+1 XSEC
137      IF (ISTOR.LE.1000) GO TO 155 XSEC
138      NR16=NR16+1 XSEC
139      NROW(NR16)=1000 XSEC
140      WRITE (16) ((SAVE(I,J),J=1,4),I=1,1000) XSEC
141      ISTOP=1 XSEC
142      155 CONTINUE XSEC
143      GO TO (160,165), IFLOW XSEC
144      160 IF (ICOUNT.LT.LO1LF2) GO TO 15 XSEC
145      ICOUNT=0 XSEC
146      IFLOW=2 XSEC
147      GO TO 5 XSEC
148      165 IF (ICOUNT.LT.LO1LF1) GO TO 15 XSEC
149      170 IF (ISTOR.EQ.1) RETURN XSEC
150      ISTOP=ISTOR-1 XSEC
151      NR16=NR16+1 XSEC
152      NROW(NR16)=ISTOR XSEC
153      WRITE (16) ((SAVE(I,J),J=1,4),I=1,ISTOR) XSEC
154      RETURN XSEC
C XSEC
155      175 FORMAT (66X,I4,I2,I3) XSEC
156      180 FORMAT (* NO INTERPOLATION CODE FOUND IN FILE 3 MAT=*,I4,* XSEC
1 MF=*,I4,* MT=*,I4) XSEC
157      END XSEC

```

SYMBOL	REFERENCES
5	16* 147
1^	17* 18
1^	21* 24 41 144 148
2^	21 22*
25	22 25*
3^	31 35*
35	24 36*
4^	21 39*
4^	34 42*
5^	44 52*
5^	46 53*
6^	36 38 53 55*
65	56* 60
7^	56 61*
75	62 64*
8^	67 70*
85	71 72*
9^	72 75*
95	64 76*
1^0	64 78*
1^5	63 79*
110	80 81*
115	90 94*
120	44 98*
125	98 102*
130	108 114*
135	107 115*
140	91 95 101 121*
145	126 127 133*
150	132 135*
155	82 122 137 142*
160	143 144*
165	143 148*
170	21 149*
175	17RD 155*
180	73WR 156*
A	110AG 111 112AG 113 117AG 118 119AG 120
ANS	84= 100AG 106AG 113= 120= 122 123= 131 134
ANS1	85= 99AG 105AG 111= 118= 122 124= 130 133
APSAV	2CU
BOOK	8CU
BILK	6CU
C	2CU
CSEC	6d= 75AG 76 77
E	5CU 66 75AG
EAUG	4CU
EG	2CU
EAG	2CU

SUBROUTINE XSEC

EMNH	-	2CO									
EMNF	-	2CO	86	87	88	89	91	95	123	124	125
EN	-	65=	66	75AG							
ERROR	-	57	74								
EV	-	6CO	81=	86	87	91	93	95	97	99AG	100AG
	-	105AG	106AG	110AG	112AG	117AG	119AG				
FAC	-	128=	129=	130	131						
GAMM	-	2CO									
I	-	32RD	37RD	49RD	54RD	64	65	76	77	108	109
	-	110AG	112AG	116=	117AG	119AG	140WR	153WR			
IAUG	-	4CO									
ICOUNT	-	13=	25=	27	42=	44	144	145=	148		
IFN	-	3CO	16	17RD							
IFLOW	-	14=	21	23=	40=	143	146=				
IWI	-	70=	72	75AG	87=	94	96=	98	102=	103	116
	-	117AG	119AG								
IT	-	31	48	82	83	87	89	91	95	123	124
	-	125	128	129	133	134					
II	-	109=	110AG	112AG							
IIO	-	66=	67	70	75AG	86=	90	92=	98	99AG	100AG
	-	104	105AG	106AG							
ILO1	-	4CO	10	39							
ILO2	-	4CO									
IM	-	2CO									
IMAX	-	31=	32RD	34=	47=	49RD	51=				
IMIN	-	26=	32RD	33=	36	37RD	43=	49RD	50=	53	54RD
IMP	-	103=	107	108							
INT	-	5CO	75AG								
INTG	-	99	100	105	106	110	112	117	119		
IPO	-	2CO									
IPES	-	2CO	62	126							
ISAVE	-	7CO									
IST	-	3CO									
ISO	-	3CO	73WR								
ISTOP	-	15=	125	130	131	133	134	135	136=	137	141=
	-	149	150=	152	153WR						
IWO	-	2CO									
IYDA	-	4CO									
IYSD	-	4CO	10	22							
I7M	-	2CO									
J	-	32RD	37RD	49RD	54RD	71	72	75AG	80	81	140WR
	-	153WR									
JK	-	104=	105AG	106AG	107	108					
KP	-	83=	86	88	91	95	123	124			
LI EVL	-	32RD	37RD	49RD	54RD	56					
LO1LF1	-	8CO	148								
LO1LF2	-	8CO	144								
LOCT	-	9EX	66	86	87						
LOLF11	-	8CO	44								
LOLF12	-	8CO	27								



MA	-	200																		
MAT	-	500	17RD	73WR																
MATX	-	400																		
M3	-	200																		
MC	-	200																		
MCR	-	200																		
MF	-	500	17RD	18	57	73WR														
MM	-	200																		
MC	-	200																		
MT	-	500	17RD	19	58	73WR														
MTNO	-	400																		
MTSL	-	400																		
MTX	-	19=	56	58=	63	127	128	129												
M7	-	200																		
N	-	28=	29	31	45=	46	48													
NHG	-	200																		
NHT	-	500	72																	
NFNH	-	200																		
NFNF	-	200																		
NFG	-	200	82																	
NGAN	-	200																		
NGG	-	200																		
NPAT	-	200																		
NHM	-	200																		
NP	-	500	66																	
NPM	-	200																		
NPTS	-	27=	28	36	37RD	44=	45	53	54RD	64	80									
		86	87	95	96	97														
NP	-	500	71																	
NP16	-	800	138=	139	151=	152														
NP0#	-	800	139=	152=																
OVER1	-	400																		
R	-	200																		
READ	-	500																		
RETURN	-	10	149	154																
RF3	-	20	59																	
RW	-	200	128	129																
RXSC	-	200	129																	
RXSF	-	200	128																	
SAVE	-	700	125=	130=	131=	133=	134=	135=	140WR	153WR										
S#	-	200	128	129	133	134														
SXSC	-	200	129																	
SXSF	-	200	128																	
TAPES	-	300																		
TFRP1	-	75																		
X	-	500	75AG																	
XDAT	-	600	32RD	37RD	49RD	54RD	65	76=	77=	81	99AG									
		100AG	105AG	106AG	110AG	112AG	117AG	119AG												
XDAT4	-	32RD	37RD	49RD	54RD	135														
XIOLIM	-	88=	93=	99AG	100AG	105AG	106AG													

XHD	-	200																		
XSEC	-	1																		
XIPLIM	-	89=	97=	99AG	100AG	117AG	119AG													

## SUBROUTINE MATRIX

```

1      SUBROUTINE MATRIX                                MATRIX
C      MATRIX READS THE MICROSCOPIC FINE GROUP PHOTON AND ENERGY PRODUCT- MATRIX
C      ION MATRIX ELEMENTS MULTIPLIED BY THE WEIGHTING FUNCTIONS AND      MATRIX
C      PERFORMS THE SUM OVER FINE GROUPS TO PRODUCE THE G X N MATRICES  MATRIX
C      WHICH ARE WRITTEN ONTO TAPE 18.                                MATRIX
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,I00,IRES,I BLANK
      IWO,IZM,MA(100),MR(50),MC(50),MCR,MM,MS,MZ(10),NRG,NENB,NENF,NFG,NG BLANK
      2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW BLANK
      3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV
3      COMMON /OVER1/ EAUG(2000),IAUG,IL01,IL02,IXDA,IXSD,MATX,MTNO(40),M OVER1
      ITSL
4      COMMON /BULK/ XDAT(3020,4)                                MATRIX
5      COMMON /SAVE/ XMAT(50,50),XEMAT(50,50)                   SAVE2
6      COMMON /BOOK/ L01LF2,L01LF12(100),L01LF1,L01LF11(500),NR16,NROW(100) BOOK
7      REWIND 16                                                MATRIX
8      DO 5 I=1,NGAM                                             MATRIX
9      DO 5 J=1,NENB                                             MATRIX
10     XEMAT(I,J)=0.0                                           MATRIX
11     5 XMAT(I,J)=0.0                                           MATRIX
12     IF (MTNO(1).EQ.0) GO TO 20                                MATRIX
13     DO 15 J=1,NR16                                           MATRIX
14     IMAX=NROW(J)                                             MATRIX
15     READ (16) ((XDAT(I,K),K=1,4),I=1,IMAX)                   MATRIX
16     DO 10 IB=1,NRG                                           MATRIX
17     DO 10 IG=1,NGG                                           MATRIX
18     DO 10 I=1,IMAX                                           MATRIX
19     IF ((XDAT(I,4).GT.EMG(IG)).OR.(XDAT(I,4).LE.EMG(IG+1))) GO TO 10 MATRIX
20     IF ((XDAT(I,1).GT.EMNB(IB)).OR.(XDAT(I,1).LE.EMNB(IB+1))) GO TO 10 MATRIX
21     XMAT(IG,IB)=XMAT(IG,IB)+XDAT(I,2)                         MATRIX
22     XEMAT(IG,IB)=XEMAT(IG,IB)+XDAT(I,3)                       MATRIX
23     10 CONTINUE                                              MATRIX
24     15 CONTINUE                                              MATRIX
25     20 WRITE (18) ((XMAT(IG,IB),IB=1,NRG),IG=1,NGG),((XEMAT(IG,IB),IB=1,N
      1NRG),IG=1,NGG)
26     RETURN                                                    MATRIX
27     END                                                        MATRIX

```

SYMBOL	REFERENCES
S	8 9 11*
1n	16 17 18 19 20 23*
1F	13 24*
2n	12 25*
AWRSAV	200
BOOK	600
BULK	400
C	200
E AUG	300
ER	200
E4G	200 19
E4NB	200 20
E4NF	200
GAMM	200
I	8 10 11 15RD 18 19 20 21 22
I AUG	300
IR	16 20 21 22 25WR
IR	17 19 21 22 25WR
IL01	300
IL02	300
IM	200
I4AX	14# 15RD 18
I00	200
I0ES	200
I40	200
IXDA	300
IXSU	300
I7M	200
J	9 10 11 13 14
K	15RD
L01LF1	600
L01LF2	600
L0LF11	600
L0LF12	600
MA	200
MATRIX	i
MATX	300
MR	200
MC	200
MCR	200
M4	200
MS	200
MTNO	300 12
MTSL	300
M7	200
NR0	200 16 25WR
NFN0	200 9
NFNF	200

NFG	-	2C0					
NGAM	-	2C0	A				
N3G	-	2C0	17	25WR			
NMAT	-	2C0					
NVM	-	2C0					
NPM	-	2C0					
NP16	-	6C0	13				
NDOW	-	6C0	14				
OVER1	-	3C0					
R	-	2C0					
RETURN	-	26					
Rw	-	2C0					
RySC	-	2C0					
RySF	-	2C0					
SAVE	-	5C0					
Sw	-	2C0					
SySC	-	2C0					
SySF	-	2C0					
XDAT	-	4C0	15RD	19	20	21	22
XFMAT	-	5C0	10=	22=	25WR		
XMAT	-	5C0	11=	21=	25WR		
XID	-	2C0					

.....

I N D E X

OVERLAY(LAPH,3,0)

PAGE 85

1 OVERLAY(LAPH,3,0)

SOURCE

I N D E X

PROGRAM SOURCE

PAGE 86

1		PROGRAM SOURCE	SOURCE
	C		SOURCE
	C	SOURCE SUPERVISES THE CALCULATION OF THE PHOTON SOURCE AND ENERGY	SOURCE
	C	SOURCE VECTORS.	SOURCE
	C		SOURCE
2		COMMON C,EG(50),EMG(50),EHNB(100),EMNF(100),GAMM(50),IM,IOO,IPRES,I	BLANK
		1WO,IZM,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NRG,NENB,NENF,NFG,NG	BLANK
		2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW	BLANK
		3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV	BLANK
3		COMMON /VEC/ A(30000)	VEC
4		IP=NGG*NRG*NPM+1	SOURCE
	C	(IP-1) IS THE LENGTH OF THE ARRAY USED FOR STORING THE PHOTON	SOURCE
	C	PRODUCTION OR ENERGY PRODUCTION MATRICES. THEREFORE, A(IP) IS	SOURCE
	C	THE FIRST ELEMENT OF THE FLUX ARRAY.	SOURCE
5		IQ=IP+NRG*IM	SOURCE
	C	IQ IS THE FIRST LOCATION OF THE SOURCE VECTOR ARRAY.	SOURCE
6		IR=IP-1+IQ+NGG*IM	SOURCE
	C	IR IS THE AMOUNT OF STORAGE REQUIRED FOR THE PHOTON PRODUCTION	SOURCE
	C	MATRIX, THE NEUTRON FLUXES, AND THE SOURCE VECTOR ARRAY.	SOURCE
7		IF (IR.GT.30000) CALL ERROR (800)	SOURCE
8		IF (IOO.EQ.10*(IOU/10)) GO TO 10	SOURCE
9		JMIN=IP	SOURCE
10		JMAX=IP+IM-1	SOURCE
11		DO 5 I=1,NRG	SOURCE
12		READ (5) (A(J),J=JMIN,JMAX)	SOURCE
13		JMIN=JMAX+1	SOURCE
14	5	JMAX=JMAX+IM	SOURCE
15	10	IF (IOO.GE.10.AND.IOO.LT.20) GO TO 15	SOURCE
16		CALL READX (A,NGG,NRG,NPM,MCR,1)	SOURCE
17		CALL MIXCX (A,NGG,NRG,NPM,0)	SOURCE
18		CALL VECTOR (A(1),A(IP),A(IQ),NGG,NRG,NPM,IM,0)	SOURCE
19		IF (IOO.LT.20) RETURN	SOURCE
20	10	CALL READX (A,NGG,NRG,NPM,MCR,2)	SOURCE
21		CALL MIXCX (A,NGG,NRG,NPM,1)	SOURCE
22		CALL VECTOR (A(1),A(IP),A(IQ),NGG,NRG,NPM,IM,1)	SOURCE
23		RETURN	SOURCE
24		END	SOURCE

SYMBOL	REFERENCES	REFERENCES																			
S	-	11	14*																		
I	-	8	15*																		
IA	-	15	20*																		
A	-	3C0	12RD	16AG	17AG	18AG	20AG	21AG	22AG												
AARSAV	-	2C0																			
C	-	2C0																			
EQ	-	2C0																			
ENG	-	2C0																			
EMNH	-	2C0																			
EMNF	-	2C0																			
ERROR	-	7																			
GAMM	-	2C0																			
I	-	11																			
IM	-	2C0	5	6	10	14	18AG	22AG													
IOO	-	2C0	8	15	19																
ID	-	4=	5	6	9	10	18AG	22AG													
IO	-	5=	6	18AG	22AG																
ID	-	6=	7																		
IPES	-	2C0																			
IWO	-	2C0																			
I7M	-	2C0																			
J	-	12RD																			
JMAX	-	10=	12RD	13	14=																
JMIN	-	9=	12RD	13=																	
MA	-	2C0																			
MR	-	2C0																			
MC	-	2C0																			
MCR	-	2C0	16AG	20AG																	
MIXCX	-	17	21																		
M4	-	2C0																			
M5	-	2C0																			
M7	-	2C0																			
N4G	-	2C0	4	5	11	16AG	17AG	18AG	20AG	21AG	22AG										
N4NB	-	2C0																			
N4NF	-	2C0																			
N4G	-	2C0																			
NGAM	-	2C0																			
NGG	-	2C0	4	6	16AG	17AG	18AG	20AG	21AG	22AG											
N4AT	-	2C0																			
NNM	-	2C0																			
NP4	-	2C0	4	16AG	17AG	18AG	20AG	21AG	22AG												
R	-	2C0																			
READX	-	16	20																		
RFTURN	-	19	23																		
Rw	-	2C0																			
RXSC	-	2C0																			
RXSF	-	2C0																			
SW	-	2C0																			

SXSC	-	2C0																			
SXSF	-	2C0																			
VFC	-	3C0																			
VFACTOR	-	18	22																		
X4D	-	2C0																			



1		SUBROUTINE READX (X,NGG,NRG,NPM,MCR,IFLAG)	READX
	C		READX
	C	THIS SUBROUTINE READS EITHER THE PHOTON PRODUCTION OR ENERGY	READX
	C	PRODUCTION MICROSCOPIC MATRICES FROM TAPE 18.	READX
	C		READX
2		DIMENSION X(NGG,NRG,NPM)	READX
3		REWIND 18	READX
4		IF (IFLAG.EQ.2) GO TO 10	READX
5		IF (IFLAG.NE.1) CALL ERROR (900)	READX
6		DO 5 I=1,MCR	READX
7	5	READ (18) ((X(IG,IR,I),IR=1,NRG),IG=1,NGG)	READX
8		RETURN	READX
9	10	DO 15 I=1,MCR	READX
10	10	HEAD (18) ((X(IG,IR,I),IR=1,NRG),IG=1,NGG),((X(IG,IR,I),IR=1,NRG),	READX
		1IG=1,NGG)	READX
11		RETURN	READX
12		END	READX

SYMBOL	=	=	=	=	=	=	=	=	=	REFERENCES	=	=	=	=	=	=
S	-	0								7*						
10	-	4								9*						
15	-	9								10*						
ERROR	-	5														
I	-	0								7RD	9					10RD
I*	-	7RD								10RD						
IFLAG	-	1AG								4	5					
IG	-	7RD								10RD						
MCR	-	1AG								6	9					
NRG	-	1AG								2DI	7RD					10RD
NGG	-	1AG								2DI	7RD					10RD
NPM	-	1AG								2DI						
READX	-	1														
RETURN	-	8								11						
X	-	1AG								2DI	7RD					10RD

SUBROUTINE MIXCX (X,NGG,NBG,NPM,IFLAG)

```

1      SUBROUTINE MIXCX (X,NGG,NBG,NPM,IFLAG)
C
C      THIS ROUTINE MULTIPLIES THE MICROSCOPIC MATRICES BY THE SPECIFIED
C      NUMBER DENSITIES AND PRINTS THE MACROSCOPIC MATRICES.
2      COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,IOO,IRES,I
1W0,IZH,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NRG,NENB,NENF,NFG,NG
2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW
3(100),SXSC(100),SXSF(100),XMD(50),AWRSV
C      COMMON /TAPES/ ISI,ISO,IEN
4      DIMENSION X(NGG,NBG,NPM)
5      IPR=IOO-10*(IOO/10)
6      IF (MS.EQ.0) GO TO 20
7      DO 15 M=1,MS
8          K=MB(M)
9          L=MC(M)
10         A=XMD(M)
11         DO 15 I=1,NGG
12             DO 15 J=1,NBG
13                 IF (L) 10,5,10
14                 X(I,J,K)=X(I,J,K)*A
15             GO TO 15
16             X(I,J,K)=X(I,J,K)+A*X(I,J,L)
17         CONTINUE
18         DO 45 I=1,NPM
19             IF (IPR.GT.2.AND.I.LE.MCR) GO TO 25
20             IF (IFLAG.EQ.0) WRITE (ISO,50) I
21             IF (IFLAG.EQ.1) WRITE (ISO,55) I
22         KA=1
23         KB=8
24         KC=MIN0(KB,NBG)
25         IF (IPR.GT.2.AND.I.LE.MCR) GO TO 40
26         WRITE (ISO,60) (K,K=KA,KC)
27         WRITE (ISO,65)
28         DO 35 J=1,NGG
29             WRITE (ISO,70) J,(X(J,K,I),K=KA,KC)
30         KA=KA+8
31         KB=KB+8
32         IF (KA.LE.NBG) GO TO 30
33         CONTINUE
34         RETURN
C      A NON-FATAL ERROR MESSAGE WILL BE PRINTED COMPLAINING THAT THE
C      ARGUMENTS IN THE CALLING SEQUENCE APPEAR IN BLANK COMMON. THIS
C      IS DUE TO THE USE OF VARIABLE DIMENSIONING.
35     50    FORMAT (*1          PHOTON PRODUCTION MATRIX FOR MATERIAL (OR MIXTU
1RE)*,I3,/)
36     55    FORMAT (*1          PHOTON ENERGY PRODUCTION MATRIX FOR MATERIAL (
1OR MIXTURE)*,I3,/)
37     60    FORMAT (1H0,5X,B(2X,5HGROUP,I3,3X))

```

SUBROUTINE MIXCX (X,NGG,NBG,NPM,IFLAG)

```

38     65    FORMAT (1H )
39     70    FORMAT (I4,1PB13.5)
40     END

```



SYMBOL	REFERENCES									
5	-	13	14*							
11	-	13	16*							
15	-	7	11	12	15	17*				
21	-	6	18*							
25	-	19	22*							
31	-	24*	32							
35	-	28	29*							
41	-	25	30*							
45	-	18	33*							
51	-	20WR	35*							
55	-	21WR	36*							
61	-	26WR	37*							
65	-	27WR	38*							
71	-	29WR	39*							
A	-	10=	14	16						
AURSAV	-	2CO								
C	-	2CO								
EG	-	2CO								
EMG	-	2CO								
EINH	-	2CO								
ENF	-	2CO								
GMM	-	2CO								
I	-	11	14	16	18	19	20WR	21WR	25	29WR
IFN	-	3CO								
IFLAG	-	1AG	20	21						
IV	-	2CO								
INO	-	2CO	5							
IPR	-	5=	19	25						
IPES	-	2CO								
ISI	-	3CO								
ISO	-	3CO	20WR	21WR	26WR	27WR	29WR			
IWO	-	2CO								
I7M	-	2CO								
J	-	12	14	16	28	29WR				
K	-	8=	14	16	26WR	29WR				
KA	-	22=	26WR	29WR	30=	32				
KR	-	23=	24	31=						
KC	-	24*	26WR	29WR						
L	-	9=	13	16						
M	-	7	8	9	10					
MA	-	2CO								
MR	-	2CO	8							
MC	-	2CO	9							
MCR	-	2CO	19	25						
MTNO	-	24								
MIXCX	-	1								
MM	-	2CO								
MS	-	2CO	6	7						

SUBROUTINE MIXCX (X,NGG,NBG,NPM,IFLAG)

MZ	-	2CO					
NHG	-	1AG	2CO	4DI	12	24	32
NPNB	-	2CO					
NPNF	-	2CO					
NFG	-	2CO					
NHAM	-	2CO					
VGG	-	1AG	2CO	4DI	11	28	
NMAT	-	2CO					
NJM	-	2CO					
NPM	-	1AG	2CO	4DI	18		
R	-	2CO					
RETURN	-	34					
RH	-	2CO					
RXSC	-	2CO					
RXSF	-	2CO					
S <sub>w</sub>	-	2CO					
SXSC	-	2CO					
SXSF	-	2CO					
TAPES	-	3CO					
X	-	1AG	4DI	14=	16=	29WR	
XMD	-	2CO	10				



```

SUBROUTINE VECTOR (X,PHI,S,NGG,NBG,NPM,IM,IFLAG)
1 SUBROUTINE VECTOR (X,PHI,S,NGG,NBG,NPM,IM,IFLAG) VECTOR
C VECTOR VECTOR
C VECTORS AND THE SCALAR RENORMALIZATION CONSTANT TO GIVE THE SOURCE VECTOR
C VECTORS. VECTOR
C VECTOR
2 COMMON C,EG(50),EMG(50),EMNB(100),EMNF(100),GAMM(50),IM,I00,IRES,I BLANK
1WO,IZM,MA(100),MB(50),MC(50),MCR,MM,MS,MZ(10),NBG,NENB,NENF,NFG,NG BLANK
2AM,NGG,NMAT(10),NNM(126),NPM,R(101),RW(100),RXSC(100),RXSF(100),SW BLANK
3(100),SXSC(100),SXSF(100),XMD(50),AWRSAV BLANK
3 COMMON /TAPES/ ISI,ISO,IEN TAPES
4 DIMENSION X(NGG,NBG,NPM), PHI(IM,NBG), S(IM,NGG) VECTOR
5 IF (I00.EQ.10*(I00/10)) RETURN VECTOR
6 IPR=I00-10*(I00/10) VECTOR
7 DO 5 I=1,NGG VECTOR
8 DO 5 J=1,IM VECTOR
9 S(J,I)=0.0 VECTOR
10 DO 10 I=1,IM VECTOR
11 K=MA(I) VECTOR
C K TELLS ME THAT THE I-TH INTERVAL IS IN THE K-TH ZONE. VECTOR
12 KK=MZ(K) VECTOR
C KK TELLS ME THAT THE KK-TH MIXTURE IS USED IN THE K-TH ZONE. VECTOR
13 DO 10 J=1,NGG VECTOR
14 DO 10 N=1,NBG VECTOR
15 S(I,J)=S(I,J)+C*X(J,N,KK)*PHI(I,N) VECTOR
16 CONTINUE VECTOR
17 IF (IFLAG.EQ.0) WRITE (ISO,25) VECTOR
18 IF (IFLAG.EQ.1) WRITE (ISO,30) VECTOR
19 DO 15 J=1,IM VECTOR
20 WRITE (ISO,35) J,R(J),R(J+1),(S(J,I),I=1,NGG) VECTOR
21 IF (IPR.EQ.2.OR.IPR.EQ.4) GO TO 20 VECTOR
22 RETURN VECTOR
23 I=IM*NGG VECTOR
24 IF (IFLAG.EQ.0) IMOL=6HSOURCE VECTOR
25 IF (IFLAG.EQ.1) IMOL=6HENERGY VECTOR
26 CALL PUNCR (S,I,IMOL) VECTOR
27 RETURN VECTOR
C A NON-FATAL ERROR MESSAGE WILL BE PRINTED COMPLAINING THAT THE VECTOR
C ARGUMENTS IN THE CALLING SEQUENCE APPEAR IN BLANK COMMON. THIS VECTOR
C IS DUE TO THE USE OF VARIABLE DIMENSIONING. VECTOR
C VECTOR
28 25 FORMAT (*1 PHOTON PRODUCTION SOURCE VECTORS AT INDICATED ME VECTOR
1SH INTERVALS*,/) VECTOR
29 30 FORMAT (*1 PHOTON ENERGY PRODUCTION SOURCE VECTORS AT INDICATED VECTOR
1ATED MESH INTERVALS*,/) VECTOR
30 35 FORMAT (* FOR MESH INTERVAL*,I3,* ROUNDED BY RADII R=*,1PE12.4 VECTOR
1,* AND R=*,1PE12.4,* THE VECTOR IS*,/,(1PE16.8)) VECTOR
31 END VECTOR

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SYMBOL	REFERENCES
S	7 8 9*
1*	10 13 14 16*
15	19 20*
2*	21 23*
25	17WR 28*
3*	18WR 29*
35	20WR 30*
A,RSAY	2CO
C	2CO 15
EG	2CO
EMG	2CO
E*NB	2CO
E*NF	2CO
GAMM	2CO
I	7 9 10 11 15 20WR 23= 26AG
IFN	3CO
IFLAG	1AG 17 18 24 25
IROL	24= 25= 26AG
IA	1AG 2CO 4DI 8 10 19 23
IOO	2CO 5 6
IDR	6= 21
IPES	2CO
ICI	3CO
ISO	3CO 17WR 18WR 20WR
IWO	2CO
I7M	2CO
J	8 9 13 15 19 20WR
K	11= 12
KK	12= 15
MA	2CO 11
MR	2CO
MC	2CO
MCR	2CO
M*	2CO
MS	2CO
M7	2CO 12
N	14 15
NG	1AG 2CO 4DI 14
NFNH	2CO
N*NF	2CO
NFG	2CO
NGAM	2CO
NGG	1AG 2CO 4DI 7 13 20WR 23
N*AI	2CO
N*IM	2CO
NPM	1AG 2CO 4DI
PHI	1AG 4DI 15
PHNCR	26

R	2CO 20WR
RETURN	5 22 27
Rw	2CO
RXSC	2CO
RXSF	2CO
S	1AG 4DI 9= 15= 20WR 26AG
S*	2CO
SXSC	2CO
SXSF	2CO
TAPES	3CO
VFCTOK	1
X	1AG 4DI 15
X*O	2CO

1		SUBROUTINE PUNCR (VECP,INP,IHOL)	PUNCR
2		COMMON /TAPES/ NINP,NOUT,IEN	PUNCR
3		DIMENSION VECP(1)	PUNCR
	C	THE PURPOSE OF THIS CODE IS TO PUNCH AND	PUNCR
	C	SERIALLY NUMBER A FLOATING POINT VECTOR	PUNCR
	C	IN THE STANDARD DTF CROSS SECTION FORMAT.	PUNCR
	C	CALLING SEQUENCE ENTRIES J	PUNCR
	C	VECP IS THE VECTOR TO BE PUNCHED.	PUNCR
	C	IBP IS THE START OF THAT VECTOR.	PUNCR
	C	INP IS THE IS THE NUMBER TO PUNCH.	PUNCR
	C	COMMON PARAMETERS J	PUNCR
	C	NOUT IS THE SYSTEM OUTPUT UNIT NUMBER.	PUNCR
	C	TEMPORARY STORAGE J	PUNCR
	C	NPP IS THE MAXIMUM NUMBER TO PUNCH.	PUNCR
	C	ICARD IS THE CARD COUNT.	PUNCR
	C	INPT IS THE WORKING COUNT.	PUNCR
	C	IBPW IS THE START OF THE LOOP.	PUNCR
	C	IEPW IS THE END OF THE LOOP.	PUNCR
	C	NPPW IS THE WORKING NUMBER TO DO ON THAT CARD.	PUNCR
4		IBP=1	PUNCR
5		NPP=6	PUNCR
6		ICARD=1	PUNCR
7		INPT=INP	PUNCR
8		IF (INPT.LT.0) GO TO 70	PUNCR
9		IRPW=IBP	PUNCR
	C	RETURN FOR NEXT PUNCH.	PUNCR
10	5	CONTINUE	PUNCR
11		IF (INPT.GT.0) GO TO 15	PUNCR
	C	RETURN.	PUNCR
12	10	CONTINUE	PUNCR
13		RETURN	PUNCR
	C	PROCESS UNIT.	PUNCR
14	15	CONTINUE	PUNCR
15		IF (INPT-NPP) 75,20,25	PUNCR
	C	EQUAL TO CARD FULL.	PUNCR
16	20	CONTINUE	PUNCR
17		INPT=0	PUNCR
	C	GREATER THAN CARD FULL.	PUNCR
18	25	CONTINUE	PUNCR
19		NPPW=NPP	PUNCR
	C	COMPUTE ENDING VALUE.	PUNCR
20	30	CONTINUE	PUNCR
21		IEPW=IBPW+NPPW-1	PUNCR
22		INPT=INPT-NPPW	PUNCR
23		GO TO (35,45,50,55,60,65), NPPW	PUNCR
	C	ONE NUMBER.	PUNCR
24	35	CONTINUE	PUNCR
25		PUNCH 80, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
	C	INCREASE CARD COUNT.	PUNCR
26	40	CONTINUE	PUNCR

27		ICARD=ICARD+1	PUNCR
28		IBPW=IEPW+1	PUNCR
29		GO TO 5	PUNCR
30	45	CONTINUE	PUNCR
31		PUNCH 85, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
32		GO TO 40	PUNCR
33	50	CONTINUE	PUNCR
34		PUNCH 90, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
35		GO TO 40	PUNCR
36	55	CONTINUE	PUNCR
37		PUNCH 95, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
38		GO TO 40	PUNCR
39	60	CONTINUE	PUNCR
40		PUNCH 100, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
41		GO TO 40	PUNCR
	C	PUNCH FULL CARD.	PUNCR
42	65	CONTINUE	PUNCR
43		PUNCH 105, (VECP(I),I=IBPW,IEPW),IHOL,ICARD	PUNCR
44		GO TO 40	PUNCR
	C	PRINT ERROR MESSAGE.	PUNCR
45	70	CONTINUE	PUNCR
46		WRITE (NOUT,110)	PUNCR
47		GO TO 10	PUNCR
	C	COUNT LESS THAN MAXIMUM.	PUNCR
48	75	CONTINUE	PUNCR
49		NPPW=INPT	PUNCR
50		INPT=0	PUNCR
51		GO TO 30	PUNCR
	C		PUNCR
52	80	FORMAT (1P1(3X,E9.2),60X,A6,I2)	PUNCR
53	85	FORMAT (1P2(3X,E9.2),48X,A6,I2)	PUNCR
54	90	FORMAT (1P3(3X,E9.2),36X,A6,I2)	PUNCR
55	95	FORMAT (1P4(3X,E9.2),24X,A6,I2)	PUNCR
56	100	FORMAT (1P5(3X,E9.2),12X,A6,I2)	PUNCR
57	105	FORMAT (1P6(3X,E9.2),A6,I2)	PUNCR
58	110	FORMAT (42H0 SPECIFICATION FOR PUNCH BLOCK IN ERROR. )	PUNCR
59		END	PUNCR

SUBROUTINE PUNCR (VECP,INP,IHOL)

SYMBOL	REFERENCES
5	10* 29
1^	12* 47
15	11 14*
2^	15 16*
25	15 18*
3^	20* 51
35	23 24*
4^	26* 32 35 38 41 44
45	23 30*
5^	23 33*
55	23 36*
6^	23 39*
65	23 42*
7^	8 45*
75	15 48*
8^	25PU 52*
85	31PU 53*
9^	34PU 54*
95	37PU 55*
1^0	40PU 56*
1^5	43PU 57*
110	46WR 58*
I	25PU 31PU 34PU 37PU 40PU 43PU
I^P	4= 9
IRPW	9= 21 25PU 28= 31PU 34PU 37PU 40PU 43PU
ICARD	6= 25PU 27= 31PU 34PU 37PU 40PU 43PU
IEN	2C0
IFPW	21= 25PU 28 31PU 34PU 37PU 40PU 43PU
IHOL	1AG 25PU 31PU 34PU 37PU 40PU 43PU
INP	1AG 7
INPT	7= 8 11 15 17= 22= 49 50=
N^NP	2C0
N^OUT	2C0 46WR
NPP	5= 15 19
N^PW	19= 21 22 23 49=
PUNCR	1
RETURN	13
TAPES	2C0
VECP	1AG 30I 25PU 31PU 34PU 37PU 40PU 43PU